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VIBRATIONAL CHARACTERISTICS OF
LARGE COMPLEX SPACE VEHICLES

FINAL REPORT

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FOREWORD

The work described in this report was carried out by Lockheed Missiles & Space Company, Huntsville Research & Engineering Center for the George C. Marshall Space Flight Center of the National Aeronautics and Space Administration, Contract NAS8-20161.

The work was administered under the direction of the Aero-Astroynamics Laboratory, NASA/MSFC, with Dr. George F. McDonough as Contracting Officer Representative.

SUMMARY

Results are presented of an analytical study involving development of methods of analysis of the vibrational characteristics of a class of large, complex space vehicles.

The method of analysis and computer program presented in this report provide a practical and accurate means of calculating the lateral modes and frequencies of a broad class of non-symmetrical vehicles. An energy method of solution involving the solution of only relatively low-order eigenproblems is used, so that computer execution times are short. For example, many modes and frequencies of a typical Saturn V configuration may be computed in three or four minutes of IBM 7094 time, including the generation of an extensive set of SC-4020 plots of both the problem definition data and the vehicle mode shapes.

The formulation upon which the program is based is presented in detail. A discussion of the computer program itself is presented, including a User's Manual which provides a guide to the use of the program.

A listing of the program, sample printed output, and solution data for a number of examples are included in the Appendixes.

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Section 1

INTRODUCTION

The method of analysis and computer program presented in this report provide a practical and accurate means of calculating the lateral modes and frequencies of a broad class of non-symmetrical space vehicles. In this analysis vehicles are modeled as a tandem sequence of non-uniform beams interconnected by arbitrary elastic interstages, with branch beams representing engines and internally cantilevered payloads, etc. Each beam is assumed to have two symmetry planes, with properties in the two planes not necessarily equal. The orientation relative to the vehicle pitch and yaw directions of the principal directions of the individual beams is arbitrary.

An energy method of solution is utilized which requires only a relatively small number of degrees of freedom, hence very short computer execution time. The generalized coordinates employed are: (1) the coefficients of arbitrary sets of lateral displacement functions representing the bending deformations of the individual beams, (2) the lateral displacement components of the end points of the beams, and (3) coordinates specifying the motions of the branch beams relative to their points of attachment to the vehicle.

The usual Timoshenko beam postulates are employed in calculating the kinetic and potential energy quadratic forms characterizing the states of the individual beams. (In the case of beams which are cylindrical shells of revolution, the Timoshenko beam postulates coincide identically with linear shell theory for the lateral bending modes - even if the shell properties vary meridionally.)

The interstages connecting the beams are assumed to be very light compared to the beams themselves, so that their kinetic energies may be adequately represented by placing appropriate lumped masses at the ends

of beams they interconnect. The flexibility characteristics of interstages are characterized by 4×4 flexibility matrices representing the relation between the (quasi-static) relative motions of the interstage extremities and the corresponding stress resultant quantities. Consider, for example, a conical interstage with stiff end rings, as shown in Figure 1-1.

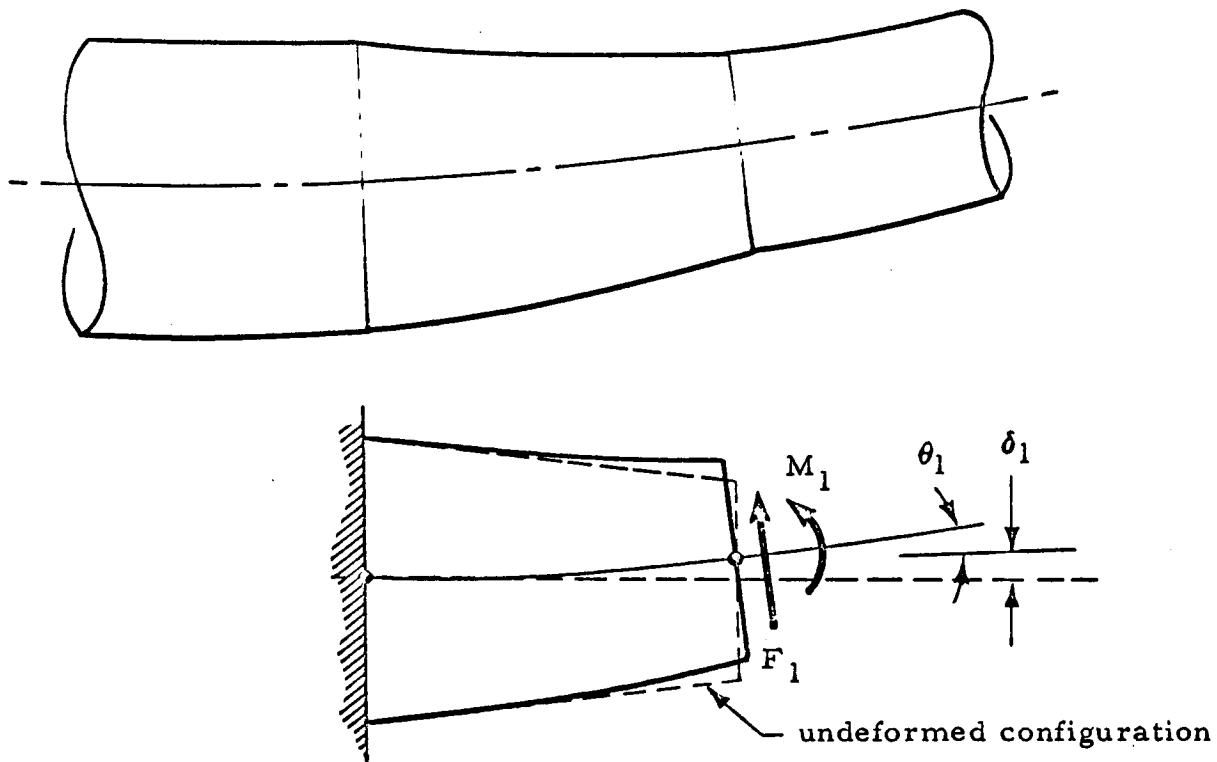


Figure 1-1 - Typical Interstage

If the above conical interstage were rotationally symmetric, it would be a straightforward matter to calculate* a 2×2 flexibility matrix, D_{11} , such that

*See e.g., Reference 3.

$$\begin{bmatrix} \delta_1 \\ \theta_1 \end{bmatrix} = D_{11} \begin{bmatrix} F_1 \\ M_1 \end{bmatrix}$$

where the subscript (1) refers to the plane of Figure 1-1. For any other plane, say plane 2, we have similarly

$$\begin{bmatrix} \delta_2 \\ \theta_2 \end{bmatrix} = D_{22} \begin{bmatrix} F_2 \\ M_2 \end{bmatrix}$$

and, for a shell of revolution, $D_{22} = D_{11}$. In general, however, interstages may be elastically non-symmetrical and their force-deflection characteristics are represented as

$$\begin{bmatrix} \delta_1 \\ \theta_1 \\ \delta_2 \\ \theta_2 \end{bmatrix} = \begin{bmatrix} D_{11} & D_{12} \\ (D_{12})^t & D_{22} \end{bmatrix} \begin{bmatrix} F_1 \\ M_1 \\ F_2 \\ M_2 \end{bmatrix},$$

where D_{11} and D_{22} are not necessarily equal, and where D_{12} is generally non-zero.

Interstage flexibility characteristics may, of course, be determined in various ways; for example the flexibility matrix of a complicated interstage (e.g., the Apollo Command Module-Service Module interstage) might best be determined by a static test.

The computer program developed to implement the method described in this report is coded in FORTRAN IV and configured for execution on the IBM 7094/SC-4020. Appendix B contains a list of the program and printed output for a sample problem. Appendix A presents the solutions, including

SC-4020 output, for several test problems. The SC-4020 plots present the projections of the vehicle mode shapes onto the pitch and yaw planes. Since most of the examples presented in the appendixes involve rotationally symmetrical vehicles, the corresponding solutions appear as pure pitch (or yaw) modes. In such cases, the program has actually computed two separate modes (a pitch mode and a yaw mode) at the same frequency. For brevity, only one of each such pairs of planar modes is included in the appendixes. In general , however, vehicle modes may be non-planar. The functioning of the program for non-symmetrical vehicles has been carefully checked out in a sequence of test executions. One such solution is included as Problem 2 in Appendix A.

Program execution time is relatively short; for example, calculation of a complete set of Saturn V modes and frequencies requires 2 to 5 minutes of IBM 7094 execution time, depending on the amount and type of output data requested. The program is set up primarily for analysis of free-free vehicles; however, provision is included for external support springs so that cantilever modes, etc., can also be calculated.

Section 2
FORMULATION

2.1 Mathematical Model

The mathematical model for this analysis consists of a system of linearly connected "beams" joined by "interstages" representable by 4×4 flexibility matrices. (See Figure 2-1.) The cross section of each of the beams has two axes of symmetry which define two principal directions for that beam. The properties of a beam may be different in the two principal directions. Each beam may be oriented such that its principal axes do not coincide with a set of reference axes (pitch and yaw) for the system.

A "branch beam" with two degrees of freedom may be included at each interstage.

The bending of the individual beams is characterized by arbitrary shape functions for each principal direction.

2.2 Coordinates

The generalized coordinates for the analysis are taken to be the displacements of the ends of the "beams", $U_i^{l(1)}$, $U_i^{l(2)}$, $U_i^{r(1)}$, $U_i^{r(2)}$, (see Figure 2-2) the "branch beam" angular displacements, $\beta_i^{(1)}$, $\beta_i^{(2)}$, and the coefficients, $\lambda_{ij}^{(1)}$, $\lambda_{ij}^{(2)}$, of the corresponding displacement functions $Y_{ij}^{(1)}(x)$ and $Y_{ij}^{(2)}(x)$.

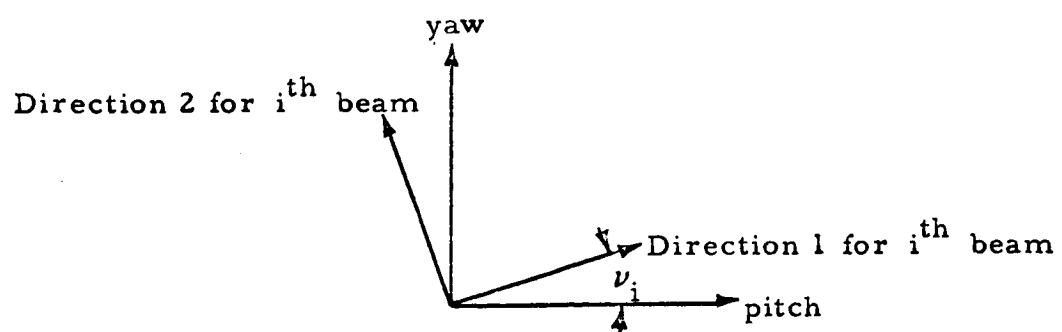
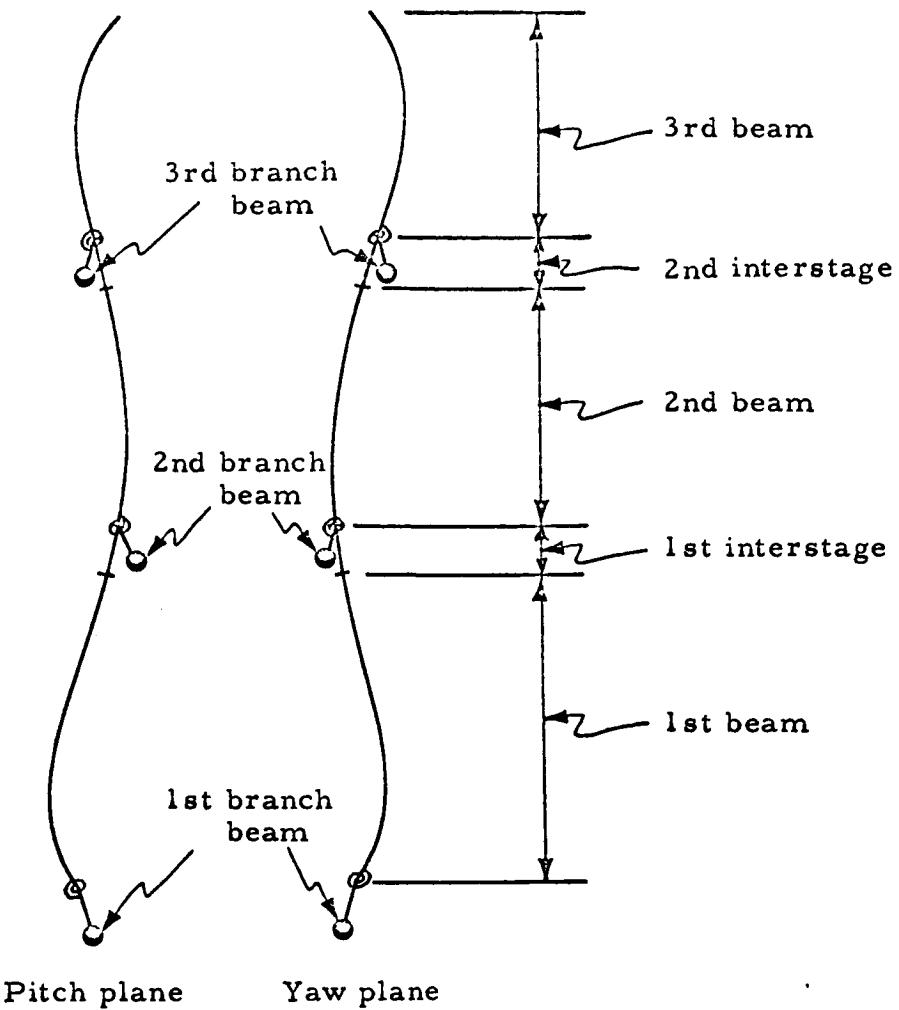
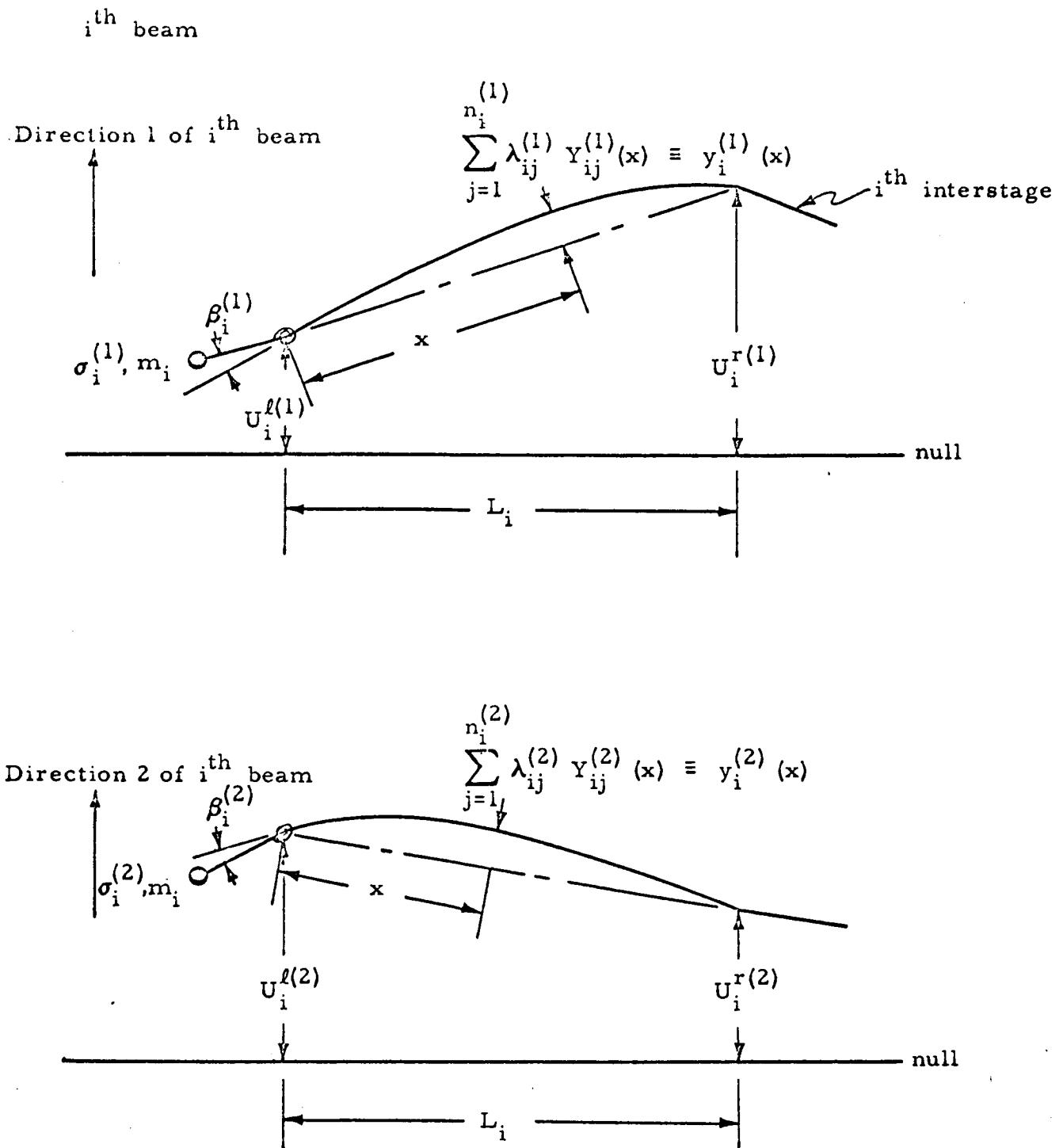


Figure 2-1 - Model Configuration

Figure 2-2 - Coordinates Associated with the i^{th} Beam

The subscripts i and j represent the i^{th} beam and the j^{th} deflection function for that beam. Superscripts l and r are used to denote the left and right ends of a beam respectively. Superscripts p and y indicate the two reference directions of the system, pitch and yaw.

2.3 Equations of Motion

For undamped, free vibrations, Lagrange's equation of motion reduces to

$$\frac{d}{dt} \left(\frac{\partial T}{\partial \dot{q}_i} \right) + \frac{\partial V}{\partial q_i} = 0 \quad i = 1, 2, \dots, n \quad (1)$$

where T and V are the kinetic and potential energies of the system, respectively and (q_1, q_2, \dots, q_n) are the generalized coordinates of the system.

The quantities T and V may be expressed as quadratic forms in the generalized coordinates, e. g.,

$$\begin{aligned} 2T &= \dot{Q}^t A \dot{Q} && \text{and} \\ 2V &= Q^t B Q \end{aligned} \quad (2)$$

where

$$Q = \begin{Bmatrix} q_1 \\ q_2 \\ \vdots \\ q_n \end{Bmatrix}$$

and A and B are kinetic and potential energy coefficient matrices, termed the "mass" matrix and "stiffness" matrix, respectively.

Equation (1) may now be written as

$$A \ddot{Q} + B Q = 0. \quad (3)$$

Assuming solutions of Equation (3) of the form

$$Q = X \sin \omega t$$

we get

$$\omega^2 A X - B X = 0. \quad (4)$$

The method of solution employed by the computer program to solve for the eigenvalues, ω^2 , and eigenvectors, X , of Equation (4) is discussed in Section 3.1.1.

2.4 Energy Terms

The kinetic and potential energy terms associated with the various components of the mathematical model are discussed below.

2.4.1 Beams

In deriving the kinetic and potential energy expressions for beam bending, a Timoshenko beam model is used, i.e., strain energy due to shear deformation is included in the analysis, as well as kinetic energy due to rotatory inertia. For tank properties involved in the Saturn V class of vehicles, the strain energy due to shear is quite significant, and the effect of including rotatory inertia is significant in the second and higher modes.

Kinetic Energy

The displacement of the i^{th} beam in the t^{th} principal direction, $\Delta_i^t(x)$, is:

$$\Delta_i^t(x) = U_i^{lt} + \frac{U_i^{rt} - U_i^{lt}}{L_i} x + \sum_{j=1}^{n_i^t} \lambda_{ij}^t Y_{ij}^t(x) \quad (5)$$

where L_i is the length of the i^{th} beam,

Y_{ij}^t is the j^{th} deflection function in the t^{th} principal direction for the i^{th} beam, and

n_i^t is the number of deflection functions used in the t^{th} principal direction for the i^{th} beam.

The kinetic energy associated with the t^{th} principal direction of the i^{th} beam, T_i^{bt} , may now be written as

$$\begin{aligned} T_i^{bt} = & \frac{1}{2} \int_0^{L_i} \left\{ \mu_i(x) \left[\dot{U}_i^{lt} + \frac{\dot{U}_i^{rt} - \dot{U}_i^{lt}}{L_i} x + \sum_{j=1}^{n_i^t} \dot{\lambda}_{ij}^t Y_{ij}^t(x) \right]^2 \right. \\ & \left. + I_i^t(x) \left[\frac{\dot{U}_i^{rt} - \dot{U}_i^{lt}}{L_i} + \sum_{j=1}^{n_i^t} \dot{\lambda}_{ij}^t Z_{ij}^t(x) \right]^2 \right\} dx \end{aligned} \quad (6)$$

where

μ_i is the mass per unit length of the i^{th} beam,

I_i^t is the mass moment of inertia per unit length for the t^{th} principal direction of the i^{th} beam, and

Z_{ij}^t is the cross-section rotation associated with the j^{th} displacement function for the t^{th} direction of the i^{th} beam.

Equation (6) may be written in the form

$$\begin{aligned}
 2 T_i^{bt} = & \left(\dot{U}_i^{lt} \right)^2 \int_0^{L_i} \mu_i(x) dx \\
 & + \left(\frac{\dot{U}_i^{rt} - \dot{U}_i^{lt}}{L_i} \right)^2 \int_0^{L_i} \left[x^2 \mu_i(x) + I_i^t(x) \right] dx \\
 & + 2 \left(\dot{U}_i^{lt} \right) \left(\frac{\dot{U}_i^{rt} - \dot{U}_i^{lt}}{L_i} \right) \int_0^{L_i} x \mu_i(x) dx \\
 & + \int_0^{L_i} \mu_i(x) \left[\sum_{j=1}^{n_i^t} \lambda_{ij}^t Y_{ij}^t(x) \right]^2 dx \\
 & + \int_0^{L_i} I_i^t(x) \left[\sum_{j=1}^{n_i^t} \lambda_{ij}^t Z_{ij}^t(x) \right]^2 dx \\
 & + 2 \dot{U}_i^{lt} \sum_{j=1}^{n_i^t} \lambda_{ij}^t \int_0^{L_i} \mu_i(x) Y_{ij}^t(x) dx \\
 & + 2 \left(\frac{\dot{U}_i^{rt} - \dot{U}_i^{lt}}{L_i} \right) \sum_{j=1}^{n_i^t} \lambda_{ij}^t \int_0^{L_i} x \mu_i(x) Y_{ij}^t(x) dx \\
 & + 2 \left(\frac{\dot{U}_i^{rt} - \dot{U}_i^{lt}}{L_i} \right) \sum_{j=1}^{n_i^t} \lambda_{ij}^t \int_0^{L_i} I_i^t(x) Z_{ij}^t(x) dx . \tag{7}
 \end{aligned}$$

The two terms of Equation (7) involving the square of a summation may be expressed as double sums, i.e.,

$$\int_0^{L_i} \mu_i(x) \left[\sum_{j=1}^{n_i^t} \lambda_{ij}^t Y_{ij}^t(x) \right]^2 dx = \sum_{j=1}^{n_i^t} \sum_{k=1}^{n_i^t} \lambda_{ij}^t \lambda_{ik}^t \int_0^{L_i} \mu_i(x) Y_{ij}^t(x) Y_{ik}^t(x) dx$$

$$\int_0^{L_i} I_i^t(x) \left[\sum_{j=1}^{n_i^t} \lambda_{ij}^t Z_{ij}^t(x) \right]^2 dx = \sum_{j=1}^{n_i^t} \sum_{k=1}^{n_i^t} \lambda_{ij}^t \lambda_{ik}^t \int_0^{L_i} I_i(x) Z_{ij}^t(x) Z_{ik}^t(x) dx$$

Making the following definitions

$$\int_0^{L_i} \mu_i(x) dx \equiv M_i$$

$$\int_0^{L_i} x \mu_i(x) dx \equiv J_i$$

$$\int_0^{L_i} [x^2 \mu_i(x) + I_i^t(x)] dx \equiv R_i^t$$

(8)

$$\int_0^{L_i} \mu_i(x) Y_{ij}^t(x) dx \equiv \gamma_{ij}^t$$

$$\int_0^{L_i} [x \mu_i(x) Y_{ij}^t(x) + I_i^t(x) Z_{ij}^t(x)] dx \equiv \Omega_{ij}^t$$

$$\int_0^{L_i} [\mu_i(x) Y_{ij}^t(x) Y_{ik}^t(x) + I_i^t(x) Z_{ij}^t(x) Z_{ik}^t(x)] dx \equiv \psi_{ijk}^t$$

equation (7) may be written in terms of the generalized coordinates.

$$\begin{aligned}
 2 T_i^{bt} = & \left(\dot{U}_i^{lt} \right)^2 \left[M_i + \left(\frac{1}{L_i} \right)^2 R_i^t - \left(\frac{2}{L_i} \right) J_i^t \right] \\
 & + \left(\dot{U}_i^{rt} \right)^2 \left[\left(\frac{1}{L_i} \right)^2 R_i^t \right] \\
 & + \left(\dot{U}_i^{lt} \dot{U}_i^{rt} \right) \left[-2 \left(\frac{1}{L_i} \right)^2 R_i^t + \left(\frac{2}{L_i} \right) J_i^t \right] \\
 & + 2 \dot{U}_i^{lt} \sum_{j=1}^{n_i^t} \dot{\lambda}_{ij}^t \left[\gamma_{ij}^t - \left(\frac{1}{L_i} \right) \Omega_{ij}^t \right] \\
 & + 2 \dot{U}_i^{rt} \sum_{j=1}^{n_i^t} \dot{\lambda}_{ij}^t \left[\left(\frac{1}{L_i} \right) \Omega_{ij}^t \right] \\
 & + \sum_{j=1}^{n_i^t} \sum_{k=1}^{n_i^t} \dot{\lambda}_{ij}^t \dot{\lambda}_{ik}^t \psi_{ijk}^t
 \end{aligned} \tag{9}$$

The total kinetic energy associated with the i^{th} beam, T_i^b , may be written as

$$T_i^b = T_i^{b1} + T_i^{b2}. \tag{10}$$

Potential Energy

The potential energy of the i^{th} beam in the t^{th} principal direction, V_i^{bt} , may be expressed as

$$V_i^{\text{bt}} = \frac{1}{2} \int_0^{L_i} \left[EI_i^t(x) \left\{ \sum_{j=1}^{n_i^t} \lambda_{ij}^t [z_{ij}^t(x)]' \right\}^2 + GA_i^t(x) \left\{ \sum_{j=1}^{n_i^t} \lambda_{ij}^t H_{ij}^t(x) \right\}^2 \right] dx \quad (11)$$

where

EI_i^t is the bending stiffness distribution for the t^{th} principal direction of the i^{th} beam,

GA_i^t is the shear stiffness distribution for the t^{th} principal direction of the i^{th} beam, and

H_{ij}^t is the shear slope associated with the j^{th} displacement function for the t^{th} direction of the i^{th} beam.

Expanding and interchanging the order of summation and integration in Equation (11) yields

$$V_i^{\text{bt}} = \frac{1}{2} \sum_{j=1}^{n_i^t} \sum_{k=1}^{n_i^t} \lambda_{ij}^t \lambda_{ik}^t \int_0^{L_i} \left\{ EI_i^t(x) [Z_{ij}^t(x)]' [Z_{ik}^t(x)]' + GA_i^t(x) H_{ij}^t(x) H_{ik}^t(x) \right\} dx. \quad (12)$$

Making the definition

$$G_{ijk}^t = \int_0^{L_i} \left\{ EI_i^t(x) [Z_{ij}^t(x)]' [Z_{ik}^t(x)]' + GA_i^t(x) H_{ij}^t(x) H_{ik}^t(x) \right\} dx \quad (13)$$

equation (12) may be written as

$$V_i^{bt} = \frac{1}{2} \sum_{j=1}^{n_i^t} \sum_{k=1}^{n_j^t} \lambda_{ij}^t \lambda_{ik}^t G_{ijk}^t . \quad (14)$$

The total potential energy of the i^{th} beam due to bending, V_i^b , may be written as

$$V_i^b = V_i^{b1} + V_i^{b2} . \quad (15)$$

2.4.2 Interstages

An interstage in the idealized model may be either of two types:

- a. Zero-length interstage
- b. Non-zero length interstage

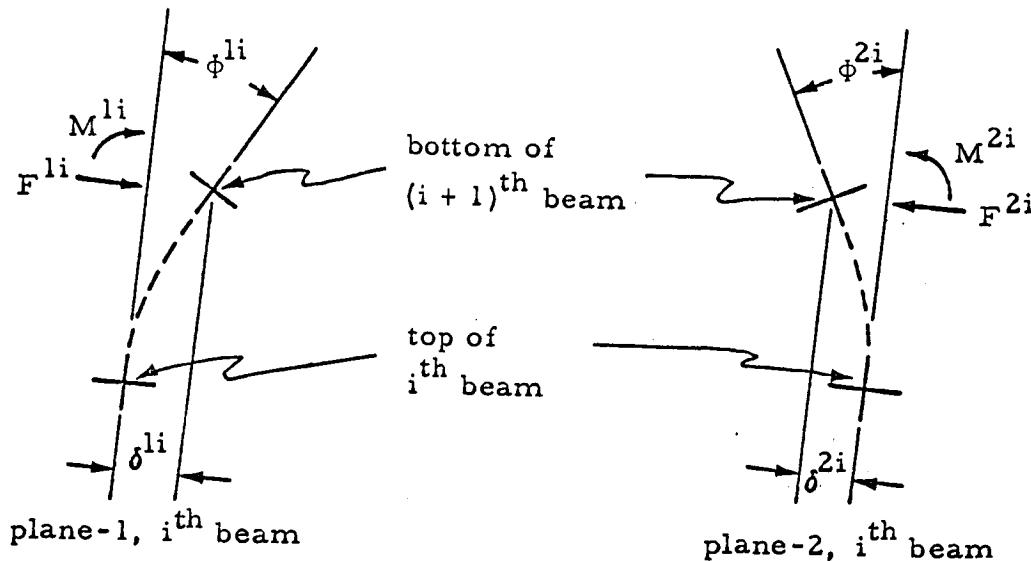
Most of the following discussion is directed toward the interstages of type-b. However, the resulting matrix equations representing the interstage strain energy are of the same form for either case.

Kinetic Energy

The interstages of type-a have no kinetic energy associated with their displacements due to the nature of that class of interstage.

The type-b interstages are assumed to be very light compared with the weights of other parts of the vehicle in the same neighborhood (engines, bulkheads, etc.) The engines are represented by branch beams and bulkhead, and other associated tank masses are included in the beams. So there are no kinetic energy terms for the interstage itself, rather the interstage mass is lumped at the ends of the adjacent beams in appropriate proportions.

The strain energy associated with the i^{th} "interstage" (type b), V_i^s , is derived as follows:



M^1, M^2, F^1, F^2 are the moments and forces exerted on the top of the interstage by the bottom of the $(i+1)^{\text{th}}$ beam.

The flexibility properties of the interstage are represented by:

$$\begin{bmatrix} M^{li} \\ F^{li} \\ M^{2i} \\ F^{2i} \end{bmatrix} = \begin{bmatrix} k_{11}^{lli} & k_{12}^{lli} & k_{11}^{l2i} & k_{12}^{l2i} \\ k_{12}^{lli} & k_{22}^{lli} & k_{21}^{l2i} & k_{22}^{l2i} \\ \hline & \text{Symmetric} & k_{11}^{22i} & k_{12}^{22i} \\ & & k_{12}^{22i} & k_{22}^{22i} \end{bmatrix} \begin{bmatrix} \phi^{li} \\ \delta^{li} \\ \phi^{2i} \\ \delta^{2i} \end{bmatrix} \quad (16)$$

The strain energy associated with the i^{th} interstage may then be written as

$$V_i^s = [\phi]_i^t [K]_i [\phi]_i, \quad \text{where } \phi_i \equiv \begin{bmatrix} \phi^{li} \\ \delta^{li} \\ \phi^{2i} \\ \delta^{2i} \end{bmatrix}. \quad (17)$$

and where K_i is the stiffness matrix of Equation (16).

It is convenient to represent the strain energy associated with an interstage in terms of a set of angular displacements, α .

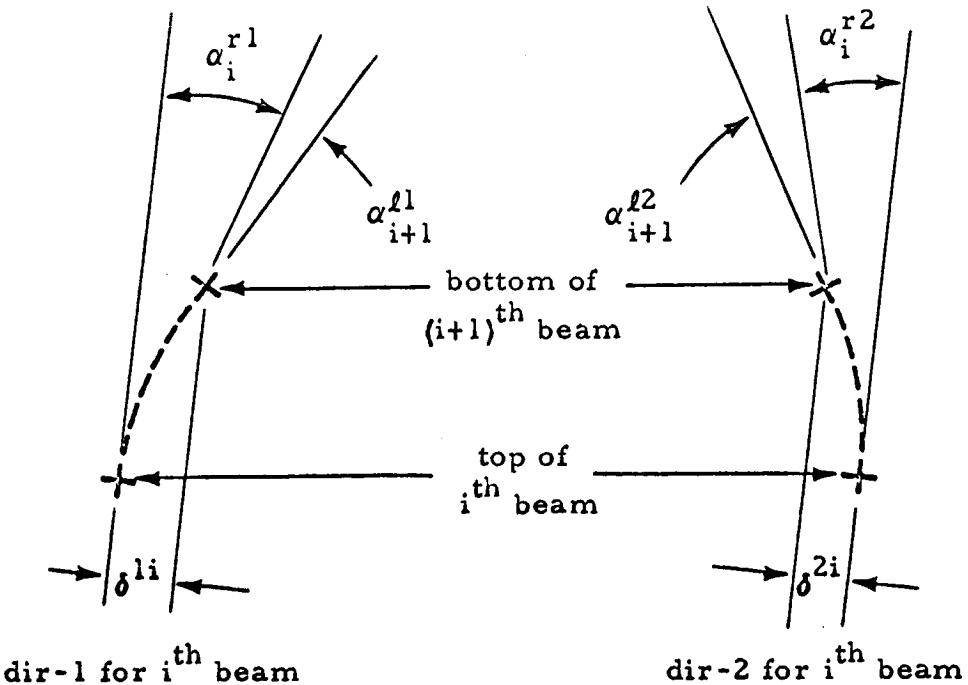


Figure 2-3

From Figure 2-3 it is easily seen that

$$\begin{aligned}\phi^{li} &= \alpha_i^{rl} + \alpha_{i+1}^{ll}, \text{ and} \\ \delta^{li} &= l \alpha_i^{rl}\end{aligned}\tag{18}$$

where l is the length of the interstage.

Writing Equations (18) in matrix form for the i^{th} interstage

$$\begin{bmatrix} \phi^{1i} \\ \delta^{1i} \\ \phi^{2i} \\ \delta^{2i} \end{bmatrix} = \begin{bmatrix} 1 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 1 \\ 0 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} \alpha_i^{r1} \\ \alpha_{i+1}^{rl} \\ \alpha_i^{r2} \\ \alpha_{i+1}^{l2} \end{bmatrix} \quad (19)$$

or

$$[\phi]_i = [T]_i [\alpha]_i \quad (20)$$

where $[T]_i$ is the transformation matrix of Equation (19).

We may now write the expression for the strain energy associated with the i^{th} interstage as

$$V_i^s = [\alpha]_i^t [T]_i^t [K]_i [T]_i [\alpha]_i. \quad (21)$$

Hence from Equation (21) we may define a new stiffness matrix, \tilde{K} ,

$$[\tilde{K}]_i = [T]_i^t [K]_i [T]_i \quad (22)$$

so that

$$V_i^s = [\alpha]_i^t [\tilde{K}]_i [\alpha]_i. \quad (23)$$

For a type-b interstage, the α 's may be expressed in terms of the generalized coordinates as follows:

$$\begin{aligned}
 \alpha_i^{r1} &= \Theta_{i1} - \sum_{j=1}^{n_i^{(1)}} \lambda_{ij}^{(1)} \left[Z_{ij}^{(1)}(x) \right]_{x=L_i} + \Theta_{i3} \\
 \alpha_i^{r2} &= \Theta_{i2} - \sum_{j=1}^{n_i^{(2)}} \lambda_{ij}^{(2)} \left[Z_{ij}^{(2)}(x) \right]_{x=L_i} + \Theta_{i4} \\
 \alpha_{i+1}^{\ell 1} &= -\Theta_{i3} - \Theta_{i5} + \cos \bar{\nu}_i \sum_{j=1}^{n_{i+1}^{(1)}} \lambda_{i+1,j}^{(1)} \left[Z_{i+1,j}^{(1)}(x) \right]_{x=0} \\
 &\quad + \sin \bar{\nu}_i \sum_{j=1}^{n_{i+1}^{(2)}} \lambda_{i+1,j}^{(2)} \left[Z_{i+1,j}^{(2)}(x) \right]_{x=0} \\
 \alpha_{i+1}^{\ell 2} &= -\Theta_{i4} - \Theta_{i6} - \sin \bar{\nu}_i \sum_{j=1}^{n_{i+1}^{(1)}} \lambda_{i+1,j}^{(1)} \left[Z_{i+1,j}^{(1)}(x) \right]_{x=0} \\
 &\quad + \cos \bar{\nu}_i \sum_{j=1}^{n_{i+1}^{(2)}} \lambda_{i+1,j}^{(2)} \left[Z_{i+1,j}^{(2)}(x) \right]_{x=0}
 \end{aligned} \tag{24}$$

where

$$\begin{aligned}
 \Theta_{i1} &= \frac{1}{L_i} \left(U_i^{\ell 1} - U_i^{r 1} \right) \\
 \Theta_{i2} &= \frac{1}{L_i} \left(U_i^{\ell 2} - U_i^{r 2} \right) \\
 \Theta_{i3} &= \frac{1}{\ell_i} \left(U_{i+1}^{\ell 1} \cos \bar{\nu}_i + U_{i+1}^{\ell 2} \sin \bar{\nu}_i - U_i^{r 1} \right) \\
 \Theta_{i4} &= \frac{1}{\ell_i} \left(-U_{i+1}^{\ell 1} \sin \bar{\nu}_i + U_{i+1}^{\ell 2} \cos \bar{\nu}_i - U_i^{r 2} \right) \\
 \Theta_{i5} &= \frac{1}{L_{i+1}} \left(U_{i+1}^{\ell 1} \cos \bar{\nu}_i + U_{i+1}^{\ell 2} \sin \bar{\nu}_i - U_{i+1}^{r 1} \cos \bar{\nu}_i - U_{i+1}^{r 2} \sin \bar{\nu}_i \right) \\
 \Theta_{i6} &= \frac{1}{L_{i+1}} \left(-U_{i+1}^{\ell 1} \sin \bar{\nu}_i + U_{i+1}^{\ell 2} \cos \bar{\nu}_i + U_{i+1}^{r 1} \sin \bar{\nu}_i - U_{i+1}^{r 2} \cos \bar{\nu}_i \right)
 \end{aligned} \tag{25}$$

and

$$\bar{\nu}_i = \nu_i - \nu_{i+1},$$

the angle between the principal axes of the i^{th} beam and the principal axes of the $(i+1)^{\text{th}}$ beam.

Substituting for the Θ 's and collecting terms we get

$$\alpha_i^{r1} = \frac{1}{L_i} U_i^{\ell 1} - \left(\frac{1}{L_i} + \frac{1}{\ell_i} \right) U_i^{r1} + \frac{1}{\ell_i} \left[U_{i+1}^{\ell 1} \cos \bar{\nu}_i + U_{i+1}^{\ell 2} \sin \bar{\nu}_i \right] - \sum_{j=1}^{n_i^{(1)}} \lambda_{ij}^{(1)} \left[Z_{ij}^{(1)}(x) \right]_{x=L_i}$$

$$\alpha_i^{r2} = \frac{1}{L_i} U_i^{\ell 2} - \left(\frac{1}{L_i} + \frac{1}{\ell_i} \right) U_i^{r2} + \frac{1}{\ell_i} \left[-U_{i+1}^{\ell 1} \sin \bar{\nu}_i + U_{i+1}^{\ell 2} \cos \bar{\nu}_i \right] - \sum_{j=1}^{n_i^{(2)}} \lambda_{ij}^{(2)} \left[Z_{ik}^{(2)}(x) \right]_{x=L_i}$$

$$\alpha_{i+1}^{\ell 1} = \frac{1}{\ell_i} U_i^{r1} - \left(\frac{1}{\ell_i} + \frac{1}{L_{i+1}} \right) \left[U_{i+1}^{\ell 1} \cos \bar{\nu}_i + U_{i+1}^{\ell 2} \sin \bar{\nu}_i \right] + \frac{1}{L_{i+1}} \left[U_{i+1}^{r1} \cos \bar{\nu}_i + U_{i+1}^{r2} \sin \bar{\nu}_i \right]$$

$$+ \cos \bar{\nu}_i \sum_{j=1}^{n_{i+1}^{(1)}} \lambda_{i+1,j}^{(1)} \left[Z_{i+1,j}^{(1)}(x) \right]_{x=0} + \sin \bar{\nu}_i \sum_{j=1}^{n_{i+1}^{(2)}} \lambda_{i+1,j}^{(2)} \left[Z_{i+1,j}^{(2)}(x) \right]_{x=0} \quad (26)$$

$$\alpha_{i+1}^{\ell 2} = \frac{1}{\ell_i} U_i^{r2} - \left(\frac{1}{\ell_i} + \frac{1}{L_{i+1}} \right) \left[-U_{i+1}^{\ell 1} \sin \bar{\nu}_i + U_{i+1}^{\ell 2} \cos \bar{\nu}_i \right] + \frac{1}{L_{i+1}} \left[-U_{i+1}^{r1} \sin \bar{\nu}_i + U_{i+1}^{r2} \cos \bar{\nu}_i \right]$$

$$- \sin \bar{\nu}_i \sum_{j=1}^{n_{i+1}^{(1)}} \lambda_{i+1,j}^{(1)} \left[Z_{i+1,j}^{(1)}(x) \right]_{x=0} + \cos \bar{\nu}_i \sum_{j=1}^{n_{i+1}^{(2)}} \lambda_{i+1,j}^{(2)} \left[Z_{i+1,j}^{(2)}(x) \right]_{x=0}$$

For an interstage of type a, the flexibility properties of the interstage are represented by a 2×2 matrix. The strain energy is still expressed by Equation (23) where the stiffness matrix $[\tilde{K}]_i$ for the i^{th} interstage is composed of the spring constants for the two principle directions of the i^{th} beam (there may be coupling between these two directions) and the components of the displacement vector $[\alpha]_i$ are defined below:

$$\begin{aligned}
 \alpha_i^{r1} &= \Theta_{i1} - \sum_{j=1}^{n_i^{(1)}} \lambda_{ij}^{(1)} \left[Z_{ij}^{(1)}(x) \right]_{x=L_i} - \Theta_{i5} + \cos \bar{\nu}_i \sum_{j=1}^{n_{i+1}^{(1)}} \lambda_{i+1,j}^{(1)} \left[Z_{i+1,j}^{(1)}(x) \right]_{x=0} \\
 &\quad + \sin \bar{\nu}_i \sum_{j=1}^{n_{i+1}^{(2)}} \lambda_{i+1,j}^{(2)} \left[Z_{i+1,j}^{(2)}(x) \right]_{x=0} \\
 \alpha_i^{r2} &= \Theta_{i2} - \sum_{j=1}^{n_i^{(2)}} \lambda_{ij}^{(2)} \left[Z_{ij}^{(2)}(x) \right]_{x=L_i} - \Theta_{i6} - \sin \nu_i \sum_{j=1}^{n_{i+1}^{(1)}} \lambda_{i+1,j}^{(1)} \left[Z_{i+1,j}^{(1)}(x) \right]_{x=0} \\
 &\quad + \cos \bar{\nu}_i \sum_{j=1}^{n_{i+1}^{(2)}} \lambda_{i+1,j}^{(2)} \left[Z_{i+1,j}^{(2)}(x) \right]_{x=0}
 \end{aligned} \tag{27}$$

Substituting for the Θ 's yields

$$\begin{aligned}
 \alpha_i^{r1} &= \frac{1}{L_i} (U_i^{\ell 1} - U_i^{r1}) + \frac{1}{L_{i+1}} (U_{i+1}^{r1} \cos \bar{\nu}_i + U_{i+1}^{r2} \sin \bar{\nu}_i - U_{i+1}^{\ell 1} \cos \bar{\nu}_i - U_{i+1}^{\ell 2} \sin \bar{\nu}_i) \\
 &\quad - \sum_{j=1}^{n_i^{(1)}} \lambda_{ij}^{(1)} \left[Z_{ij}^{(1)}(x) \right]_{x=L_i} + \cos \bar{\nu}_i \sum_{j=1}^{n_{i+1}^{(1)}} \lambda_{i+1,j}^{(1)} \left[Z_{i+1,j}^{(1)}(x) \right]_{x=0} + \sin \bar{\nu}_i \sum_{j=1}^{n_{i+1}^{(2)}} \lambda_{i+1,j}^{(2)} \left[Z_{i+1,j}^{(2)}(x) \right]_{x=0} \\
 \alpha_i^{r2} &= \frac{1}{L_i} (U_i^{\ell 2} - U_i^{r2}) + \frac{1}{L_{i+1}} (-U_{i+1}^{r1} \sin \bar{\nu}_i + U_{i+1}^{r2} \cos \bar{\nu}_i + U_{i+1}^{\ell 1} \sin \bar{\nu}_i - U_{i+1}^{\ell 2} \cos \bar{\nu}_i) \\
 &\quad - \sum_{j=1}^{n_i^{(2)}} \lambda_{ij}^{(2)} \left[Z_{ij}^{(2)}(x) \right]_{x=L_i} - \sin \bar{\nu}_i \sum_{j=1}^{n_{i+1}^{(1)}} \lambda_{i+1,j}^{(1)} \left[Z_{i+1,j}^{(1)}(x) \right]_{x=0} + \cos \bar{\nu}_i \sum_{j=1}^{n_{i+1}^{(2)}} \lambda_{i+1,j}^{(2)} \left[Z_{i+1,j}^{(2)}(x) \right]_{x=0}
 \end{aligned} \tag{28}$$

For either type of interstage the vector of angular displacements, $[\alpha]$, may be written in terms of the generalized coordinate vector $[Q]$,

$$[\alpha] = [C] [Q] \tag{29}$$

where $[C]$ is the matrix of coefficients defined by Equation (28) (for a type-a interstage) or by Equation (26) (for a type-b interstage). Therefore, the expression

$$v = [\alpha]^t [\tilde{K}] [\alpha]$$

may be written as

$$v = [Q]^t [C]^t [\tilde{K}] [C] [Q]. \tag{30}$$

Hence, the potential energy coefficient matrix for the interstage spring system, $[\bar{B}]$, is

$$[\bar{B}] = [C]^t [\tilde{K}] [C]. \tag{31}$$

2.4.3 Branch Beams

Kinetic Energy

The kinetic energy expression for the i^{th} branch beam in the t^{th} principal direction of the i^{th} beam may be written as

$$T_i^{mt} = \frac{1}{2} m_i \left\{ \dot{U}_i^{lt} - d_i [\dot{S}_{ij}^t] \right\}^2 + \frac{1}{2} \sigma_i^t [\dot{S}_{ij}^t]^2 \quad (32)$$

where .

$$\dot{S}_{ij}^t = \frac{1}{L_i} (\dot{U}_i^{rt} - \dot{U}_i^{lt}) + \sum_{j=1}^{n_i^t} \lambda_{ij}^t [z_{ij}^t(x)]_{x=0} - \dot{\beta}_i^t$$

and m_i is the effective mass of the i^{th} branch beam,
 d_i is the effective length of the i^{th} branch beam,
 σ_i is the effective mass moment of inertia of the
 i^{th} branch beam.

Substituting for S yields

$$\begin{aligned} T_i^{mt} &= \frac{1}{2} m_i \left[\left(\dot{U}_i^{lt} \right)^2 \right. \\ &+ \left(d_i^2 + \frac{\sigma_i^t}{m_i} \right) \left\{ \frac{1}{L_i} (\dot{U}_i^{rt} - \dot{U}_i^{lt}) + \sum_{j=1}^{n_i^t} \lambda_{ij}^t [z_{ij}^t(x)]_{x=0} - \dot{\beta}_i^t \right\}^2 \\ &\left. - 2 \dot{U}_i^{lt} d_i \left\{ \frac{1}{L_i} (\dot{U}_i^{rt} - \dot{U}_i^{lt}) + \sum_{j=1}^{n_i^t} \lambda_{ij}^t [z_{ij}^t(x)]_{x=0} - \dot{\beta}_i^t \right\} \right] \end{aligned} \quad (33)$$

which may be written as

$$\begin{aligned}
2 T_i^{mt} = & \left(\dot{U}_i^{lt} \right)^2 \left[m_i + \left(\frac{1}{L_i} \right)^2 \left(m_i d_i^2 + \sigma_i^t \right) + \frac{2 m_i d_i}{L_i} \right] \\
& + \left(\dot{U}_i^{rt} \right)^2 \left[\left(\frac{1}{L_i} \right)^2 \left(m_i d_i^2 + \sigma_i^t \right) \right] \\
& - 2 \left(\dot{U}_i^{lt} \dot{U}_i^{rt} \right) \left[\left(\frac{1}{L_i} \right)^2 \left(m_i d_i^2 + \sigma_i^t \right) + \frac{m_i d_i}{L_i} \right] \\
& + \left(\dot{\beta}_i^t \right)^2 \left[m_i d_i^2 + \sigma_i^t \right] \\
& + 2 \left(\dot{U}_i^{lt} \dot{\beta}_i^t \right) \left[\left(\frac{1}{L_i} \right) \left(m_i d_i^2 + \sigma_i^t \right) + m_i d_i \right] \\
& + 2 \left(\dot{U}_i^{rt} \dot{\beta}_i^t \right) \left[- \left(\frac{1}{L_i} \right) \left(m_i d_i^2 + \sigma_i^t \right) \right] \\
& + \left\{ \sum_{j=1}^{n_i^t} \sum_{k=1}^{n_i^t} \dot{\lambda}_{ij}^t \dot{\lambda}_{ik}^t \left[Z_{ij}^t(x) \right]_{x=0} \left[Z_{ik}^t(x) \right]_{x=0} \right\} \left(m_i d_i^2 + \sigma_i^t \right) \\
& - 2 \left\{ \dot{U}_i^{lt} \sum_{j=1}^{n_i^t} \dot{\lambda}_{ij}^t \left[Z_{ij}^t(x) \right]_{x=0} \right\} \left[\left(\frac{1}{L_i} \right) \left(m_i d_i^2 + \sigma_i^t \right) + m_i d_i \right] \\
& + 2 \left\{ \dot{U}_i^{rt} \sum_{j=1}^{n_i^t} \dot{\lambda}_{ij}^t \left[Z_{ij}^t(x) \right]_{x=0} \right\} \left[\left(\frac{1}{L_i} \right) \left(m_i d_i^2 + \sigma_i^t \right) \right] \\
& - 2 \left\{ \dot{\beta}_i^t \sum_{j=1}^{n_i^t} \dot{\lambda}_{ij}^t \left[Z_{ij}^t(x) \right]_{x=0} \right\} \left[m_i d_i^2 + \sigma_i^t \right]. \tag{34}
\end{aligned}$$

The total kinetic energy associated with the i^{th} branch beam may be written as

$$T_i^m = T_i^{m1} + T_i^{m2}. \quad (35)$$

Potential Energy

The potential energy associated with the branch displacements may be written as

$$V_i^m = [\beta]_i^t [K_b]_i [\beta]_i \quad (36)$$

where

$$[\beta]_i = \begin{bmatrix} \beta_i^{(1)} \\ \beta_i^{(2)} \end{bmatrix}, \quad \text{and} \quad [K_b]_i = \begin{bmatrix} k_{bi}^{11} & k_{bi}^{12} \\ k_{bi}^{12} & k_{bi}^{22} \end{bmatrix}$$

the branch beam displacement vector and stiffness matrix respectively.

2.4.4 External Support Springs

External support springs, which may be placed at the beam ends, are of two types:

- a. lateral
- b. rotational

The strain energy associated with each is discussed below.

The strain energy associated with the lateral support springs for the i^{th} beam may be expressed as

$$V_i^{ls} = [U_{ls}]_i^t [K_{ls}]_i [U_{ls}]_i \quad (37)$$

where

$$[U_{ls}]_i = \begin{bmatrix} U_i^{\ell 1} \\ U_i^{r1} \\ U_i^{\ell 2} \\ U_i^{r2} \end{bmatrix}, \text{ and } [K_{ls}]_i = \begin{bmatrix} k_{\ell s i}^{\ell 1} & 0 & 0 & 0 \\ 0 & k_{\ell s i}^{r1} & 0 & 0 \\ 0 & 0 & k_{\ell s i}^{\ell 2} & 0 \\ 0 & 0 & 0 & k_{\ell s i}^{r2} \end{bmatrix}.$$

The strain energy associated with the rotational support springs for the i^{th} beam may be expressed as

$$V_i^{rs} = [U_{rs}]_i^t [K_{rs}]_i [U_{rs}]_i \quad (38)$$

where

$$[U_{rs}]_i = \begin{bmatrix} \tilde{\theta}_i^{\ell 1} \\ \tilde{\theta}_i^{r1} \\ \tilde{\theta}_i^{\ell 2} \\ \tilde{\theta}_i^{r2} \end{bmatrix}, \text{ and } [K_{rs}]_i = \begin{bmatrix} k_{rs i}^{\ell 1} & 0 & 0 & 0 \\ 0 & k_{rs i}^{r1} & 0 & 0 \\ 0 & 0 & k_{rs i}^{\ell 2} & 0 \\ 0 & 0 & 0 & k_{rs i}^{r2} \end{bmatrix}.$$

The $\tilde{\theta}_i$'s are defined in terms of the generalized coordinates as follows:

$$\begin{aligned}
 \tilde{\theta}_i^{\ell 1} &= \frac{U_i^{r1} - U_i^{\ell 1}}{L_i} + \sum_{j=1}^{n_i^{(1)}} \lambda_{ij}^{(1)} \left[Z_{ij}^{(1)}(x) \right]_{x=0} \\
 \tilde{\theta}_i^{r1} &= \frac{U_i^{r1} - U_i^{\ell 1}}{L_i} + \sum_{j=1}^{n_i^{(1)}} \lambda_{ij}^{(1)} \left[Z_{ij}^{(1)}(x) \right]_{x=L_i} \\
 \tilde{\theta}_i^{\ell 2} &= \frac{U_i^{r2} - U_i^{\ell 2}}{L_i} + \sum_{j=1}^{n_i^{(2)}} \lambda_{ij}^{(2)} \left[Z_{ij}^{(2)}(x) \right]_{x=0} \\
 \tilde{\theta}_i^{r2} &= \frac{U_i^{r2} - U_i^{\ell 2}}{L_i} + \sum_{j=1}^{n_i^{(2)}} \lambda_{ij}^{(2)} \left[Z_{ij}^{(2)}(x) \right]_{x=L_i}
 \end{aligned} \tag{39}$$

The total potential energy due to support springs for the i^{th} beam, V_i^{ss} , may be written as

$$V_i^{\text{ss}} = V_i^{\ell s} + V_i^{rs}. \tag{40}$$

The total kinetic energy for the system may now be written as

$$T = \sum_{i=1}^N (T_i^b + T_i^m) \tag{41}$$

where N is the number of beams in the system.

The total potential energy for the system may similarly be written as

$$V = \sum_{i=1}^N (V_i^b + V_i^s + V_i^m + V_i^{\text{ss}}). \tag{42}$$

From T and V the coefficient matrices A and B may be constructed.

Section 3 COMPUTER PROGRAM

3.1 General Features

A digital computer program has been developed implementing the solution method described in the preceding section. The program is coded in FORTRAN IV and configured for execution on the IBM 7094 computer with 32 K core storage capacity. Only minor modifications would be necessary to configure the program for execution on another computer equipped with a FORTRAN IV compiler.

Due to the storage limitation of the present computer the present version of the program restricts the beam properties to be identical in two directions. By changing a few cards in the program, different properties may be allowed in each direction, at the expense of limiting program "size" in other aspects. This program version solves up to a 60 degree-of-freedom system obtaining all 60 eigenvalues and eigenvectors in from 2 to 5 minutes of execution time, depending on the amount of printed and plotted output requested.

3.1.1 Method of Eigenproblem Solution

The solution of the $\omega^2 A X - B X = 0$ problem is acquired by transforming the equation into the standard eigenvalue problem $(F - \lambda I) Y = 0$, solving for the eigenvalues and eigenvectors, and transforming the eigenvectors obtained back into the vectors for the original system.

Define a non-singular, triangular matrix P such that $A = PP^t$.

Substitution into Equation (4) yields

$$\omega^2 P P^t X - B X = 0 \quad (43)$$

Define the transformation

$$Y = P^t X \quad (44)$$

so that

$$X = (P^{-1})^t Y \quad (45)$$

Equation (43) now becomes

$$\omega^2 P Y - B (P^{-1})^t Y = 0$$

Pre-multiplying by P^{-1} yields

$$\omega^2 Y - P^{-1} B (P^{-1})^t Y = 0$$

or

$$(F - \omega^2 I) Y = 0 \quad (46)$$

where

$$F = P^{-1} B (P^{-1})^t$$

Once the Y's are obtained, the original system vectors are obtained by Equation (45). The eigenvalues, ω^2 , are the system eigenvalues or natural frequencies of vibration.

3.1.2 Program Organization

The OVERLAY configuration of the program is illustrated on Figure 3-1.

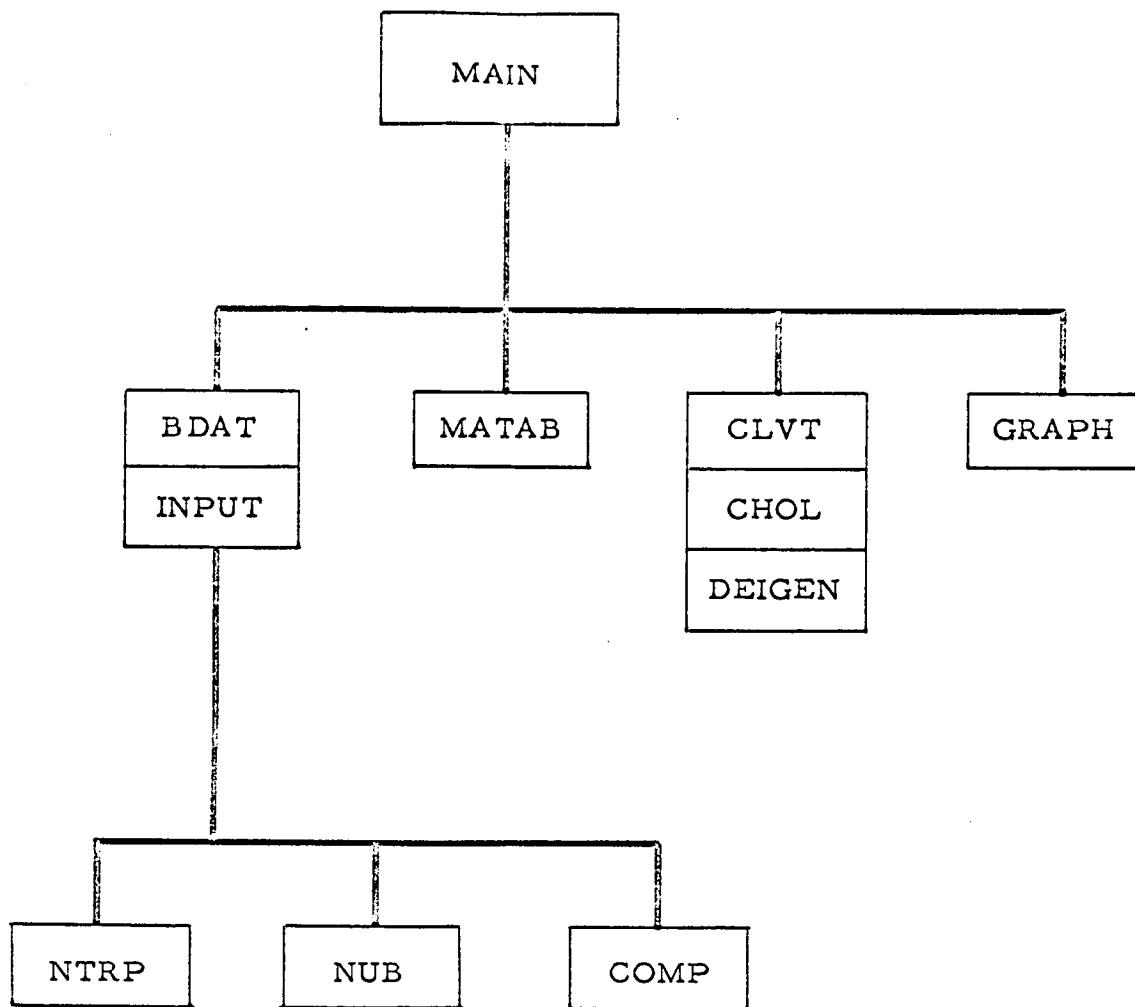


Figure 3-1 - Overlay Configuration

The functions of the principal subroutines are briefly outlined below.

BLOCK DATA: Used for input of all spring constant data, i.e., interstage spring constants, branch beam spring constants, and support spring constants if any.

INPUT: Reads in all problem definition data, other than spring constants, from cards.

NTRP: Interpolates the beam property input data (which may be input in a minimum fashion) to the array form used by the program for integral evaluations and plots.

NUB: Performs static deflection analysis of the beams subject to specified loading conditions to generate displacement functions (along with the associated functions -- shear angle, etc.) which are used in the solution process.

COMP: Evaluates all integral terms needed for construction of the kinetic and potential energy coefficient matrices and prints out these terms along with the problem definition data.

MATAB: Constructs the kinetic and potential energy coefficient matrices.

CLVT: Using subroutines CHOL and DEIGEN, CLVT solves the eigenvalue problem, computing the vehicle natural frequencies and lateral modes.

GRAPH: Plots beam input data and the displacement functions used in the analysis for each beam, and the vehicle mode shapes.

3.1.3 Calculation of Static Displacement Functions

The method employed in the subroutine (NUB) used by the program to calculate the lateral deflections of arbitrary non-uniform Timoshenko beams is described below. The method accommodates all possible boundary conditions and allows for both edge loading and arbitrary lateral loading.

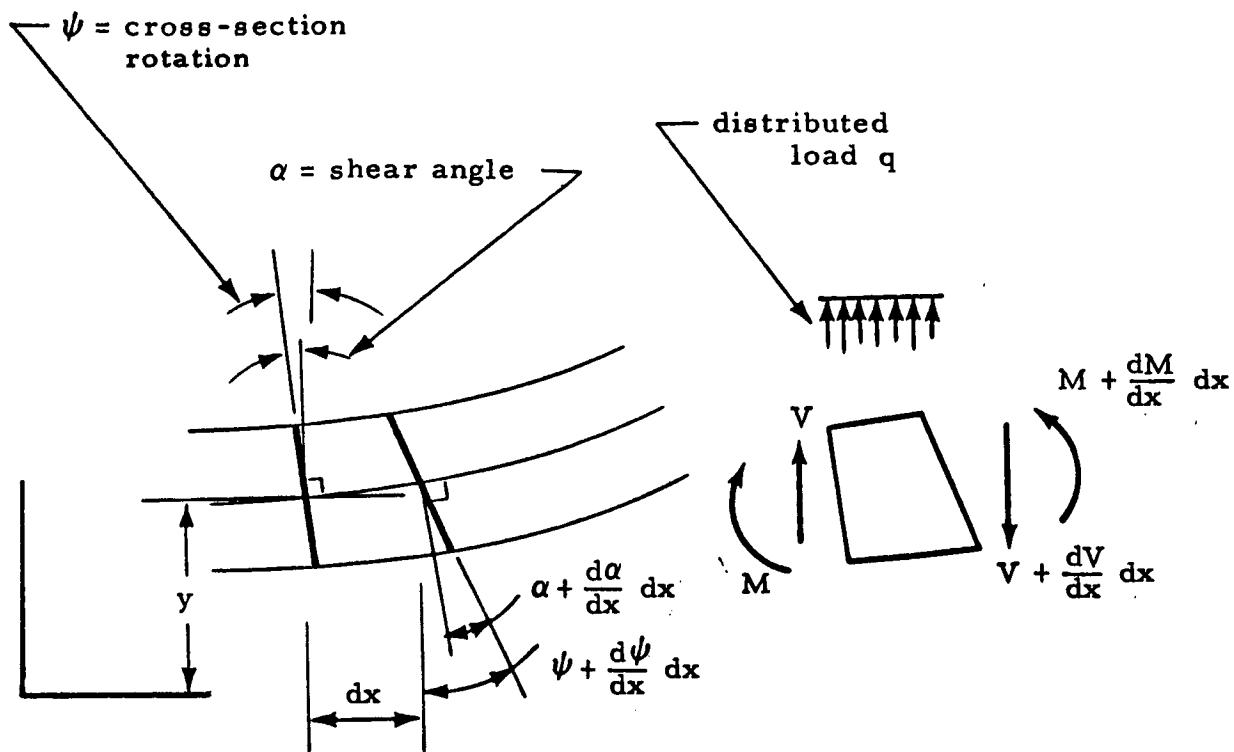


Figure 3-2 - Arbitrary Timoshenko Beam Element

Where, as shown on Figure 3-2 above,

y \equiv lateral deflection,

ψ \equiv cross-section rotation (sometimes called "bending slope"),

α \equiv shear angle,

M \equiv bending moment,

V \equiv shear,

x \equiv position coordinate along beam center line,

$EI(x)$ \equiv bending stiffness, and

$GA(x)$ \equiv shear stiffness,

the usual Timoshenko beam postulates are:

$$\psi' = \frac{M}{EI} \quad (47)$$

and

$$\alpha = \frac{V}{GA} . \quad (48)$$

The static relations between the stress resultants and applied loads are:

$$M' = V \quad (49)$$

and

$$V' = q . \quad (50)$$

The geometrical relation,

$$\psi = y' + \alpha \quad (51)$$

will be used subsequently.

Expanding y and ψ in power of Δ about x we have:

$$y(x+\Delta) = y(x) + y'(x)\Delta + y''(x) \frac{\Delta^2}{2} + y'''(x) \frac{\Delta^3}{3!} + y''''(x) \frac{\Delta^4}{4!} + \dots \quad (52)$$

and

$$\psi(x+\Delta) = \psi(x) + \psi'(x)\Delta + \psi''(x) \frac{\Delta^2}{2} + \psi'''(x) \frac{\Delta^3}{3!} + \dots . \quad (53)$$

From equations (47) through (51) we have (assuming, over the interval Δ , $EI' \equiv 0$, $GA' \equiv 0$, q' and all higher derivatives of $q \equiv 0$):

$$y' = \psi - \alpha = \psi - \frac{V}{GA} , \quad (54)$$

$$y'' = \psi' - \alpha' = \frac{M}{EI} - \frac{q}{GA} , \quad (55)$$

$$y''' = \frac{M'}{EI} = \frac{V}{EI} = \psi'' , \text{ and} \quad (56)$$

$$y'''' = \frac{V'}{EI} = \frac{q}{EI} = \psi''' . \quad (57)$$

The assumptions involved in the four preceding equations are consistent with modeling non-uniform beams as "stepped" beams composed of a large number of short uniform segments, over each of which the distributed load, q , is constant.

Substitution of Equations (54) through (57) into (52) and (53) yields:

$$y(x+\Delta) = y(x) + \left[\psi(x) - \frac{V(x)}{GA} \right] \Delta + \left[\frac{M(x)}{EI} - \frac{q(x)}{GA} \right] \frac{\Delta^2}{2} + \frac{V(x)}{EI} \frac{\Delta^3}{6} + \frac{q(x)}{EI} \frac{\Delta^4}{24} ,$$

or

$$y(x+\Delta) = y(x) + \psi(x)\Delta + M(x) \frac{\Delta^2}{2EI} + V(x) \left[\frac{\Delta^3}{6EI} - \frac{\Delta}{GA} \right] + q(x) \left[\frac{\Delta^4}{24EI} - \frac{\Delta^2}{2GA} \right] , \quad (58)$$

and

$$\psi(x+\Delta) = \psi(x) + M(x) \frac{\Delta}{EI} + V(x) \frac{\Delta^2}{2EI} + q(x) \frac{\Delta^3}{6EI} . \quad (59)$$

The expansions of M and V are

$$M(x+\Delta) = M(x) + V(x)\Delta + q(x) \frac{\Delta^2}{2} \quad (60)$$

and

$$V(x+\Delta) = V(x) + q(x)\Delta . \quad (61)$$

Equations (58) through (61) may be written as:

$$\begin{bmatrix} y(x+\Delta) \\ \psi(x+\Delta) \\ M(x+\Delta) \\ V(x+\Delta) \end{bmatrix} = \begin{bmatrix} 1 & \Delta & \frac{\Delta^2}{2EI} & \left(\frac{\Delta^3}{6EI} - \frac{\Delta}{GA} \right) \\ 0 & 1 & \frac{\Delta}{EI} & \frac{\Delta^2}{2EI} \\ 0 & 0 & 1 & \Delta \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} y(x) \\ \psi(x) \\ M(x) \\ V(x) \end{bmatrix} + q(x) \begin{bmatrix} \frac{\Delta^4}{24EI} - \frac{\Delta^2}{2GA} \\ \frac{\Delta^3}{6EI} \\ \frac{\Delta^2}{2} \\ \Delta \end{bmatrix} . \quad (62)$$

It will now be assumed that the beam is divided into a large number ($n - 1$) of uniform segments, each of the same length, Δ . It will also be convenient to make the following definitions:

For $i = 1$ to n ,

$$x_i \equiv (i-1)\Delta,$$

$$y_i \equiv y(x_i), \psi_i \equiv \psi(x_i), M \equiv M(x_i), V_i \equiv V(x_i), \text{ and } q_i \equiv q(x_i),$$

and for $x_i < x < x_{i+1}$:

$$EI_i \equiv EI(x) \text{ and}$$

$$GA_i \equiv GA(x);$$

also,

$$S_i \equiv \begin{bmatrix} y_i \\ \psi_i \\ M_i \\ V_i \end{bmatrix} .$$

Using the above definitions, Equation (62) may be re-written as

$$S_{i+1} \equiv T_i S_i + R_i , \quad (63)$$

where

$$T_i \equiv \begin{bmatrix} 1 & \Delta & \frac{\Delta^2}{2EI_i} & \left(\frac{\Delta^3}{6EI_i} - \frac{\Delta}{GA_i} \right) \\ 1 & \frac{\Delta}{EI_i} & \frac{\Delta^2}{2EI_i} & \\ & 1 & \Delta & \\ & & & 1 \end{bmatrix}$$

, and

$$R_i = q_i \begin{bmatrix} \frac{\Delta^4}{24EI_i} - \frac{\Delta^2}{2GA_i} \\ \frac{\Delta^3}{6EI_i} \\ \frac{\Delta^2}{2} \\ \Delta \end{bmatrix} .$$

Where $i = 1$ at the extreme left end of the beam, the "state", S_2 , at the right end of the first segment may be written in terms of the left end boundary conditions, S_1 , as

$$S_2 = T_1 S_1 + R_1 .$$

Similarly,

$$S_3 = T_2 S_2 + R_2 = T_2 T_1 S_1 + T_2 R_1 + R_2 .$$

In general, then,

$$S_i = C_i S_1 + E_i , \quad (64)$$

so that

$$S_{i+1} = T_i C_i S_1 + T_i E_i + R_i .$$

Accordingly, the recursion relations for the 4×4 matrix C_i and the vector E_i are

$$C_{i+1} = T_i C_i \quad \text{and} \quad (65)$$

$$E_{i+1} = T_i E_i + R_i . \quad (66)$$

The foregoing equations provide a straightforward basis for calculations C_n and E_n , so that the relation between the boundary conditions at the left end, S_1 , the boundary conditions at the right end, S_n , and the applied loading field may be written as:

$$S_n = C_n S_1 + E_n \quad (67)$$

As boundary conditions, the values of the following quantities must be prescribed (not necessarily zero):

- At the left end, either Y_1 or V_1 , and either ψ_1 or M_1 .
- At the right end, either Y_n or V_n , and either ψ_n or M_n .

Since C_n and E_n are known, Equation (67) becomes a set of four linear equations in the four unknown boundary conditions once the four known boundary conditions have been stated.

The program is set up to solve Equation (67) for the unknown boundary conditions for any possible set of edge conditions. Once the state, S_1 , at the left edge has been evaluated in this way, Equation (63) may be used to calculate the state at all interior points in the beam.

3.2 Modeling

3.2.1 Beam Selection and Choice of Displacement Functions

Selection of the number of beams and their end-point locations is closely related to the choice of beam displacement functions. For example, in a particular problem one might achieve equally accurate solutions by either (1) using a small number of beams and a large number of complicated displacement functions for each beam, or (2) using a larger number of beams and only a few displacement functions for each beam. In general, the latter approach appears to be more appropriate; especially if the stiffness properties of the vehicle vary drastically. The two approaches usually involve about the same number of degrees of freedom, hence about the same computer execution time.

Another consideration is that the present program set-up allows external support springs (translational and/or rotational) only at the ends of beams.

Usually, the governing factor in the selection of beam end point locations is the vehicle stiffness distribution. Interior spans of beams should not contain zones which are very weak in shear or bending relative to adjacent parts of the beam--that is, the stiffness properties of a given beam should not vary drastically. Otherwise, the static displacement functions calculated by the program for such beams will not be capable of describing accurately the dynamic behavior of that part of the system--hence the calculated vehicle frequencies may be significantly too high.

In all of the examples presented in Appendix A, the displacement functions used are "static displacement functions" generated internally by the program. The set most commonly used is:

- For each interior beam, three functions, each corresponding to a particular loading of the beam with pinned-pinned boundary conditions: (1) moment applied at one end, (2) moment applied at the other end, and (3) lateral distributed loading proportional to the beam's mass distribution.

- For the end beams, the above three pinned-pinned static functions are used, except where the end is free, in which case the last function mentioned above is replaced by a cantilever function with lateral loading proportional to beam mass intensity.

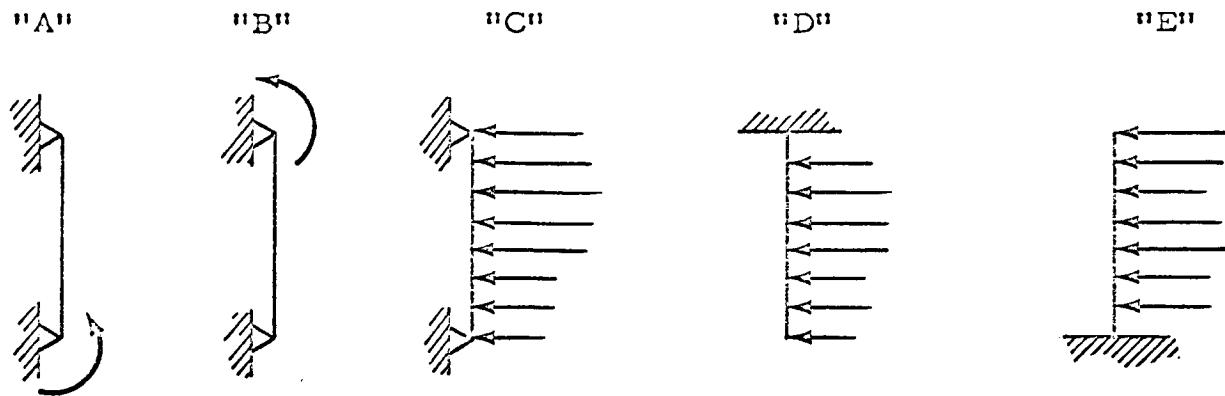
These "standard" sets of displacement functions are illustrated on Figure 3-3.

The configuration of the program is such that with only a few minor alterations in the coding, virtually any static displacement function that one might wish to use can be internally generated (see the discussion in Section 3.1.3). Also, it is easy to provide for reading in displacement function data generated externally. However, as may be seen in the results presented in Appendix A, the simple "standard" set of displacement functions described above works quite well, provided that the locations of the beam end points are well-selected.

3.2.2 Interstages

Normally the interstage stiffness matrices (K_i in Section 2.4.2) may be calculated by shell theory, finite element methods, etc.; or perhaps they might be known from full-scale or model tests.

Also, one may wish to rigidly butt together the ends of two beams for various modeling purposes. In order to do this a zero-length interstage, as discussed in Section 2.4.2, may be employed. In this case, relatively large moment-rotational stiffness constants must be used; however, care must be exercised not to select numbers so large that serious arithmetic round-off errors are introduced into the solution. Normally, a good choice of such constants is approximately 10^3 or 10^4 times a representative value of beam bending stiffness (EI adjacent to the interstage) divided by the length of one of the connected beams. If the constant so selected is too small, it will be evident in the calculated mode shapes. If it is too large, numerical inaccuracies, which will be reflected in the program error checks, will appear.



Types of Static Displacement Functions

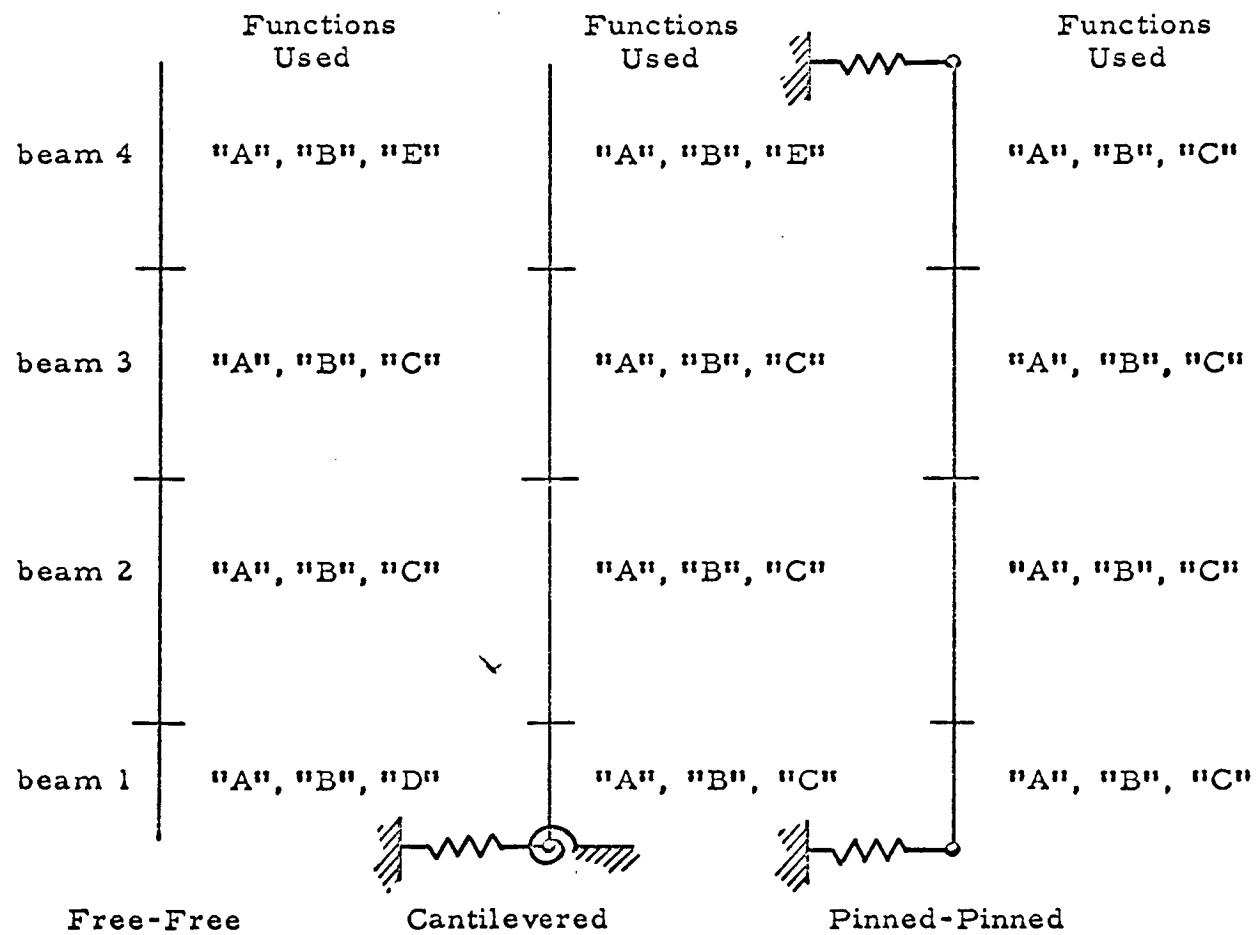


Figure 3-3 - Standard Beam Displacement Functions Used in the Program

In the case of free-free vehicles, a common symptom of arithmetic round-off difficulties is obvious error in the rigid body modes. Some round-off error is always present, of course, so that the frequencies calculated for the rigid body modes will not be exactly zero; for example they may be typically 1/100 or 1/1000 of the lowest elastic frequency for a large complicated vehicle. However, when comparatively large frequencies are calculated for these modes, the trouble is usually due to an unreasonably large value of some spring constant having been arbitrarily chosen.

Another possible source of round-off error is the use of extremely short non-zero length interstages where a zero-length interstage is more appropriate for modeling purposes. Care should be exercised in modeling the interstages to avoid the possibility of this difficulty. Normally, if the interstage is at least 1/100 the length of the shortest attached beam, no accuracy problem will arise.

3.2.3 External Support Springs

External support springs which, as discussed in Section 2.4.4, are allowed at the ends of any or all of the beams comprising the vehicle may, if inappropriately chosen, result in substantial round-off errors. Where EI is the maximum value of bending stiffness occurring throughout the vehicle and L is the vehicle length, one should normally not use values of lateral support spring constants exceeding approximately $10^5 \times EI/L^3$, nor values of rotational spring constants exceeding about $10^4 \times EI/L$ when employing such springs to approximate pinned, guided, or fixed boundary conditions. Spring constants in the neighborhood of those values effectively suppress lateral displacement and rotation, respectively, for the lower vehicle modes. If an error is inadvertently made in choosing the values of such spring constants, it is normally immediately evident in the calculated results.

3.3 User's Manual

3.3.1 Input

All problem definition data is input on data cards (FORMAT described below) except spring constant data which is input through a BLOCK DATA subroutine.

Data Cards

The first three data cards contain general data for the system. The remainder of the cards, which contain beam definition data, are assembled in data groups - a group for each beam in the system.

The format for the first three cards is given below.

Card No.	Symbol	Format	Card Column
1	TITLE	I2A6	1-72
2	OPTION (1)	I6	1-6
	OPTION (2)	I6	7-12
	OPTION (3)	I6	13-18
	OPTION (4)	I6	19-24
	OPTION (5)	I6	25-30
	OPTION (6)	I6	31-36
3	N	I3	1-3
	REF (1)	E12.8	4-15

The symbols appearing on the first three cards are defined below

TITLE: BCD Problem description (Veh. no., Date, etc.)

OPTION (1): = 1 Rotary inertia is included.

 = 0 Rotary inertia is neglected.

OPTION (2): = 1 Displacement functions and associated arrays
 (shear angle, etc.) are printed out

 = 0 Arrays not printed out

OPTION (3) = 1 Shear deflections are included
 = 0 Shear deflections are neglected
 OPTION (4) Not operational
 OPTION (5) Not operational
 OPTION (6) = K K is the number of modes to be plotted by
 the SC-4020 plotter. If N = 0 the plot routine
 (GRAPH) will not be called.
 N : Number of beams
 REF(1) Vehicle reference location (normally 0.). This
 value is used for plotting purposes and in calcu-
 lating distance to CG.

A description of the cards which compose a beam data group is given below. The group defining the i^{th} beam will be discussed.

Card No.	Symbol	Format	Card Column
I1	NP(I)	I6	1-6
	NF(I)	I6	7-12
	NMP(I)	I6	13-18
	NIP(I)	I6	19-24
	NEI(I)	I6	25-30
	NGA(I)	I6	31-36
I2	BL(I)	E12.8	1-12
	SL(I)	E12.8	13-24
	BM(I)	/ E12.8	25-36
	BD(I)	/ E12.8	37-48

The symbols appearing on the first two cards of the data group for the i^{th} beam are defined below.

NP(I)	No. of stations for purposes of numerical integration and plotting
NF(I)	No. of displacement functions (N_i) (the same number in both principal directions)

NMP(I)	No. of mass input points (2 x no. of mass data pairs)
NIP(I)	No. of mass moment of inertia input points
NEI(I)	No. of bending stiffness input points
NGA(I)	No. of shear stiffness input points
BL(I)	Beam length (L_i)
SL(I)	Interstage length (ℓ_i)
BM(I)	Branch beam mass (m_i)
BD(I)	Branch beam length (d_i)

The DIMENSION statements presently used in the program require that the following limitations be observed:

$$N \leq 12,$$

For any I,

$$\begin{aligned} NP(I) &\leq 200, & NF(I) &\leq 4, \\ NMP(I) &\leq 500, & NIP(I) &\leq 500, \\ NEI(I) &\leq 500, & NGA(I) &\leq 500. \end{aligned}$$

Also,

$$\begin{aligned} \sum_{I=1}^N NMP(I) &\leq 900, & \sum_{I=1}^N NIP(I) &\leq 900, \\ \sum_{I=1}^N NEI(I) &\leq 900, & \sum_{I=1}^N NGA(I) &\leq 900. \end{aligned}$$

The remainder of the cards of a beam data group contain the beam mass, inertia and stiffness distribution data. This data is input as a set of data pairs for each beam property function. Each data pair consists

of a position coordinate (origin at lower end of beam) and the corresponding magnitude of the function.

A listing of a sample set of input cards which constitute a data group for a typical beam (Figure 3-4) is presented below.

100	3	10	10	8	8			
20	+02	20	+01	240	+03	15	+01	
			4	+04	6	+01	6	+04
				+04	6	+02	4	+04
14	+02	4	+04	20	+02	4	+02	+04
			2	+02	6	+01	3	+02
14	+02	2	+02	20	+02	2	+02	+02
			8	+09	6	+01	10	+02
20	+02	8	+09		+01	10	+10	+10
			7	+07	6	+01	8	+07
20	+02	7	+07			+07	14	+02
						+02	8	+07

In the above list, the first card specifies NP = 100, NF = 3, NMP = 10, NIP = 10, NEI = 8, NGA = 8. The second card specifies BL = 20.0, SL = 2.0, BM = 240.00, BD = 1.5. The next two cards specify the mass distribution, the next two the cross-section mass mount data, the next two the bending stiffness, and the last two the shear stiffness.

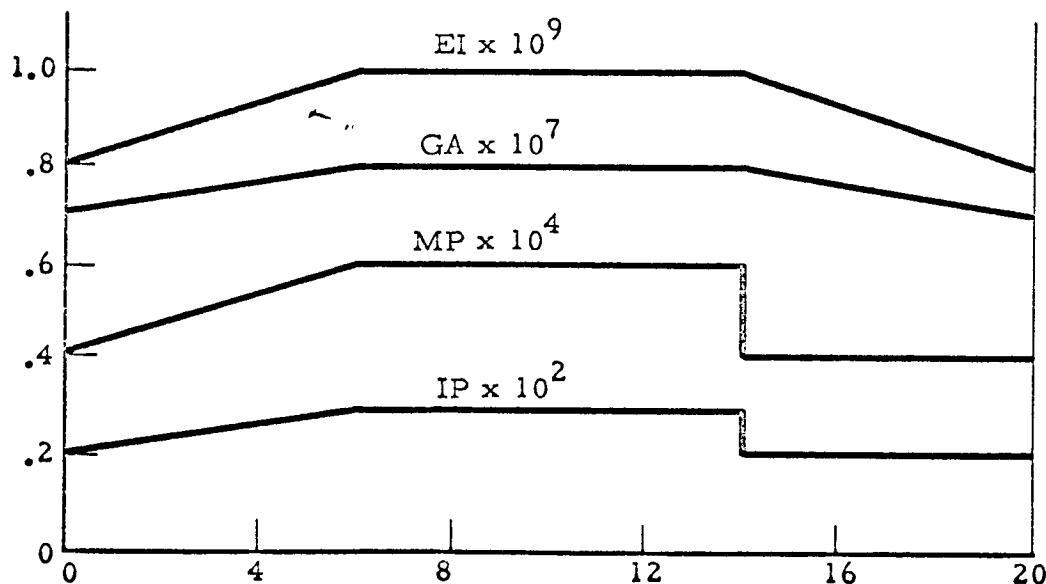


Figure 3-4 - Typical Beam Properties

Block Data

The following quantities are input through block data. The corresponding variable used in Section 2 is listed parenthetically.

SK's	interstage spring constants	(k^i)
SKB's	branch beam spring constants	(k_{bi})
SSL1	lateral support springs (left end-dir 1)	(k_{lsi}^{l1})
SSL2	lateral support springs (left end-dir 2)	(k_{lsi}^{l2})
SSR1	lateral support springs (right end-dir 1)	(k_{rsi}^{r1})
SSR2	lateral support springs (right end-dir 2)	(k_{rsi}^{r2})
RSL1	rotational support springs (left end-dir 1)	(k_{rsi}^{l1})
RSL2	rotational support springs (left end-dir 2)	(k_{rsi}^{l2})
RSR1	rotational support springs (right end-dir 1)	(k_{rsi}^{r1})
RSR2	rotational support springs (right end-dir 2)	(k_{rsi}^{r2})

Only the non-zero spring constant values need be input. A sample BLOCK DATA input appears in the program listing (Appendix B).

3.3.2 Output

The program output is in two parts:

- a. Printed output
- b. SC-4020 plotted output.

Printed Output:

- Problem Definition Data

The input data is printed out, including the beam property arrays containing the interpolated values. The displacement functions and associated functions for each beam may be printed out (OPTION(2)). If these arrays are not printed, only the beam boundary conditions used in the static analysis are printed out.

- Intermediate Computed Terms, used for construction of the "mass" matrix and "stiffness" matrix.

The quantities are identified in the output by their FORTRAN variable names. A table is presented below showing the correlation between the FORTRAN variables and the symbols used in the formulation (Section 2.4).

BW	M
BJ	J
R1	R ⁽¹⁾
R2	R ⁽²⁾
Y1	$\gamma(1)$
Y2	$\gamma(2)$
YZ1	$\Omega(1)$
YZ2	$\Omega(2)$
Y1PL	$[Z^{(1)}(x)]_{x=0}$

Y2PL	$[Z^{(2)}(x)]_{x=0}$
Y1PR	$[Z^{(1)}(x)]_{x=L}$
Y2PR	$[Z^{(2)}(x)]_{x=L}$
G1	$G^{(1)}$
G2	$G^{(2)}$
BYZ1	$\psi^{(1)}$
BYZ2	$\psi^{(2)}$

- Kinetic and Potential Energy Coefficient Arrays.

These and other arrays are identified in the output by English text headings.

- System Frequencies and Eigenvectors.

The system eigenvectors are printed out in an unnormalized matrix form and in a normalized tabular form along with the natural frequency and generalized mass for each mode.

- Solution Accuracy Checks.

Two matrix solution accuracy checks are included in the output: (1) an eigenvector orthogonality check, which gives an indication of the accuracy of the eigenproblem solution (for diagonal elements of unity, off-diagonal terms should be of the order of 10^{-6} or smaller), (2) a normalized error matrix which represents the right side of Equation (4) (ideally zero) upon substitution of the system eigenvalues and eigenvectors computed by the program. The elements of this array are typically 10^{-3} or smaller.

Note that this type of solution accuracy check represents a sufficient but not necessary condition for judging the accuracy of the solution.

Plotted Output:

The SC-4020 plots contain both problem definition data and solution information. For each beam, the distributed property data (mass distribution, bending stiffness, etc.) is plotted in both the minimal input form and in the interpolated form generated by the program for use in calculating various integrals. The minimal input form of such data is represented by the piece-wise continuous straight lines appearing on the plots, and the interpolated values are shown as "points." Also included are plots of the sets of lateral displacement functions used to represent the deformation of each beam.

The solution data plots consist of projections of each vehicle mode shape onto the pitch and yaw planes.

Section 4

RECOMMENDED ADDITIONAL DEVELOPMENTS

While the program in its present configuration provides a basis for solving a wide class of problems, there are several additional developments which could be incorporated to expand the program's usefulness greatly. They are:

- Torsion. By inserting as additional coordinates the angles of twist (roll) of the ends of the individual beams comprising the vehicle, provision could be made for taking into account the effects of bending-torsion coupling in interstages (such as the Apollo Command Module-Service Module interstage). Internally-calculated quasi-static twist functions would be used for each beam and the effects of off-center mass placement accounted for.
- Lateral Propellant Slosh. Lateral propellant slosh effects may be modeled using the usual mass-spring mechanical analogy. One significant advantage of having the capability of doing this is to permit closer verification of mathematical models with dynamic test stand and model test results. This is desirable regardless of whether or not lateral slosh modes are employed in analysis of flight vehicle stability, response, etc.
- Internal Stress Resultants. Moment and shear distributions (and twisting moment, if torsion is included) should be calculated and plotted.
- Automatic Error Analyses. Further solution accuracy checks should be incorporated to check for the occurrence of significant round-off error, and to prominently flag any such error in the output.
- Propellant Mass Distribution. Provision should be incorporated for automatic calculation of propellant levels, propellant mass distribution, etc., for arbitrary flight times.
- Displacement Functions. Further study should be made of beam displacement functions. As noted in the present report, static displacement functions work quite well if the internal points of subdivision into "beams" and interstages are well-chosen. However, several other techniques appear quite attractive. For example,

one could initially use static displacement functions to calculate a vehicle mode, then use a "static loading" based on this vehicle mode and the mass distribution to calculate a new additional set of displacement functions which would then be used in a second analysis, and so on until convergence is observed. This would have to be done for each vehicle mode separately; however, since the calculations involved require only a few seconds at each such step, there appears to be no problem of excessive expense in terms of computer execution time.

Section 5
REFERENCES

1. Pearson, M. L., "Nonplanar Vibrational Characteristics of Complex Space Vehicles," LMSC/HREC A782412, Lockheed Missiles & Space Company, Huntsville Research & Engineering Center, 22 March 1966.
2. Kiefling, L., "Modified Stodola Method for Bending Vibration Analyses," NASA/MSFC R-AERO-IN-22-64, 18 September 1964.
3. Yen, C. L., "Numerical Analysis of Orthotropic Shells of Revolution," LMSC/HREC A782778, Lockheed Missiles & Space Company, Huntsville Research & Engineering Center, May 1966.

APPENDIX A
PROGRAM RESULTS

PROGRAM RESULTS

The results of ten executions of the program are presented and summarized in this appendix. These are only a small fraction of the test cases executed for various purposes during the course of program development. Briefly, these problems are:

Problem No.

- 1 Uniform simple free-free beam
- 2 A non-symmetrical problem involving non-planar modes
- 3 SA-202D upper stages (free-free)
- 4 SA-D6 upper stages (cantilevered)
- 5 SA-501, free-free, 4-beam model
- 6 SA-501, free-free, 6-beam model
- 7 SA-501, free-free, S-II/S-IVB interstage constants evaluated using Timoshenko beam theory
- 8 SA-501, free-free, S-II/S-IVB interstage constants evaluated using shell theory
- 9 SA-501, cantilevered, S-II/S-IVB interstage constants evaluated using Timoshenko beam theory
- 10 SA-501, cantilevered, S-II/S-IVB interstage constants evaluated using shell theory

Problem Nos. 3 through 10 all involve rotationally symmetrical vehicles. Accordingly, the program (expecting a completely general non-symmetrical vehicle in each case) always calculated pairs of modes (one in the pitch plane, one in yaw) at identical frequencies. In presenting these solutions, one member of each such pair is deleted for brevity.

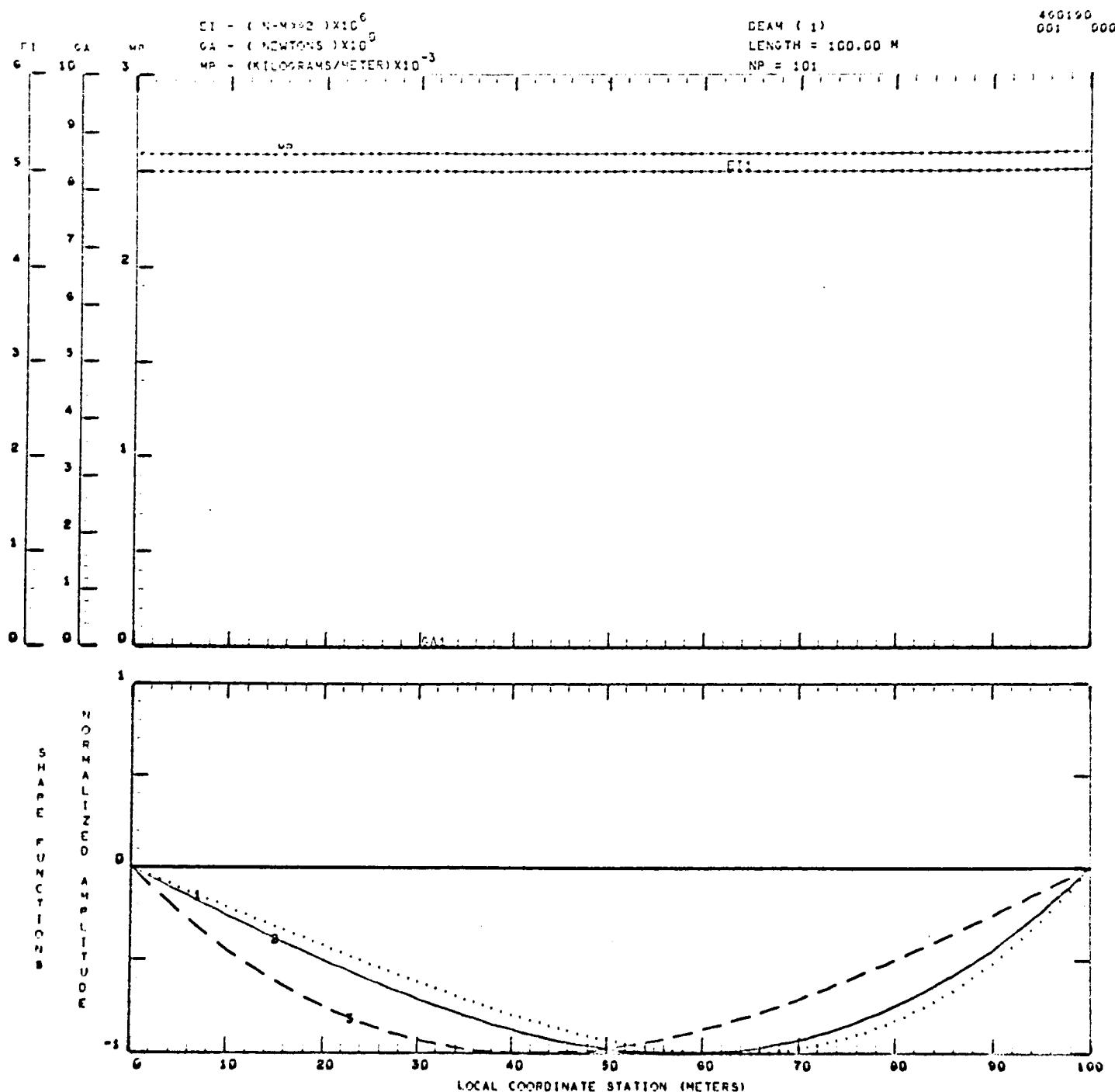
On the beam property plots in the first three problems, lb-sec-in. units, rather than the mks units indicated, apply.

PROBLEM NO. 1

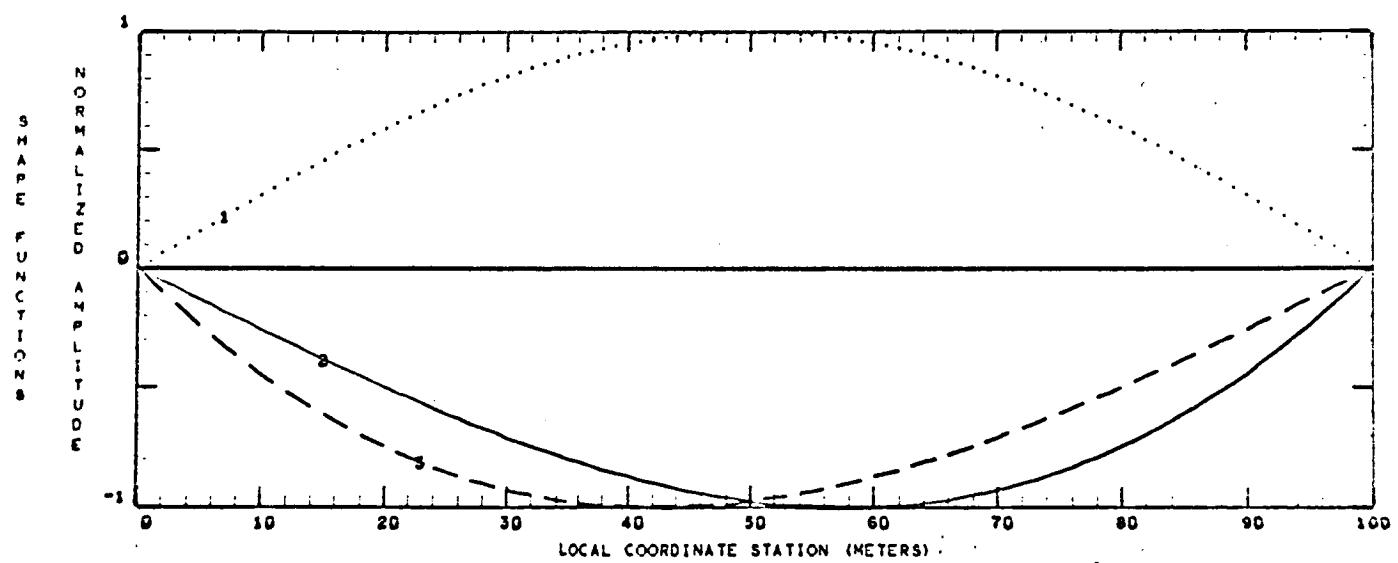
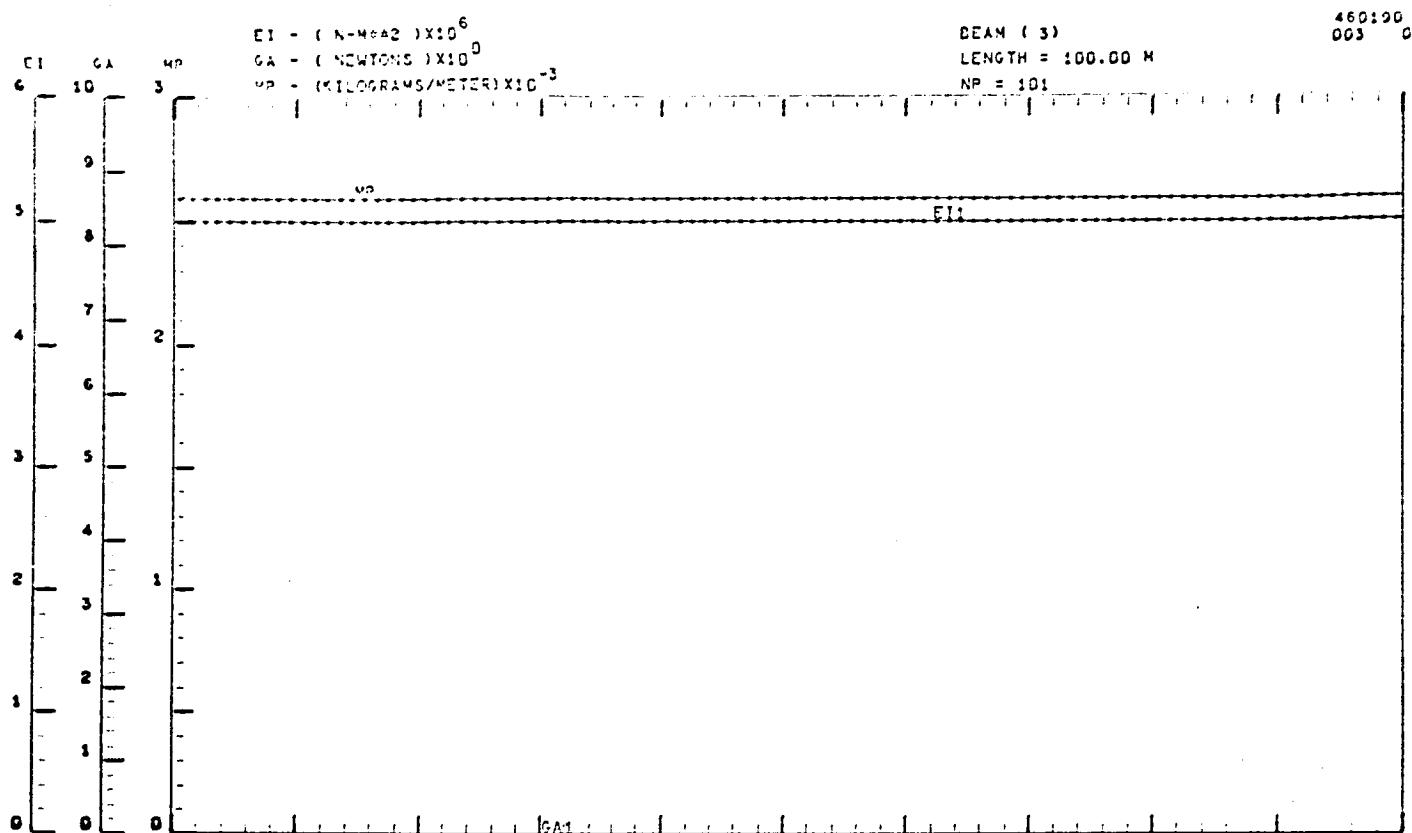
DESCRIPTION: A uniform dually-symmetrical free-free beam modeled as five beam segments, each of equal length. Three displacement functions (standard set discussed in Section 3.2.1) were used for each beam segment. Rotary inertia and shear were neglected. In the table below, the results of the analysis are summarized and compared with the exact free-free uniform beam solutions.

Since the beam is symmetrical with equal properties in both planes, only one set of solutions is shown. The beam is 500 inches long with $EI = 5 \times 10^6 \text{ lb/in.}^2$ and mass per unit length = $.00259 \text{ lb-sec}^2/\text{in.}^2$

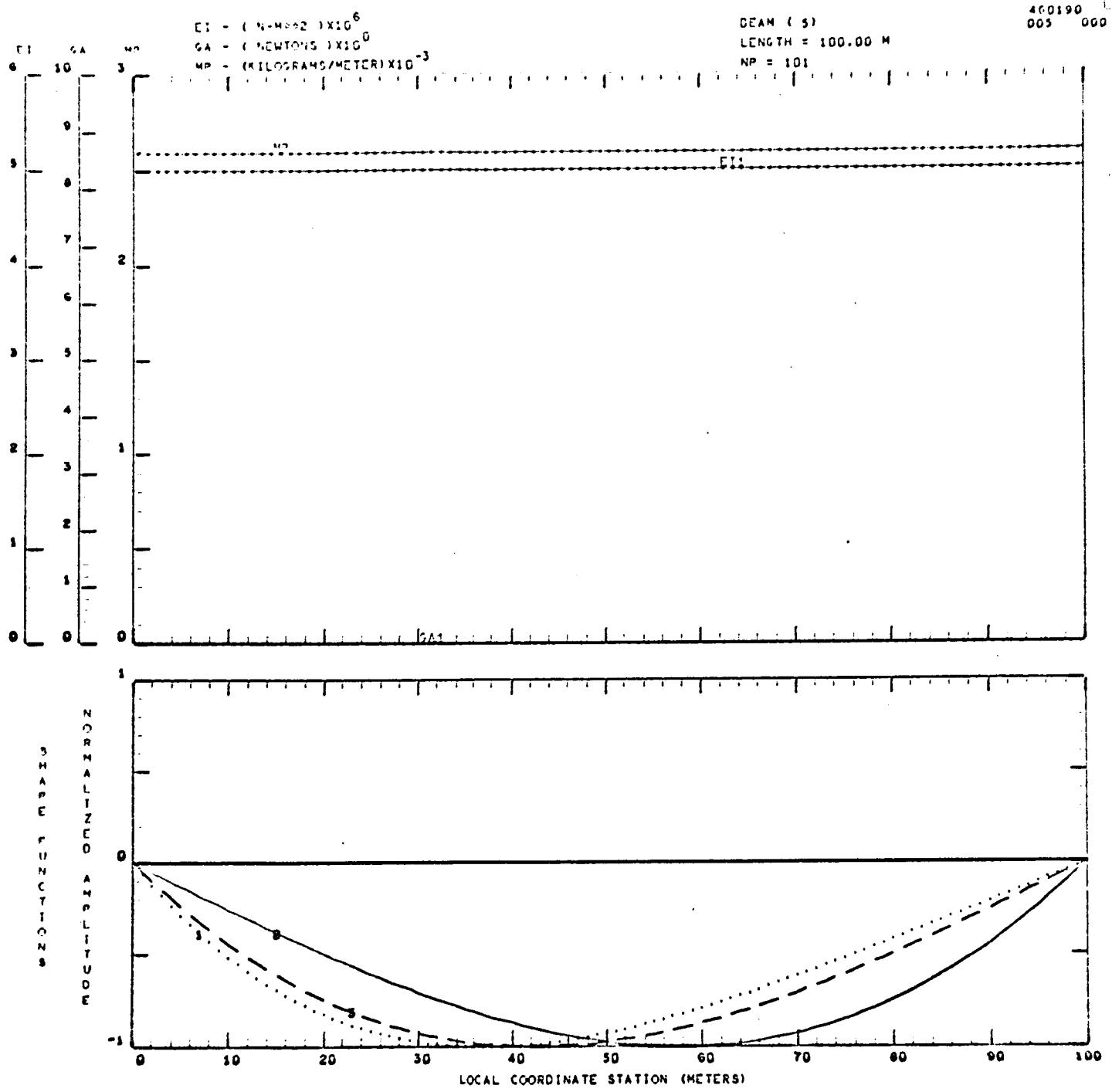
SUMMARY OF RESULTS:	Mode	Calculated Frequency (cps)	Exact Frequency
	1	.626	.626
	2	1.725	1.725
	3	3.384	3.382
	4	5.611	5.590
	5	8.382	8.351

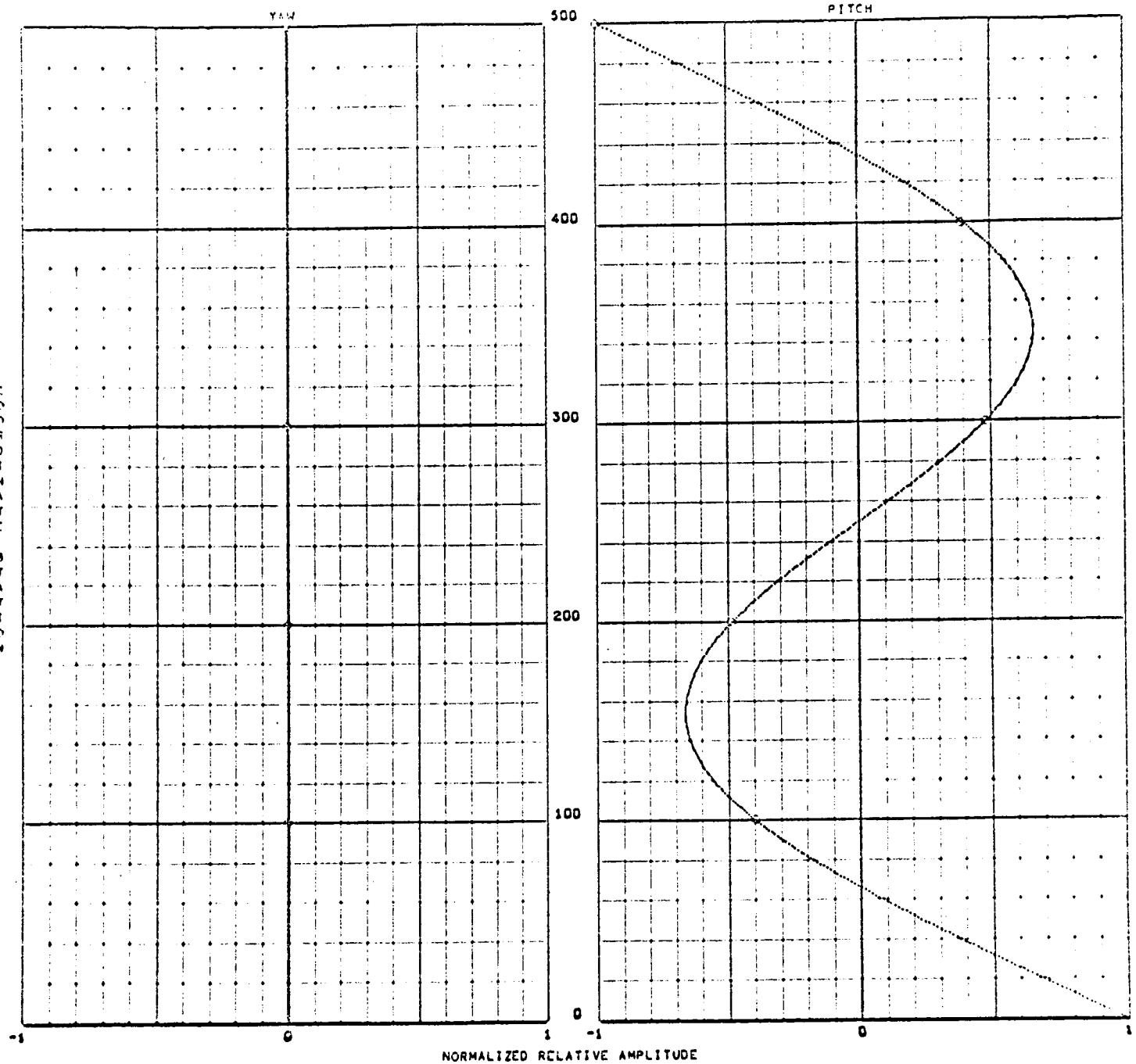


VEHICLE REFERENCE
STATION = 0.00

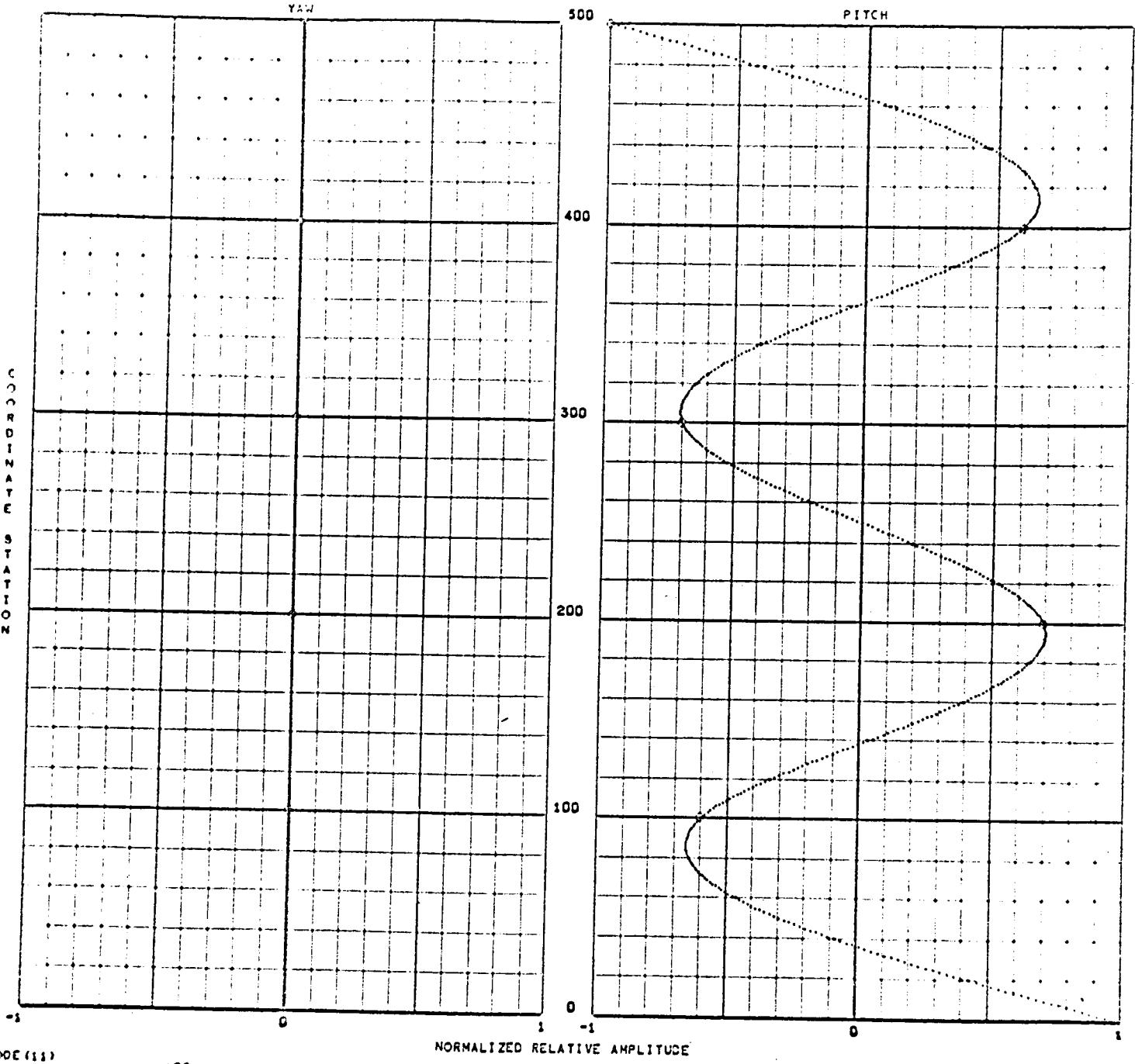
460190
003 000

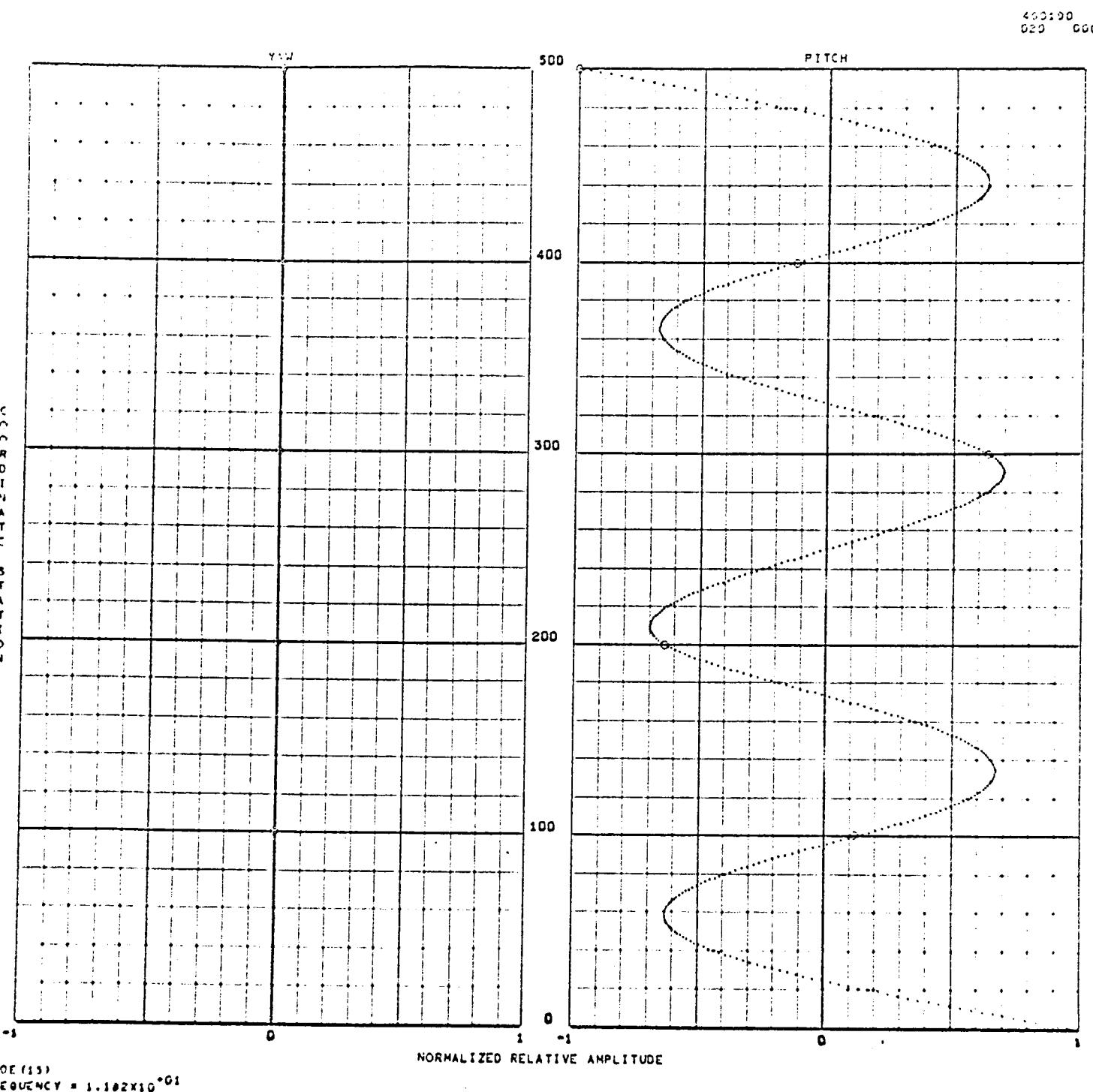
VEHICLE REFERENCE
STATION = 200.00



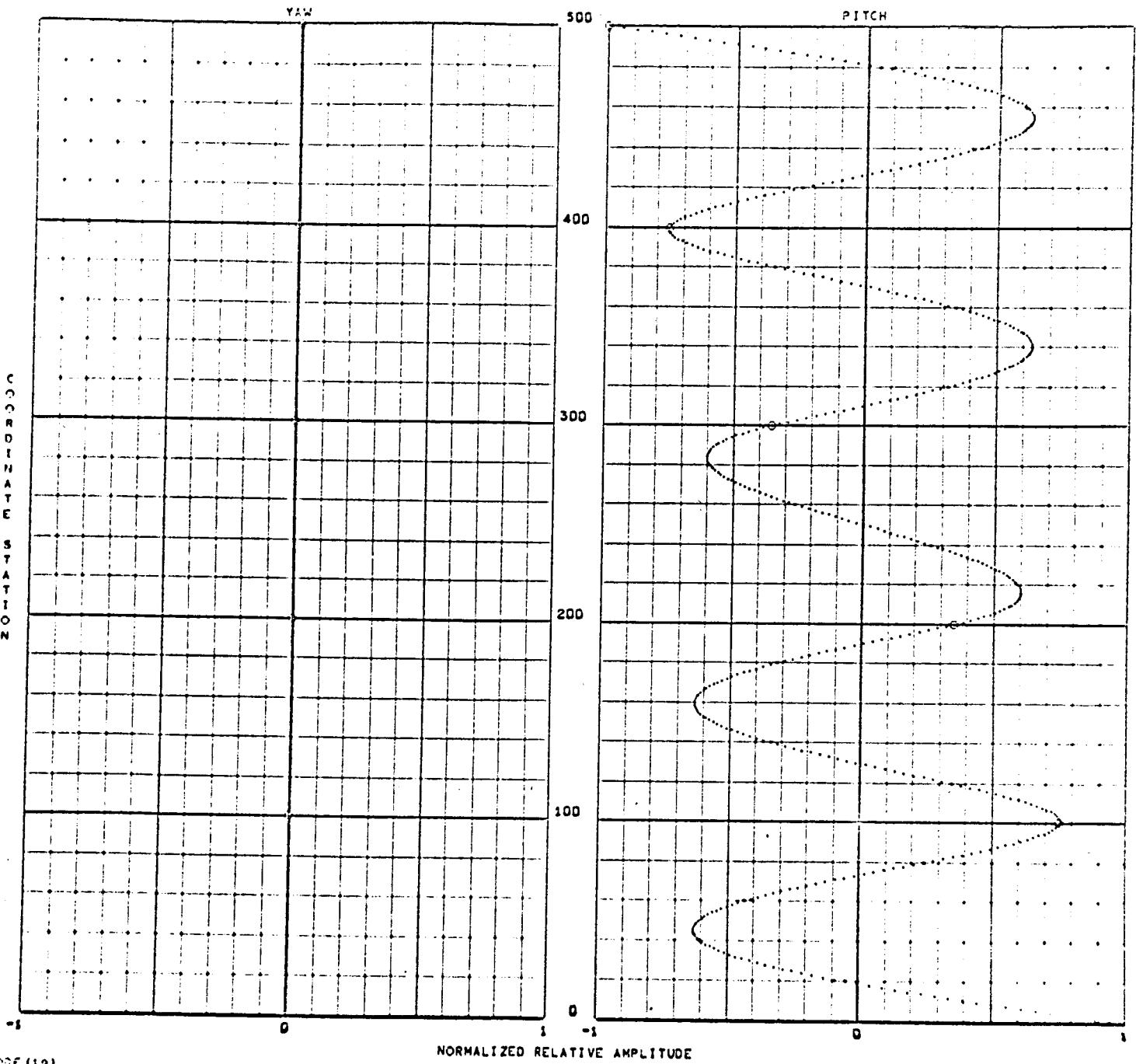
463190
012 000 L

M0FF(7)
FREQUENCY = 1.724×10^{00}

460190
016 600 L



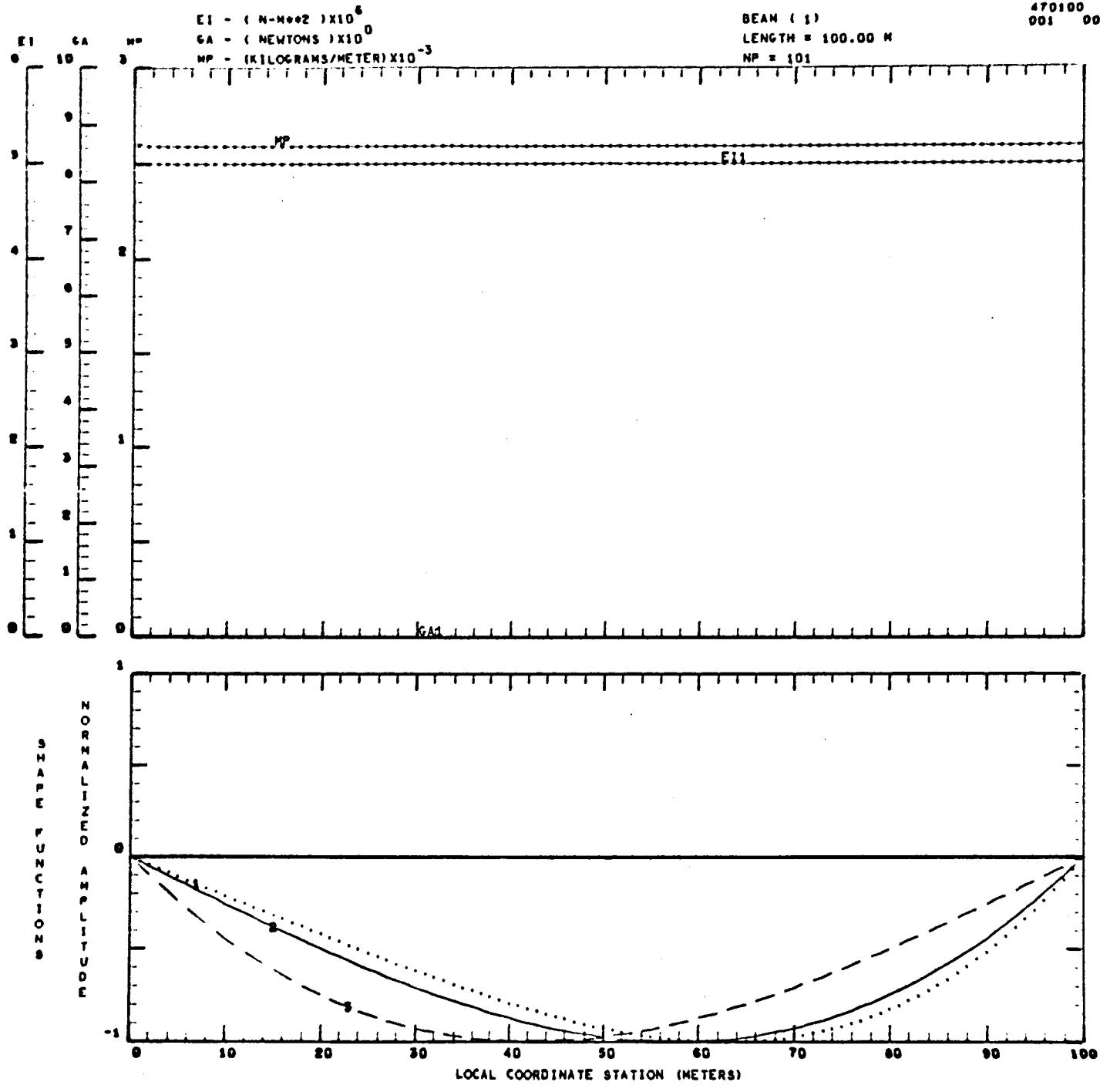
460190
024 000



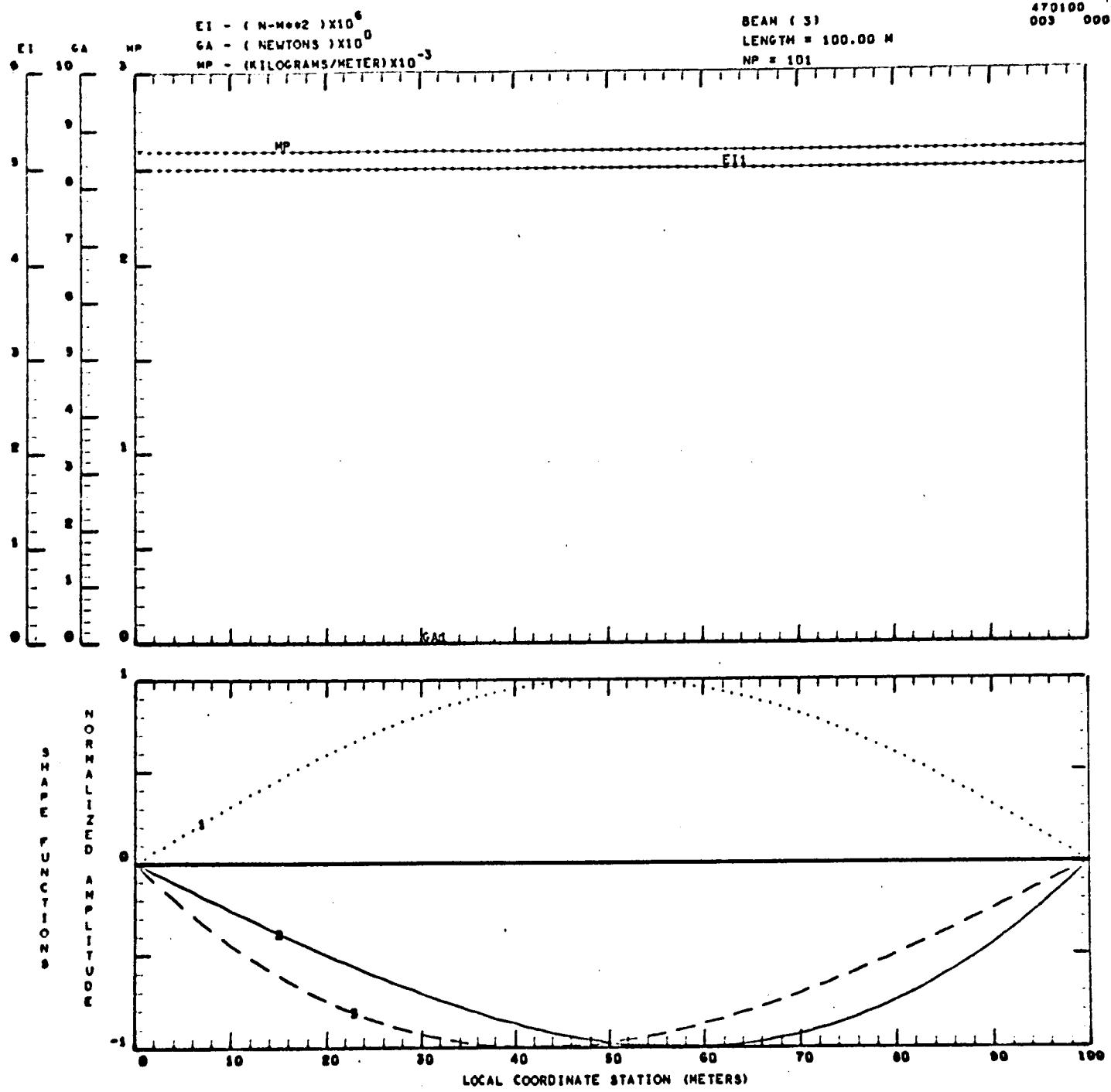
PROBLEM NO. 2

DESCRIPTION: Same as Problem No. 1, except that the bending stiffness in the second principal direction for each beam segment was doubled ($EI_2 = 10 \times 10^6 \text{ lb/in.}^2$) and the first beam segment was rotated such that its principal axes were inclined at an angle of 30° with the principal axes of the other four beams. It is interesting to compare these results with those of Problem No. 1.

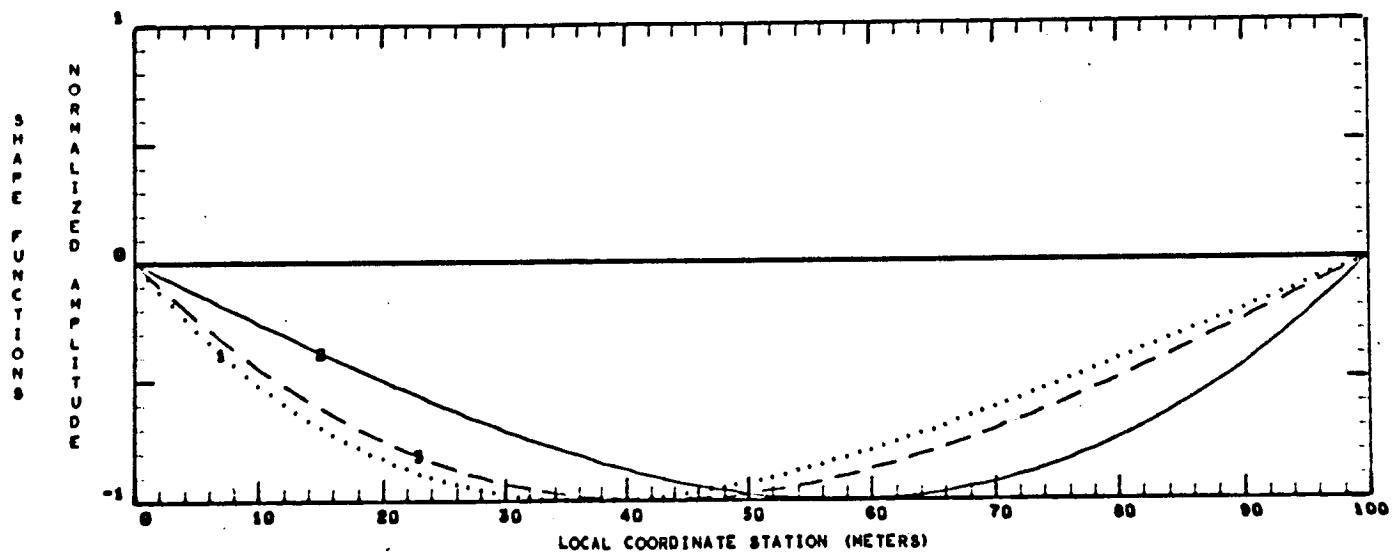
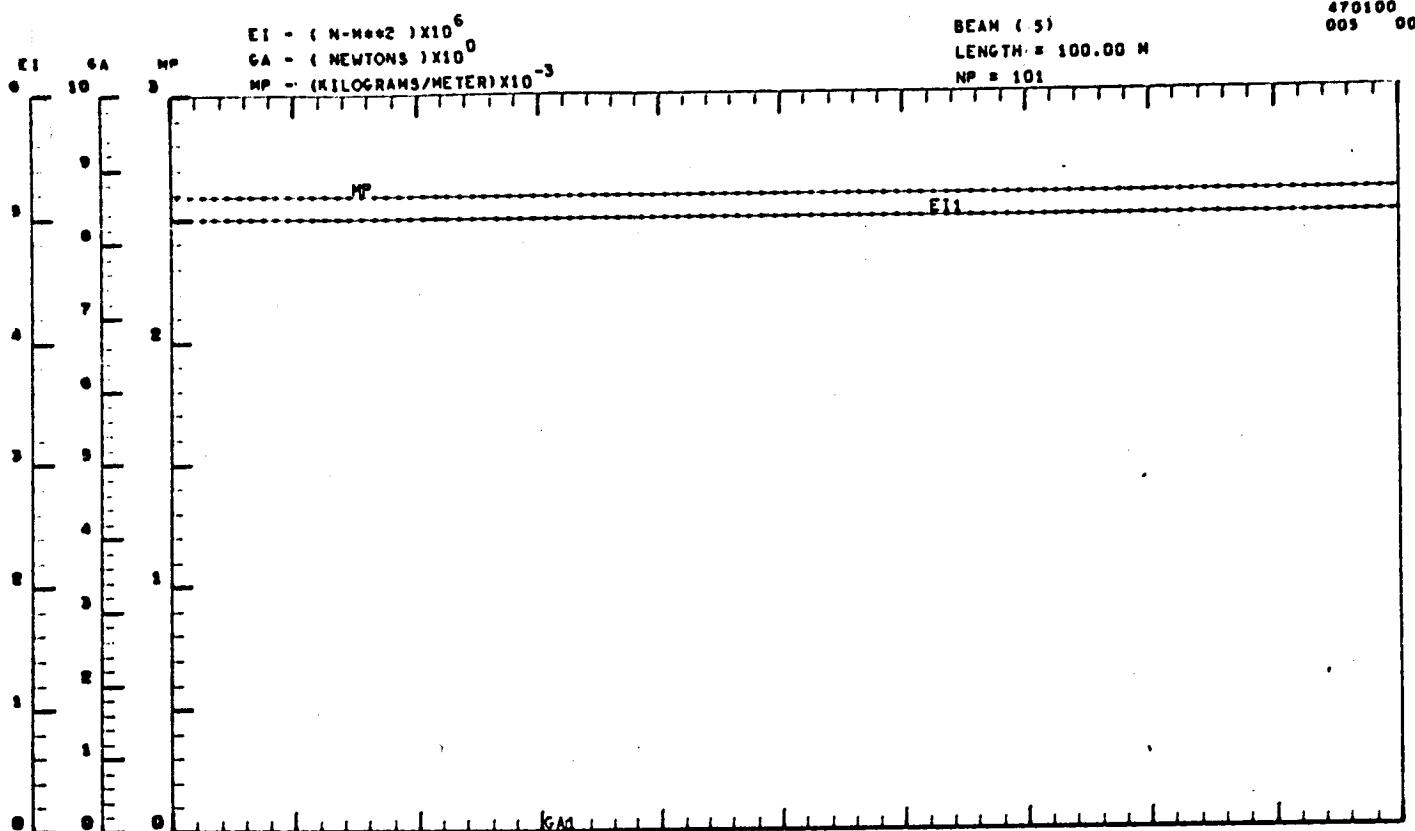
SUMMARY OF RESULTS:	Mode	Calculated Frequency (cps)
	1	.626
	2	.883
	3	1.733
	4	2.414
	5	3.418
	6	4.680
	7	5.713
	8	7.691
	9	8.621
	10	11.430

470100
001 000

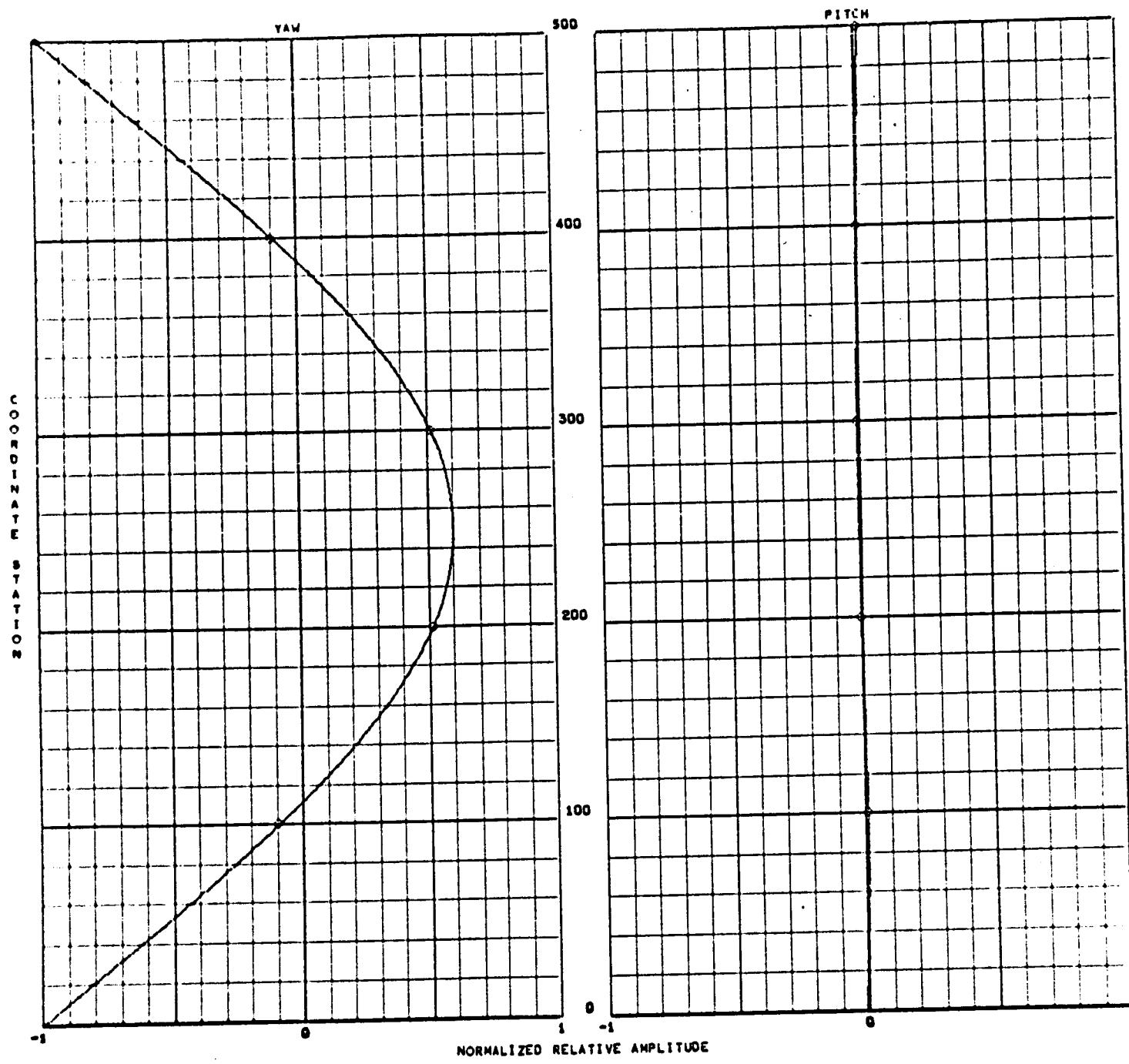
VEHICLE REFERENCE
STATION = 0.00



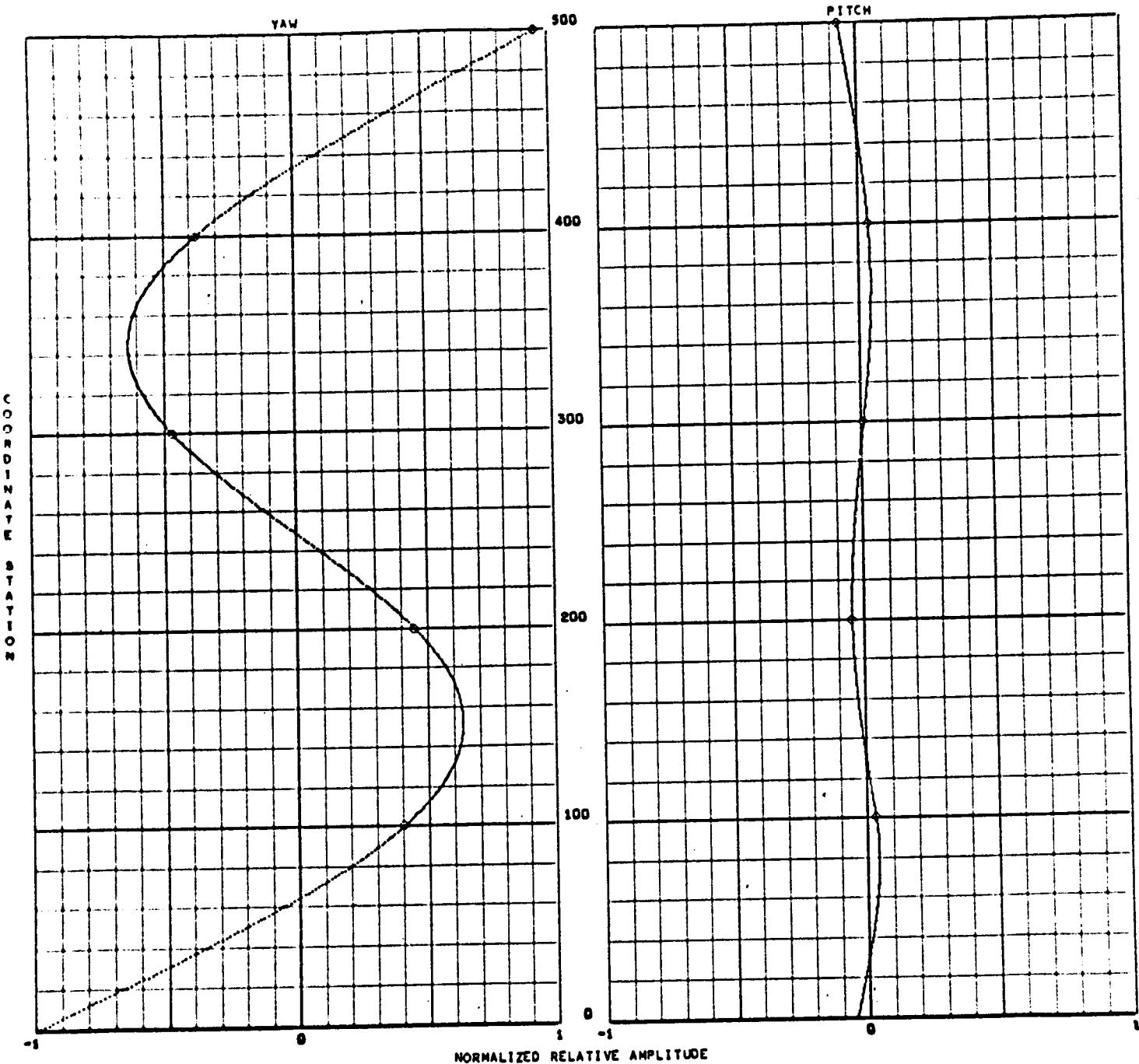
VEHICLE REFERENCE
 STATION = 200.00

470100
009 000

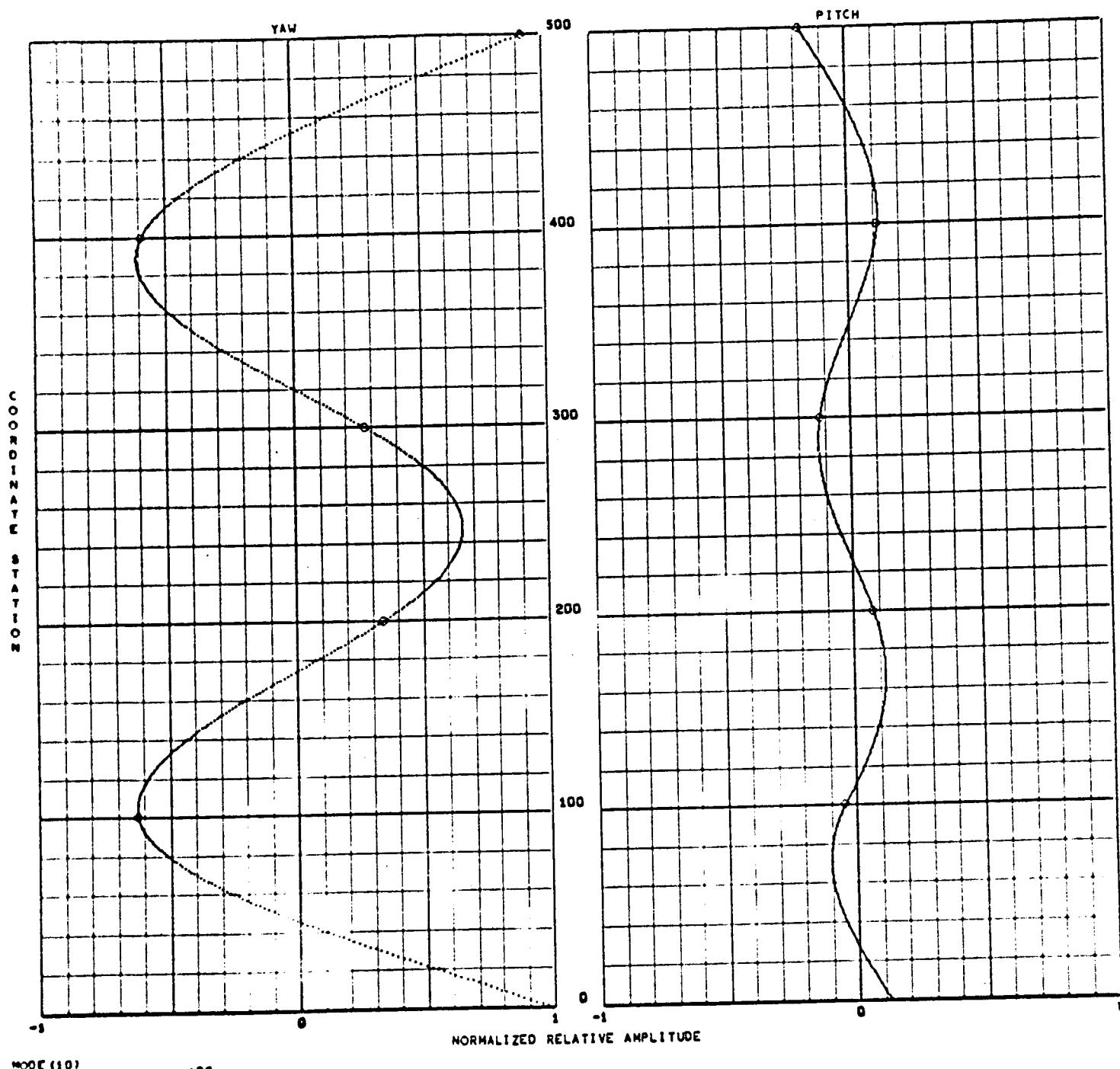
VEHICLE REFERENCE
STATION # 400.00

470100
011 000

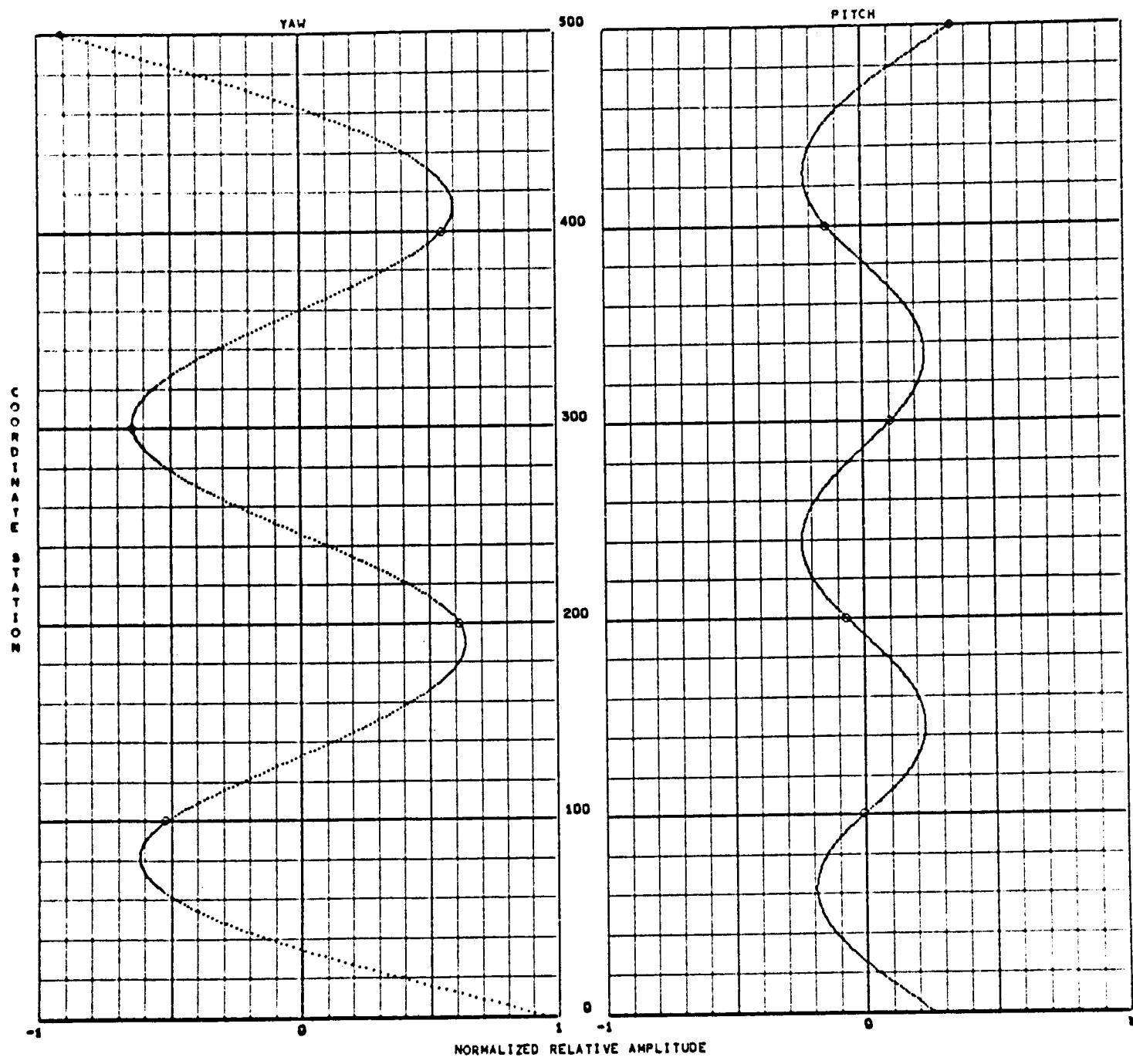
MODE 1 (6)
FREQUENCY = 0.026×10^{-3}

470100
013 000

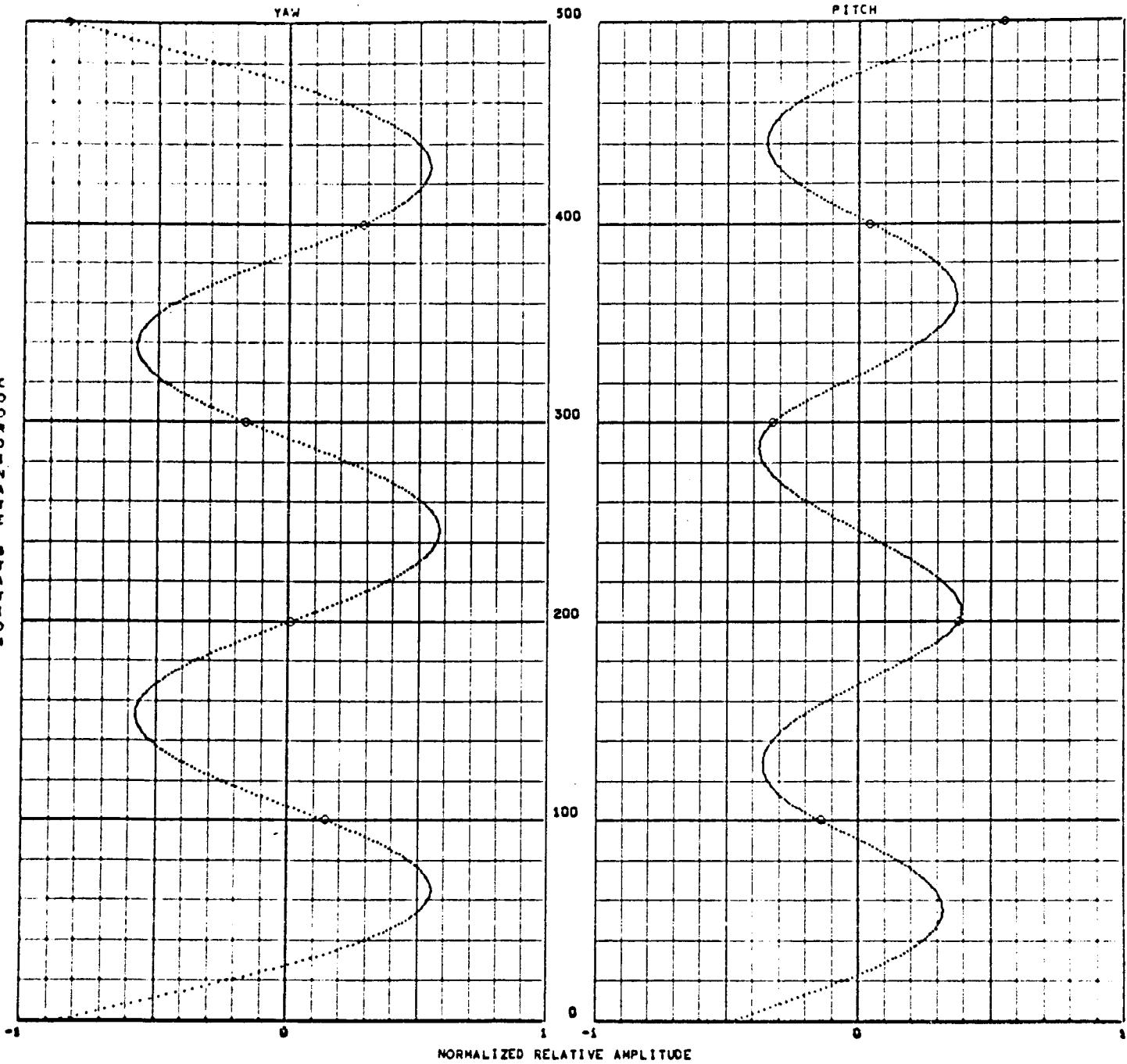
MODE (8)
FREQUENCY = 2.413×10^00

470100
015 000

MODE (10)
FREQUENCY = 4.679×10^{-6}

470100
017 000 L

MODE (12)
- FREQUENCY = 7.690×10^{-00}

470100
019 000

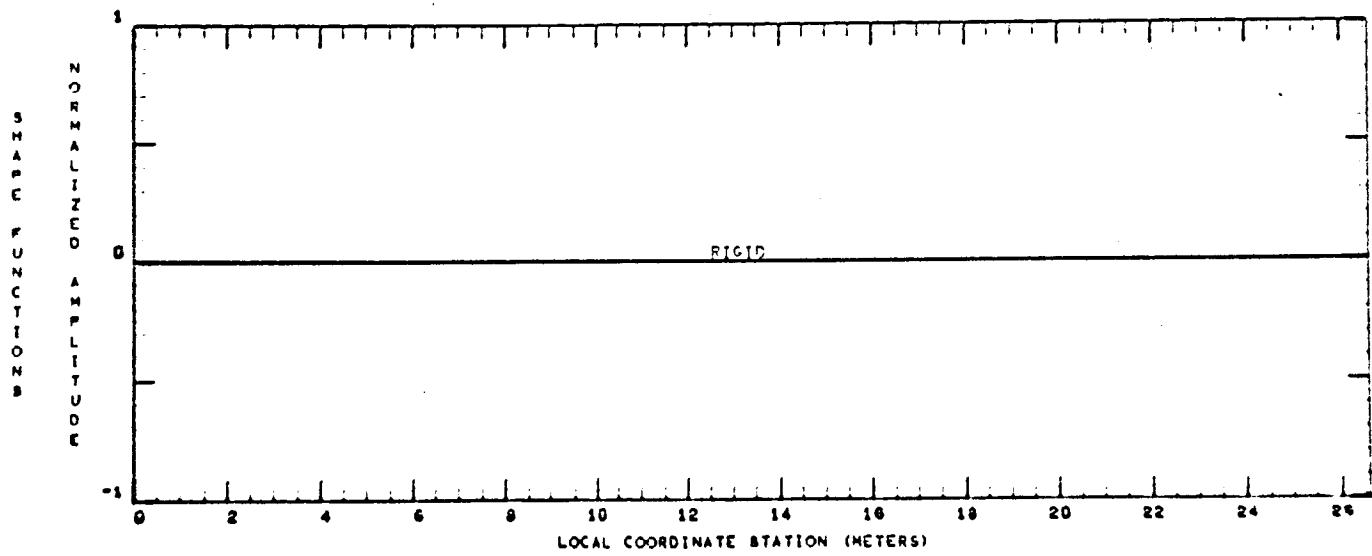
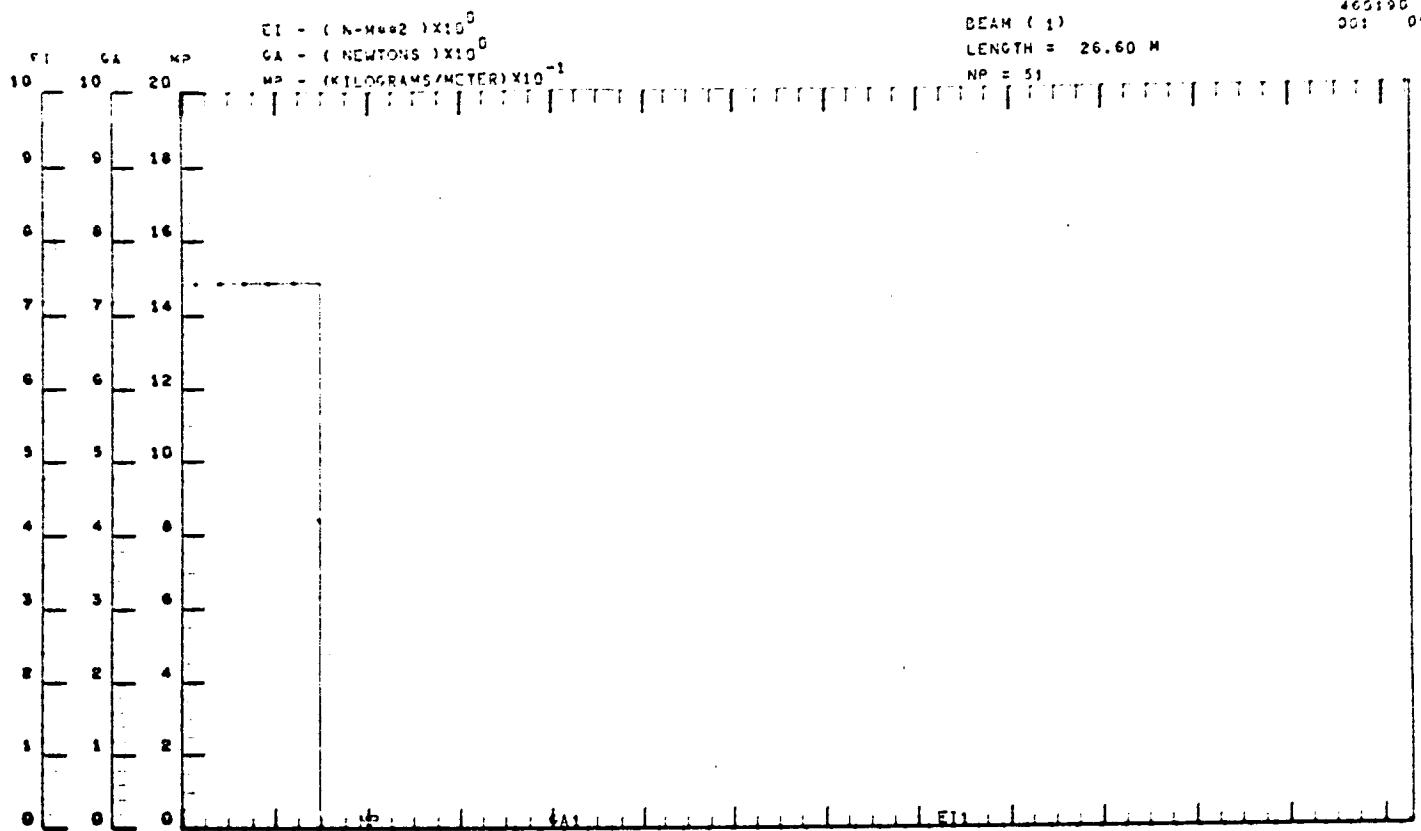
PROBLEM NO. 3

DESCRIPTION: SA-202D upper stages (free-free). This symmetrical vehicle was modeled as seven beams, each butted together with zero-length interstages. The interstage moment-rotation spring constants for the zero-length interstages were large (i.e., about 4 orders of magnitude larger than characteristic EI/L terms), so that the vehicle was in effect modeled as a continuous Timoshenko beam. The standard set of displacement functions, as described in Section 3.2.1, was used so that the model involved 56 degrees of freedom, 28 in each plane. Since the program computed a sequence of "identical" pairs of modes (one in the pitch plane, one in the yaw), only one member of each such pair is included here. The purpose of this analysis was to compare the solution obtained with this (in effect) 28-degree-of-freedom analysis with a very nearly exact* solution of the same Timoshenko beam analysis calculated by the NASA-Stodola program (Reference 2). The results are summarized below. The figures listed parenthetically are those calculated by the NASA-Stodola program.

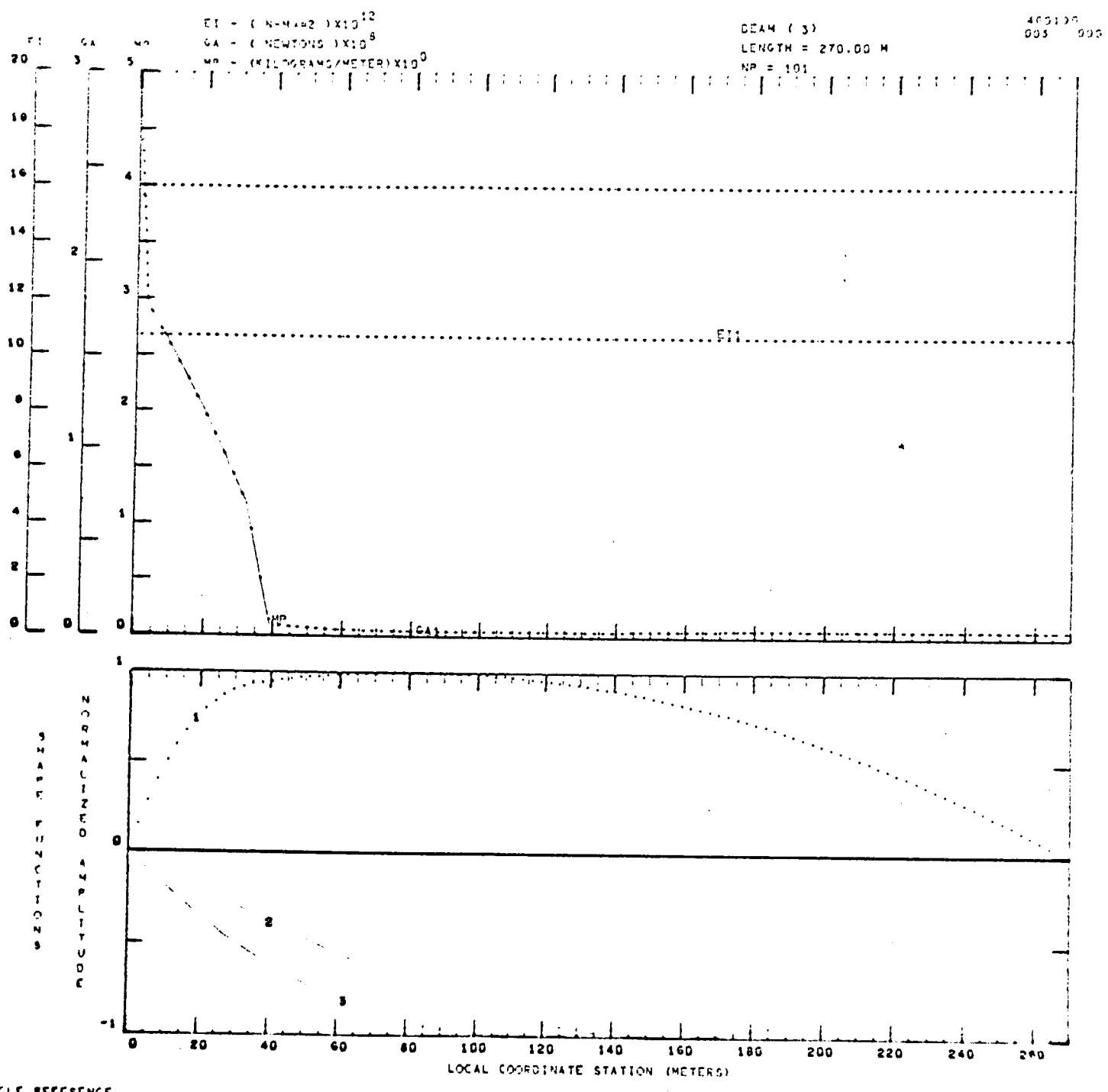
**SUMMARY OF
RESULTS:**

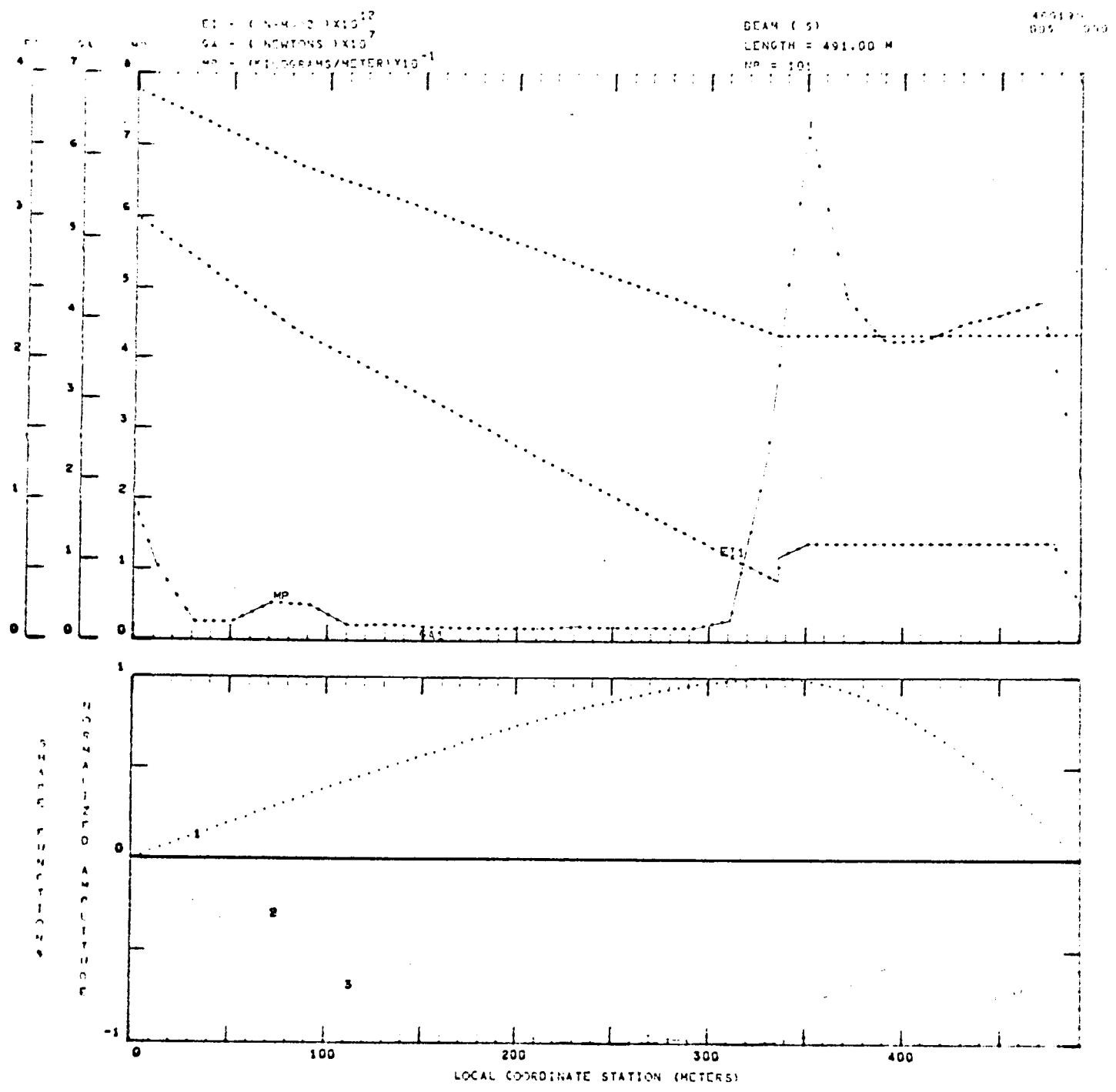
Mode	Frequency (cps)	Generalized Mass ($lb\cdot sec^2/in.$)
1	2.47 (2.44)	8.14 (8.18)
2	4.46 (4.35)	9.24 (9.68)
3	7.04 (6.92)	25.66 (22.06)
4	11.47 (11.26)	24.89 (27.85)
5	15.75 (- -)	8.42 (- -)

*By "exact," we mean here (and in similar cases discussed later) exact solutions to the finite representation of the Timoshenko beam problem, rather than the exact solution to the continuum problem approximated by the finite model.

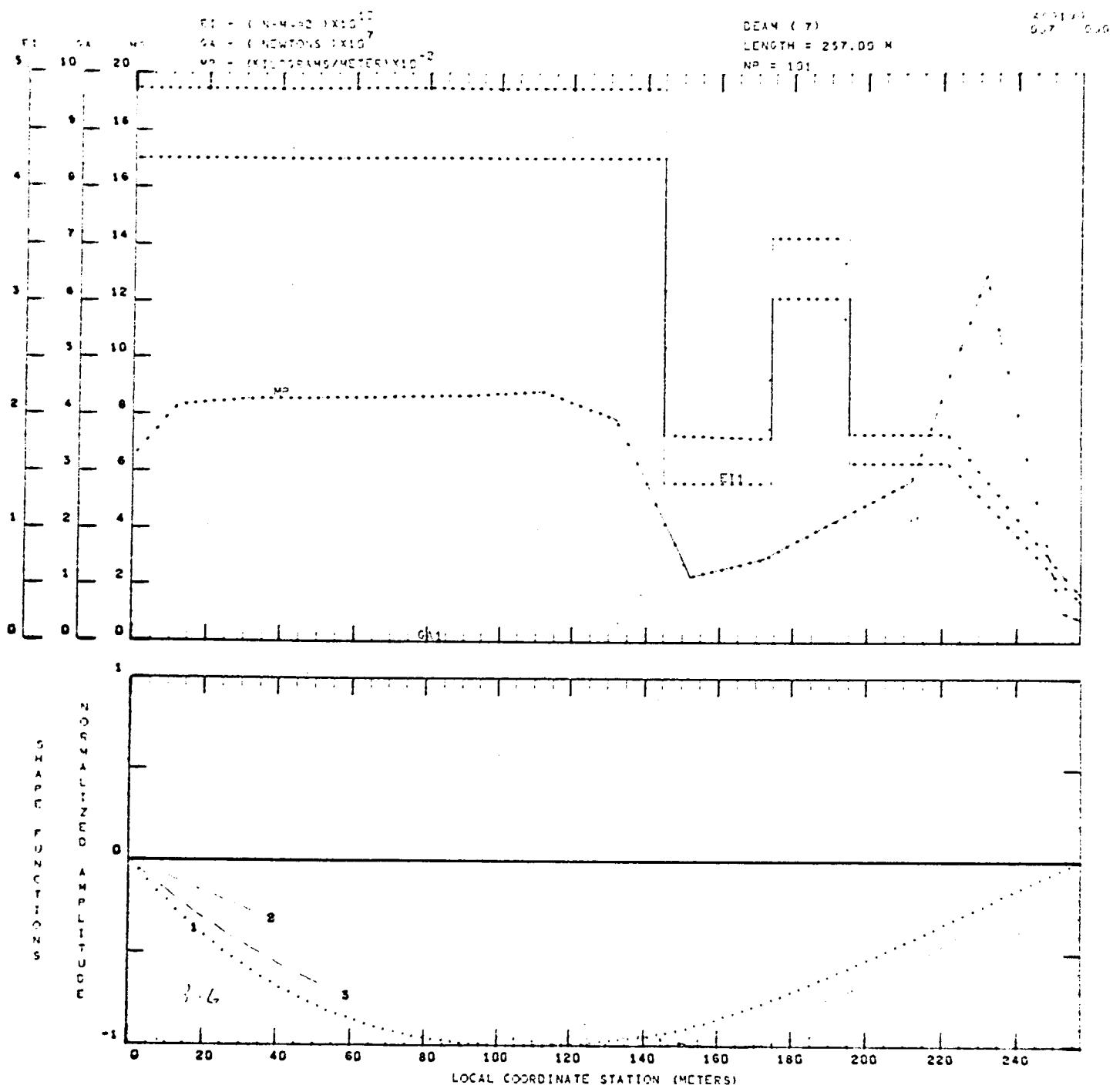
465190
001 000

VEHICLE REFERENCE
STATION # = 32.50



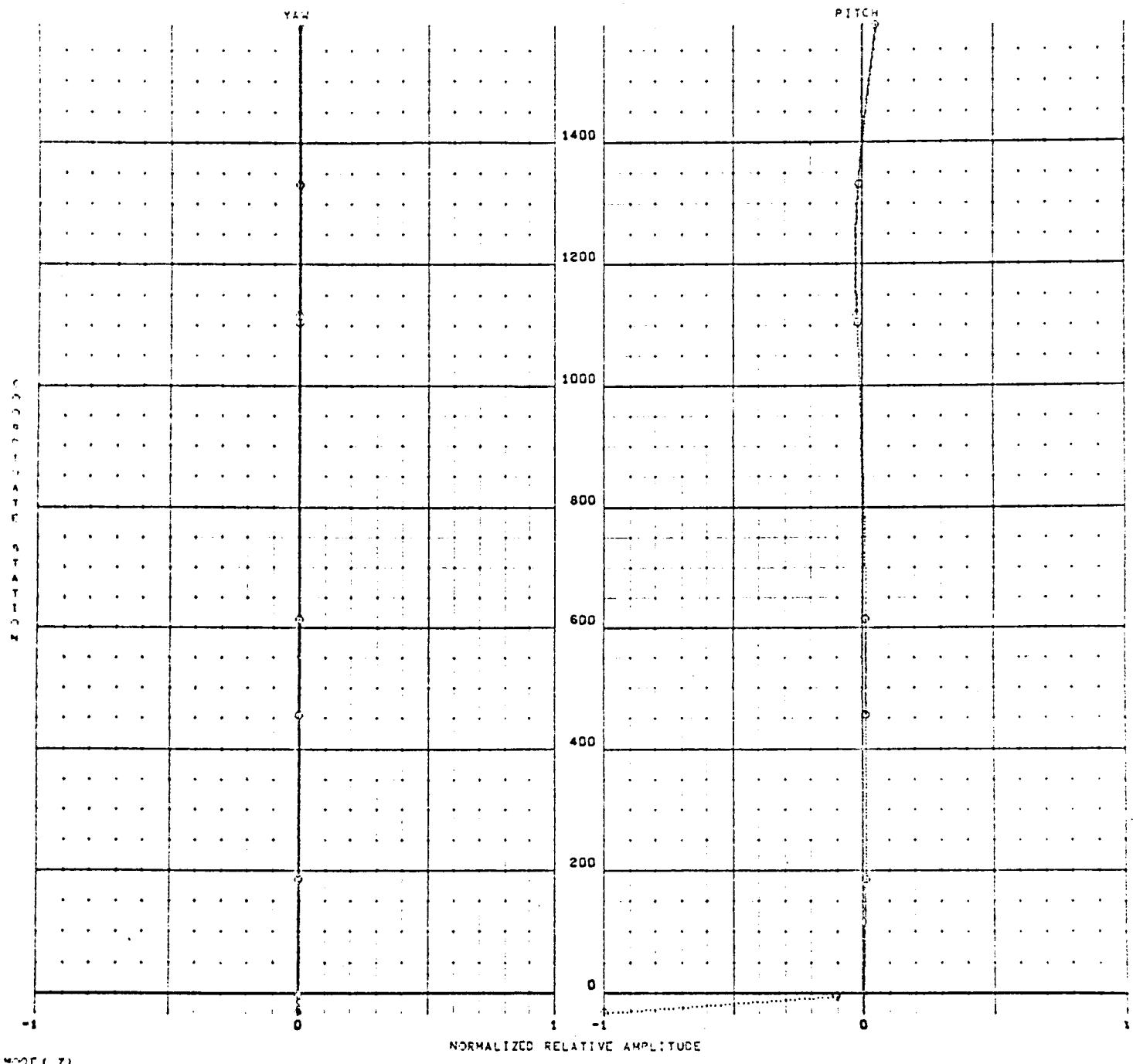


VEHICLE REFERENCE
STATION X = 614.00

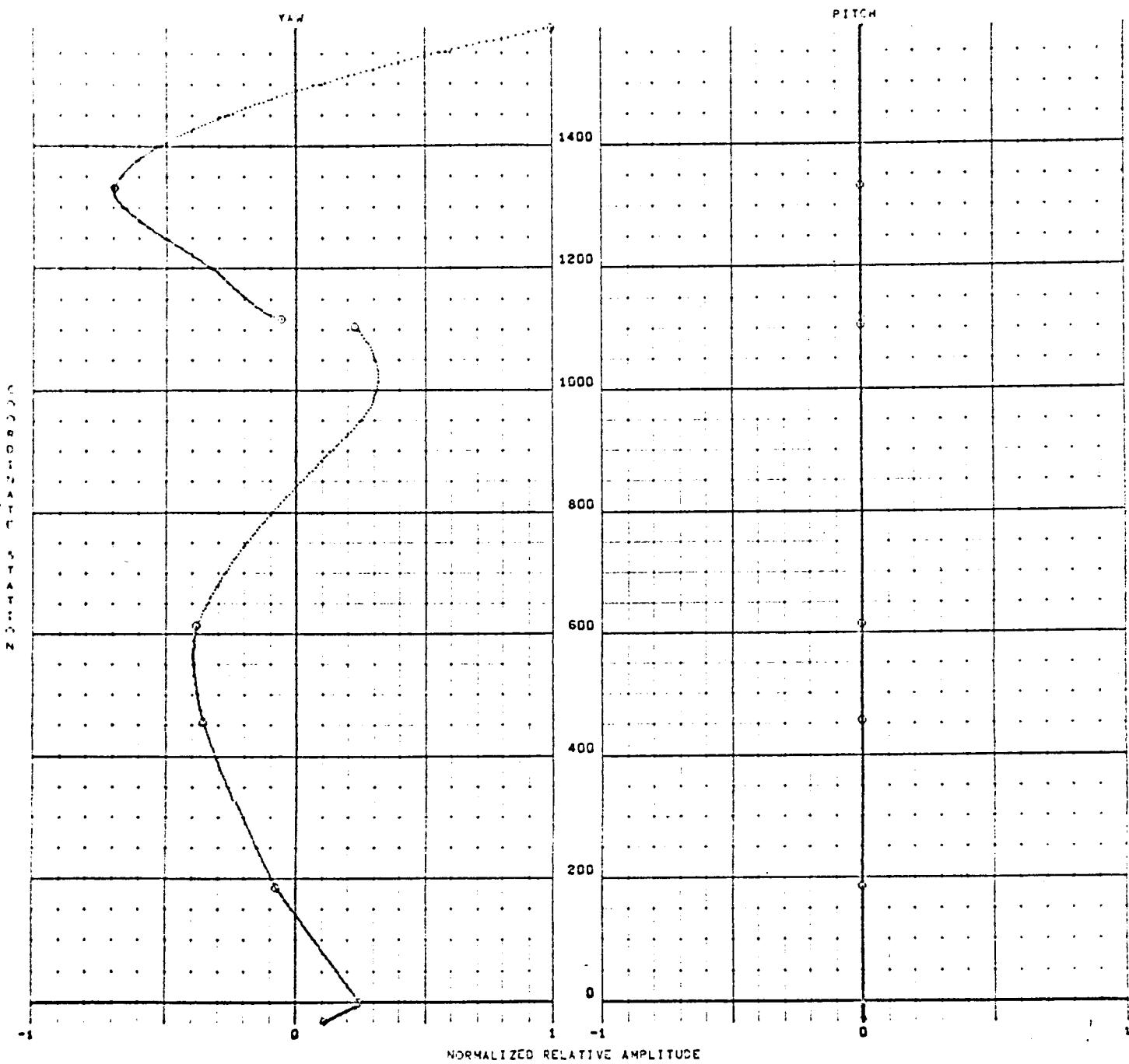


LMSC/HREC A783589

460195
014 000



MODE (7)
FREQUENCY = 4.455×10^{-6}

469196
018 001

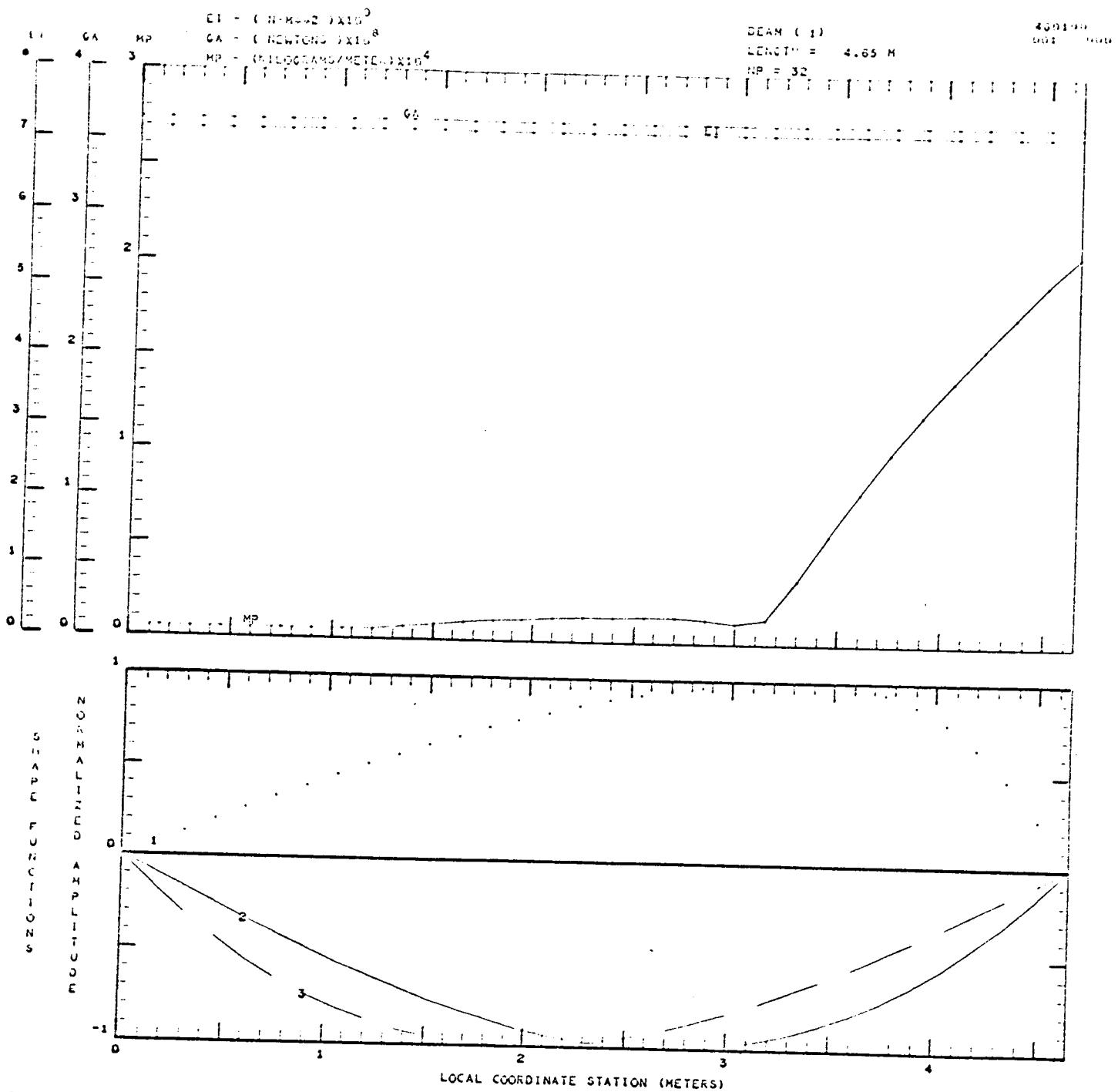
MODE (11)
FREQUENCY = 1.147×10^{10}

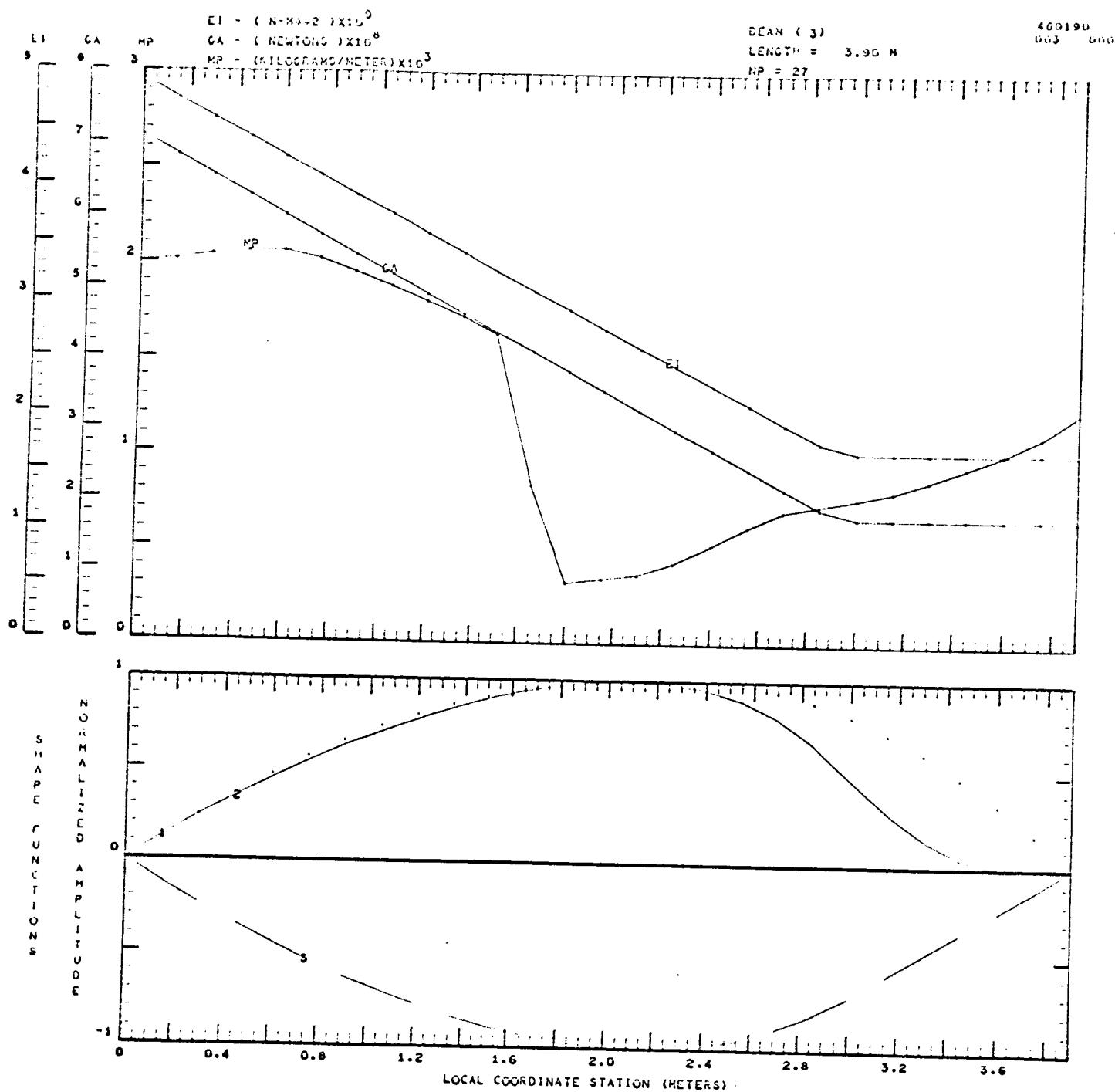
PROBLEM NO. 4

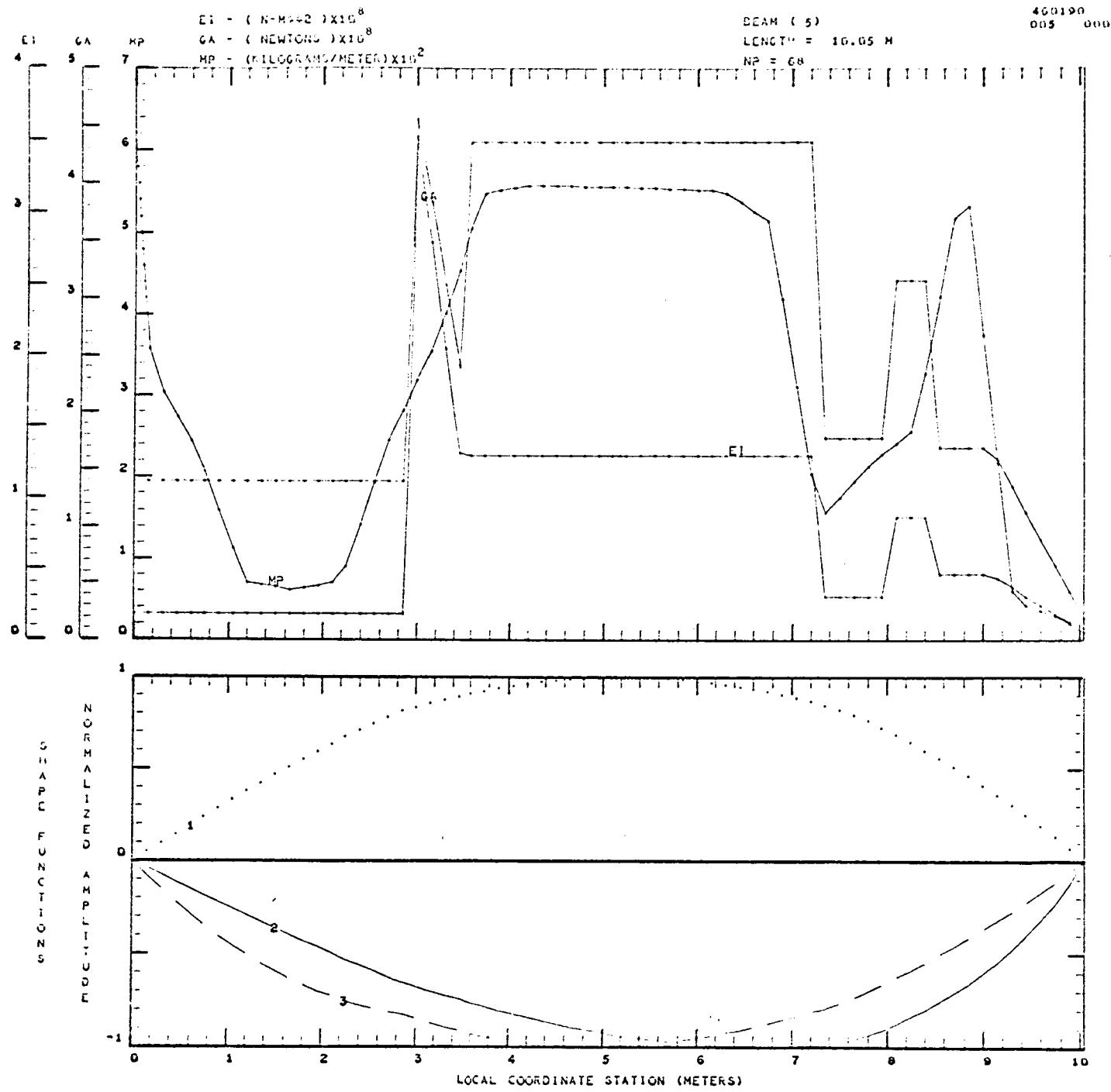
DESCRIPTION: SA-D6 upper stages (cantilevered). This symmetrical vehicle is modeled as five beams, each, in effect, butted rigidly together as described in Problem No. 3. As in Problem No. 3, the purpose of this analysis was to compare the results of the analysis of a highly non-uniform symmetrical beam with the nearly exact results of the same problem executed by the NASA-Stodola program. In both programs, the detailed mathematical models (e.g., the locations of the 227 "station" boundaries used in the numerical integrations, etc.) are essentially identical, so that the differences in the results are due to the fact that the present analysis involves only 21 degrees of freedom compared to 554 degrees of freedom (227 displacements and 227 rotations) in the Stodola program. In the table of results presented below, the results of the NASA-Stodola program are listed parenthetically. It is evident that the consequences of the artificial restraints introduced, in effect, by the reduction from 554 to 21 degrees of freedom is slight.

**SUMMARY OF
RESULTS:**

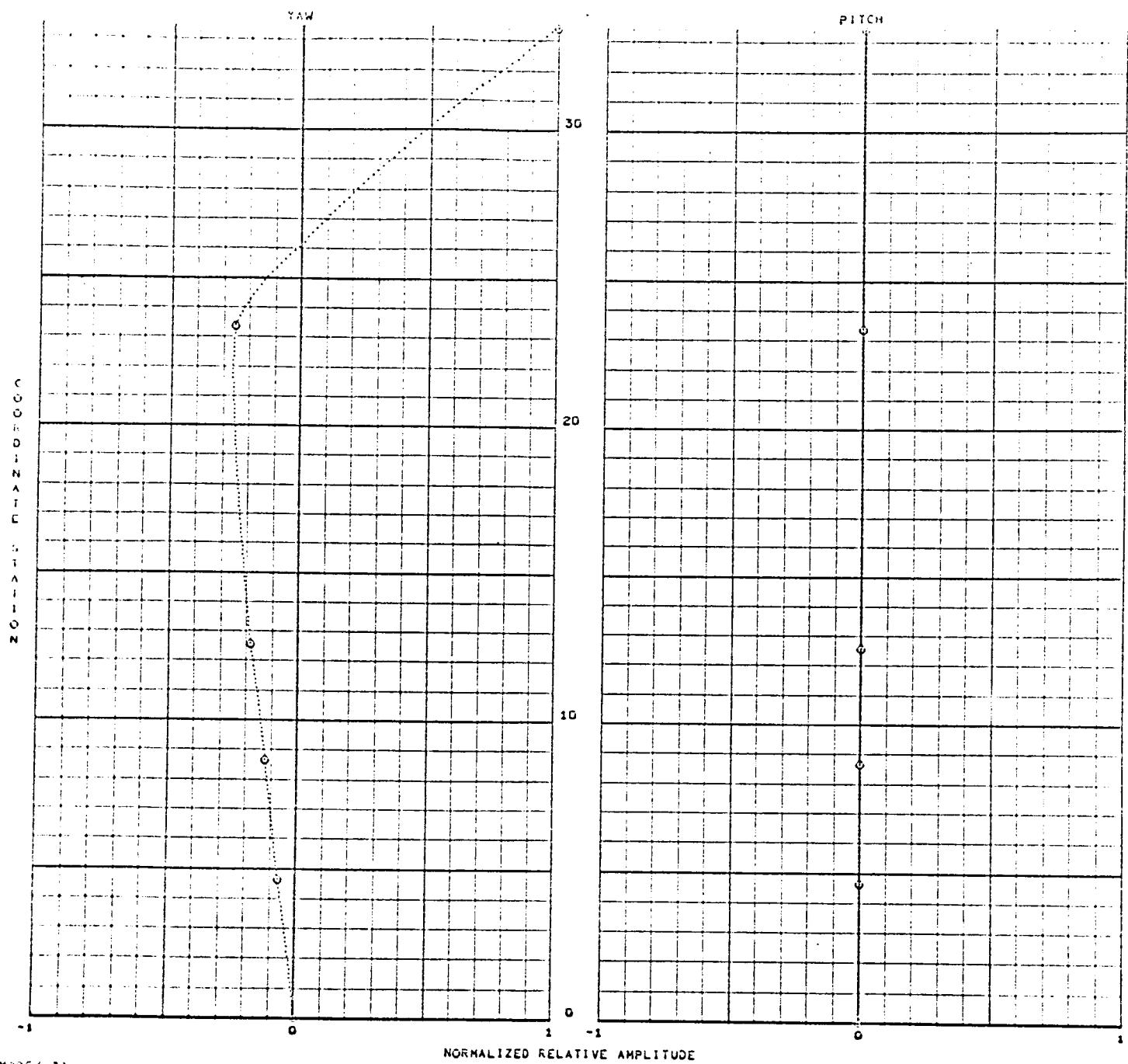
Mode	Frequency (cps)	Generalized Mass (kg)
1	1.588 (1.584)	2507 (2614)
2	3.93 (3.87)	1505 (1262)
3	6.45 (6.40)	4376 (4906)
4	14.56 (- -)	(- -)

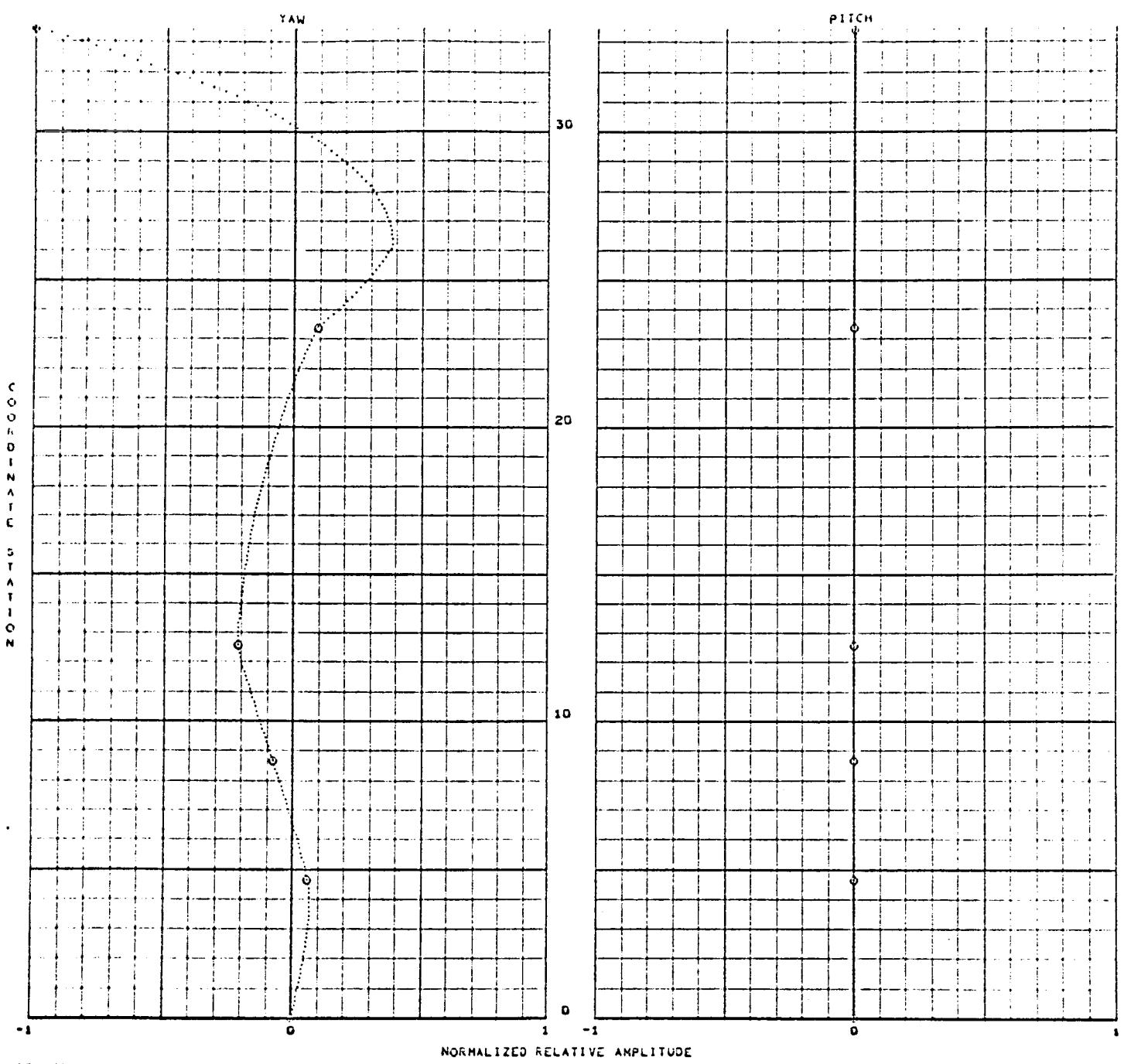






VEHICLE REFERENCE
STATION = 23.40

460190
008 0..0

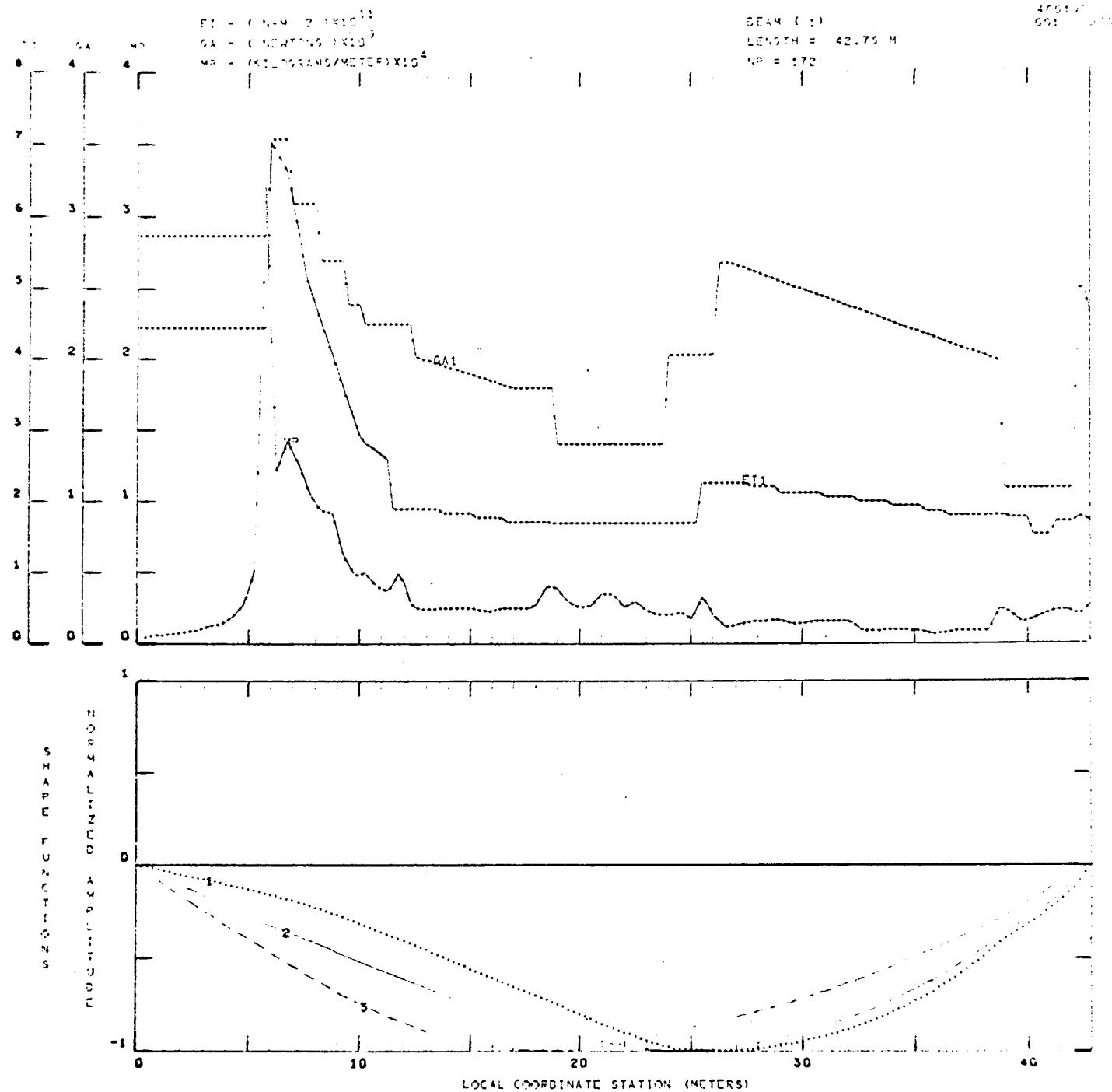
460190
012 000

PROBLEM NO. 5

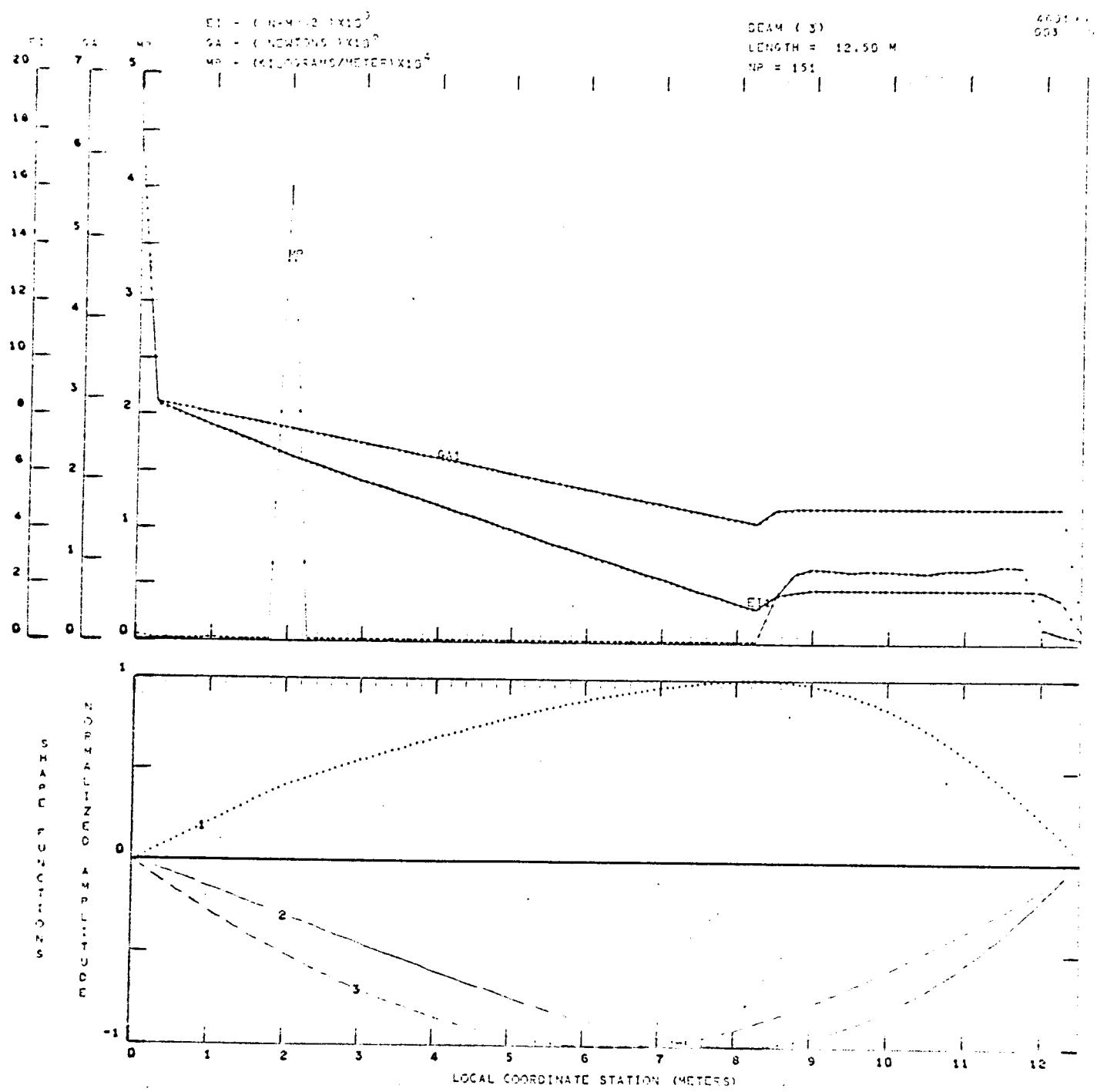
DESCRIPTION: Unfueled SA-501 (free-free). This rotationally symmetrical vehicle is modeled as four tandem Timoshenko beams rigidly butted together as in the two preceding problems. The results obtained in this analysis are shown below with the corresponding results of the NASA-Stodola program listed parenthetically.

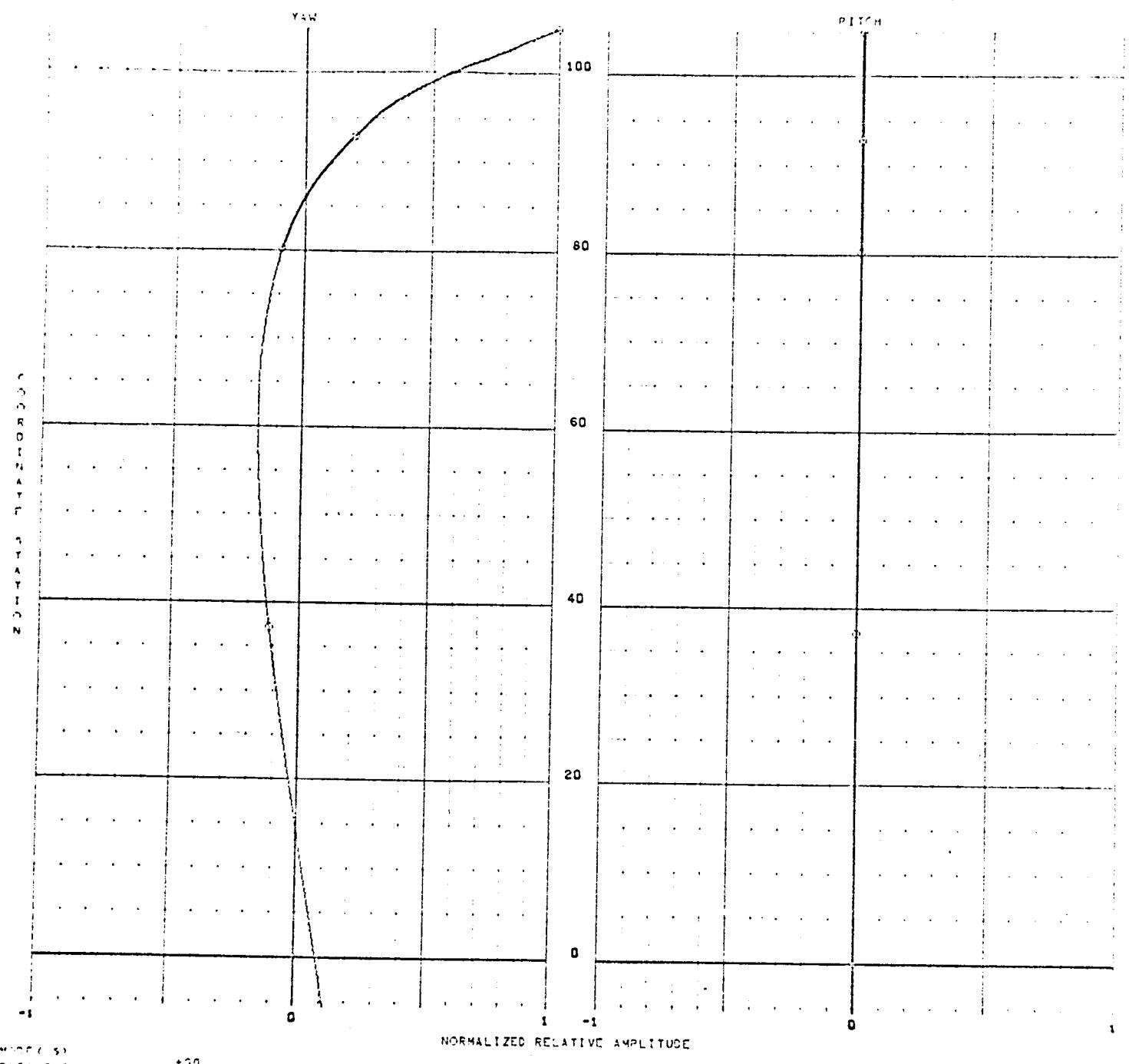
**SUMMARY OF
RESULTS:**

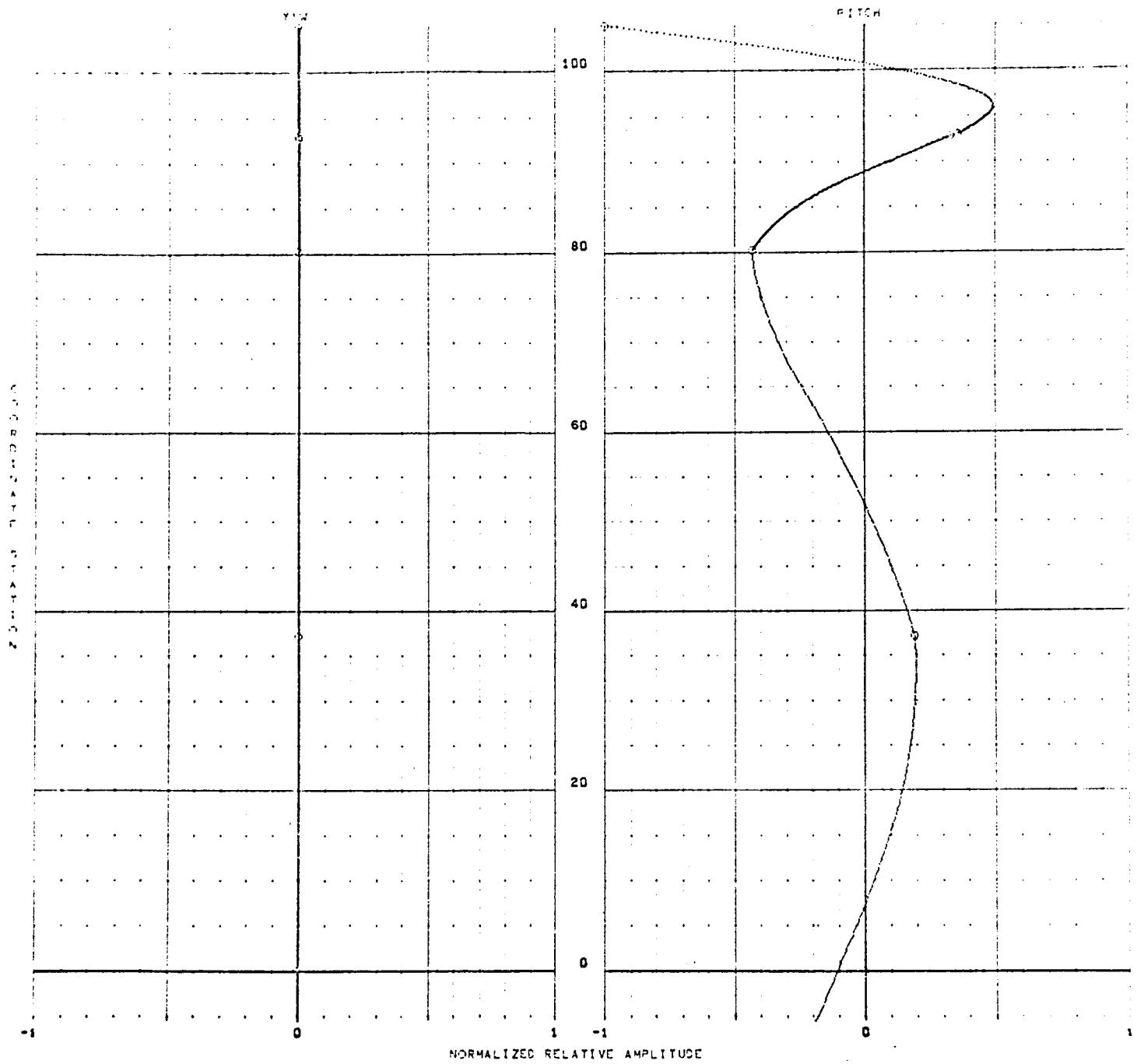
Mode	Frequency (cps)	Generalized Mass (kg)
1	1.583 (1.558)	4425 (4242)
2	2.65 (2.59)	2330 (2393)
3	5.04 (4.84)	8576 (10,027)
4	8.51 (7.99)	- - - (9067)



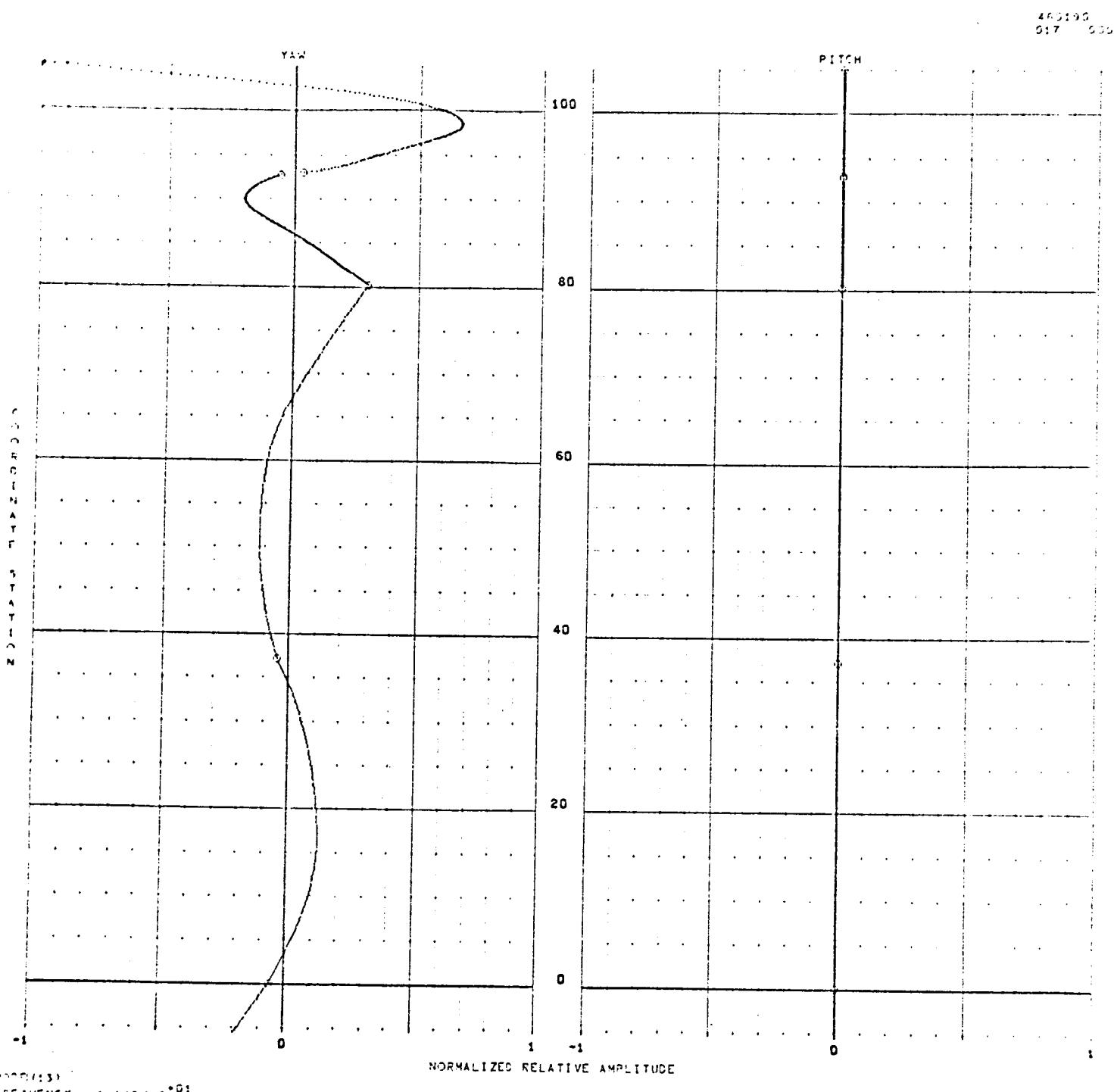
VEHICLE REFERENCE
STATION = 5.50





400120
913 002

X 000000
frequency = 5.036×10^{-9}

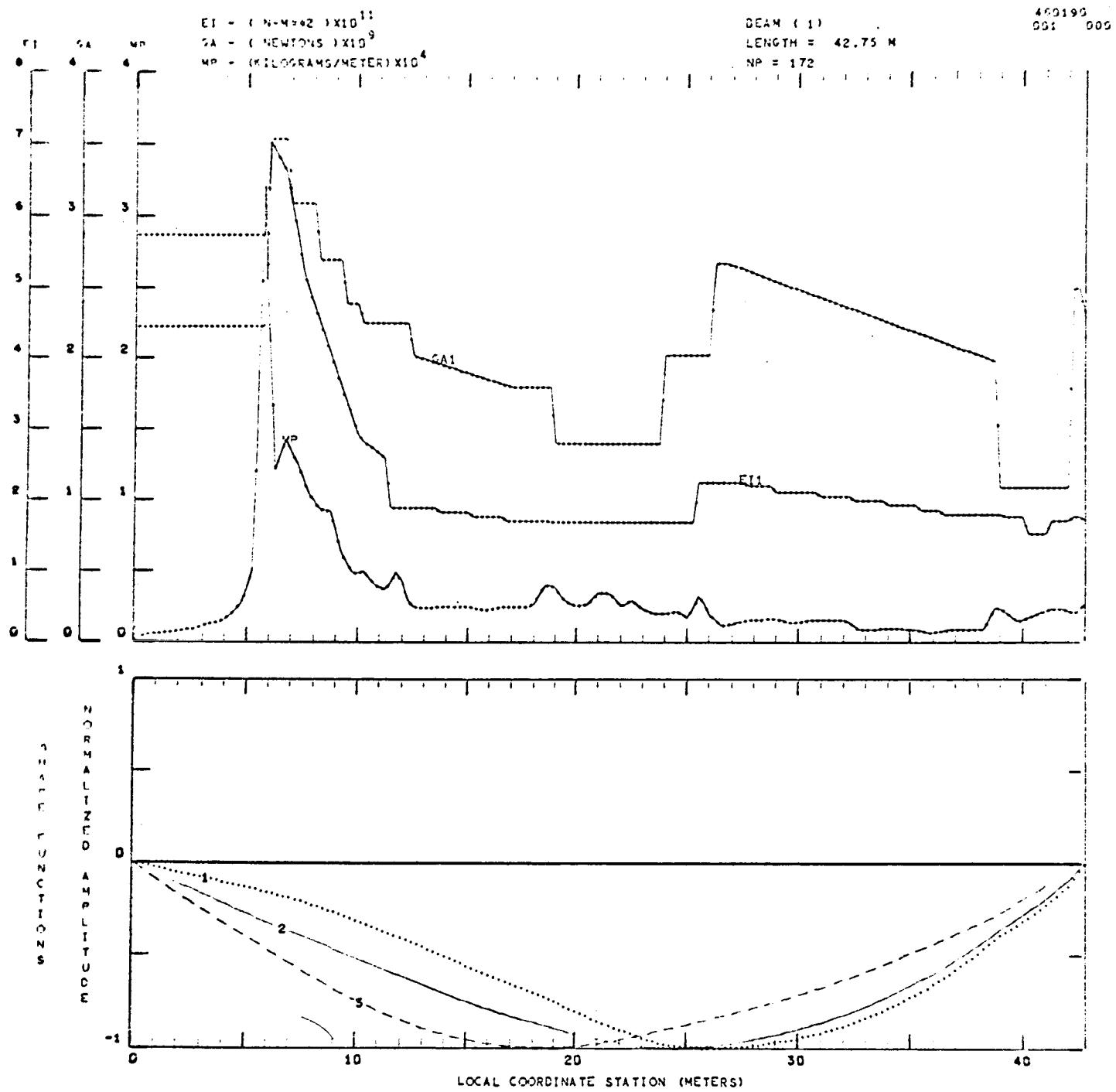


PROBLEM NO. 6

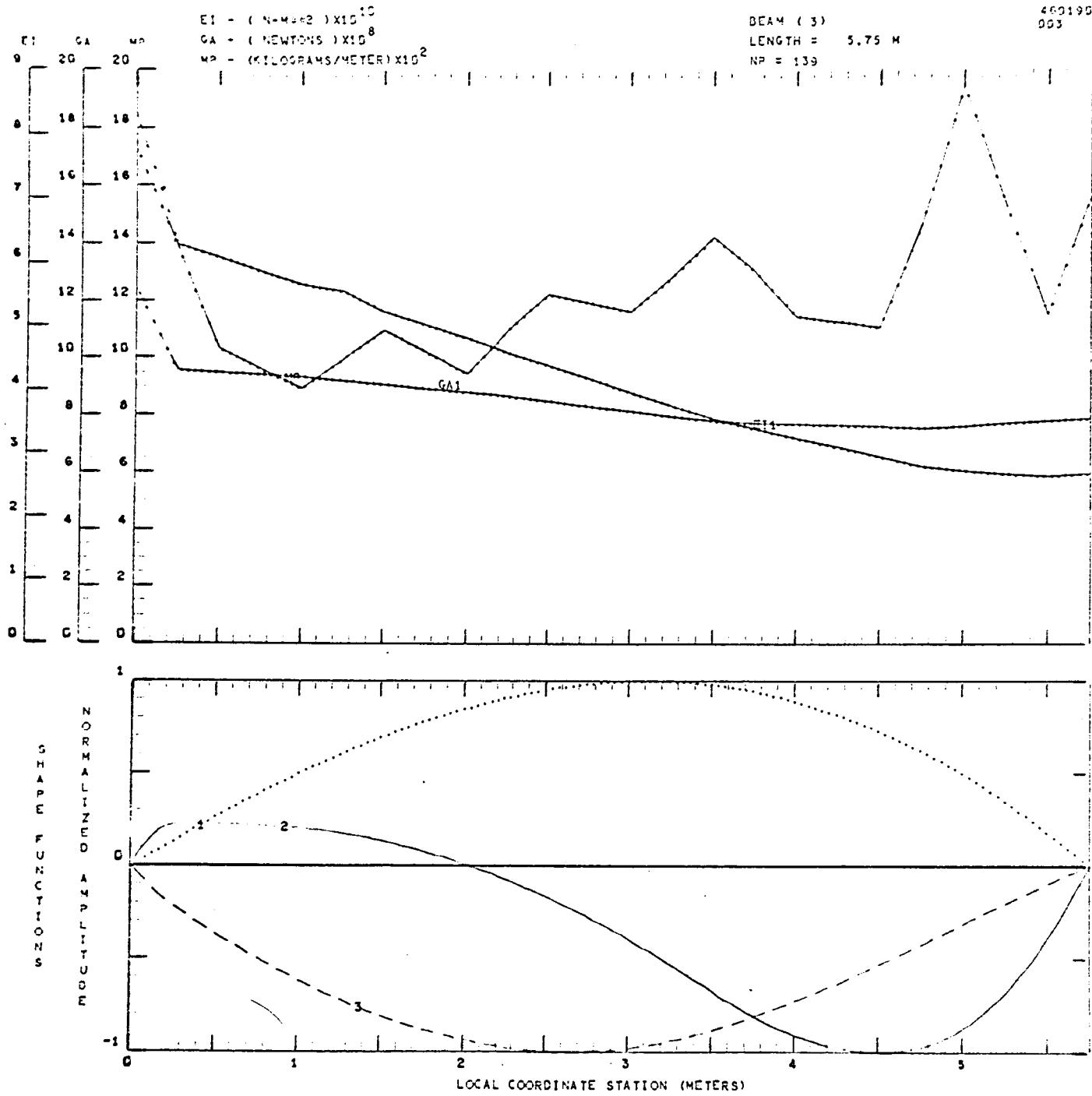
DESCRIPTION: Unfueled SA-501 (free-free). This is the same vehicle analyzed in Problem No. 5, except that in this case, it is modeled as six beams rather than four. As before, the NASA-Stodola program results are listed parenthetically in the summary of results presented below. Comparison of these results with those of Problem No. 5 indicates a typical improvement in solution accuracy associated with increasing the number of beams used in the model.

**SUMMARY OF
RESULTS:**

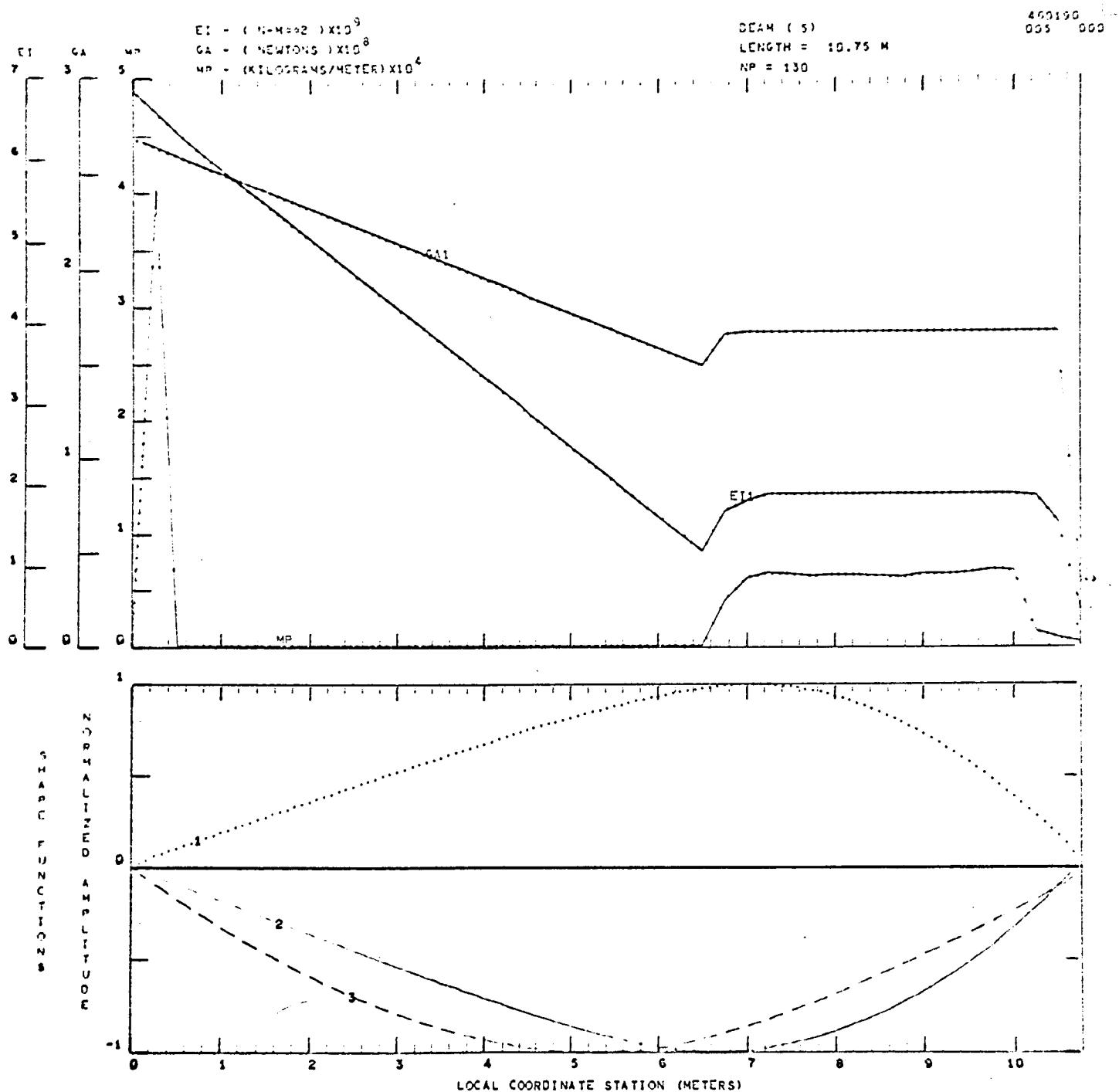
Mode	Frequency (cps)	Generalized Mass (kg)
1	1.577 (1.558)	4471 (4242)
2	2.65 (2.59)	2320 (2393)
3	4.95 (4.84)	8999 (10,027)
4	8.41 (7.99)	- - (9067)



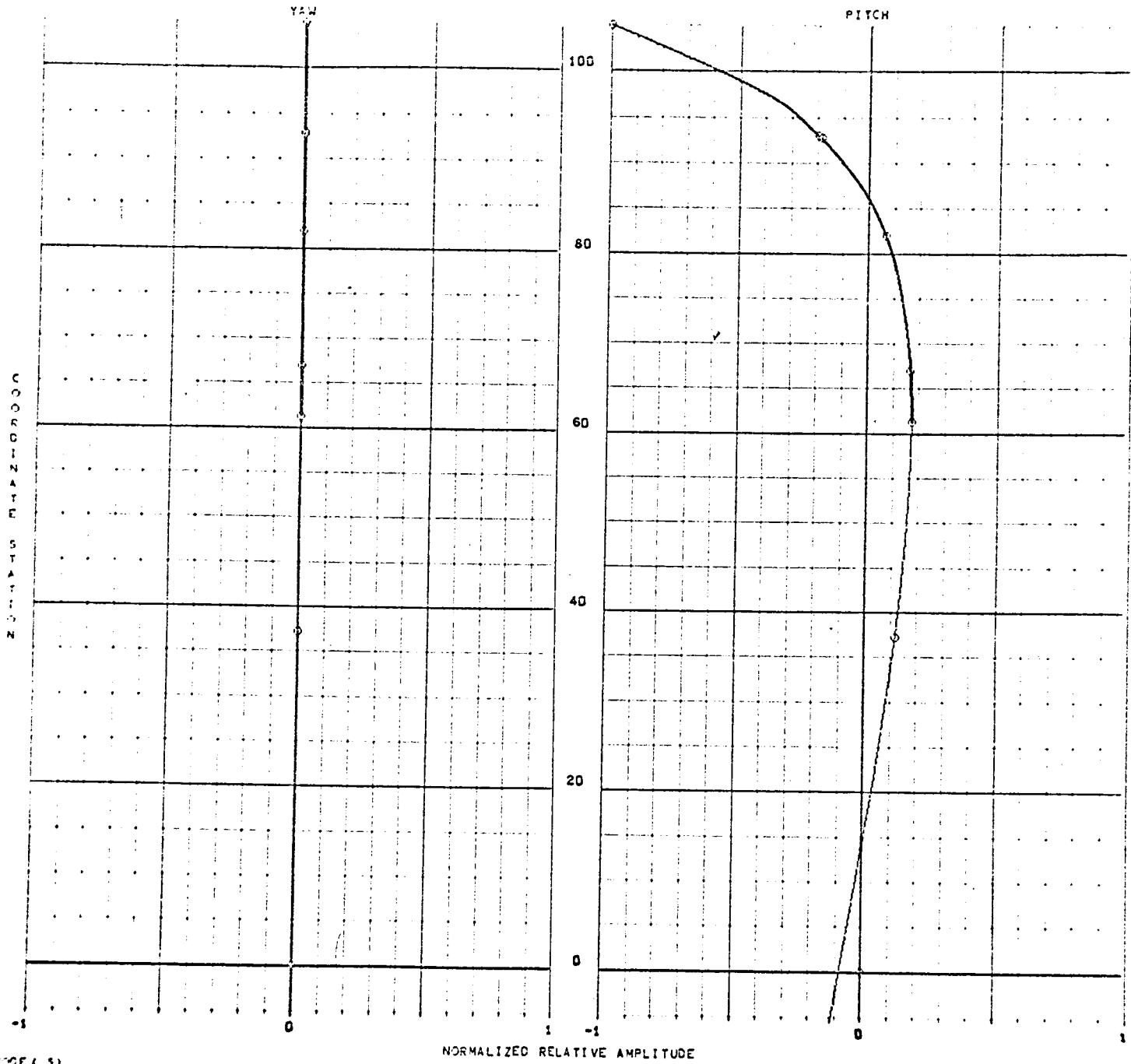
FILE REFERENCE
 TON = 5.50

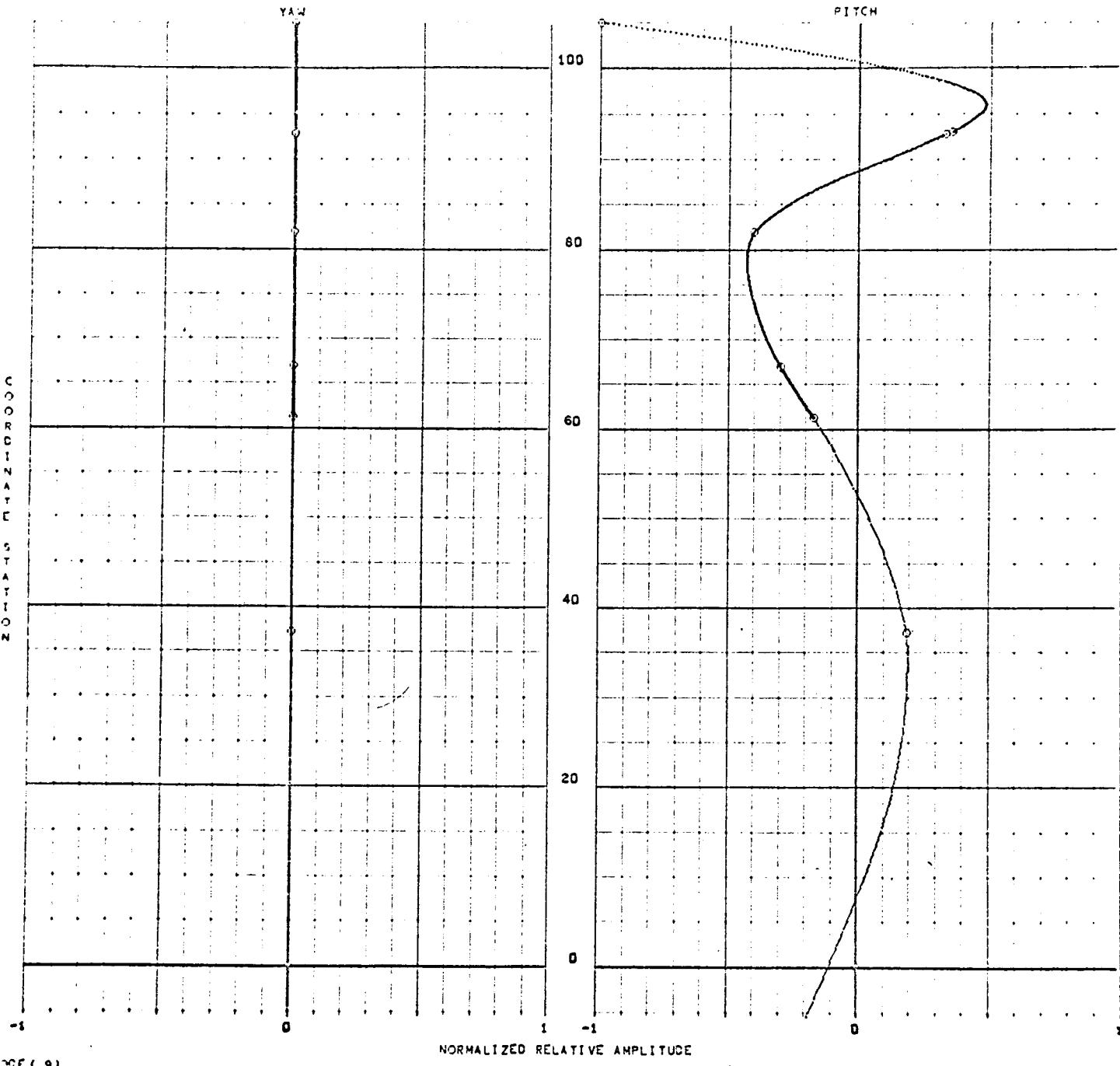
469195
003 000

VEHICLE REFERENCE
 STATION = 61.25



VEHICLE REFERENCE
STATION # 02.00

460190
011 505MODE (S)
FREQUENCY = 1.576×10^{-3}

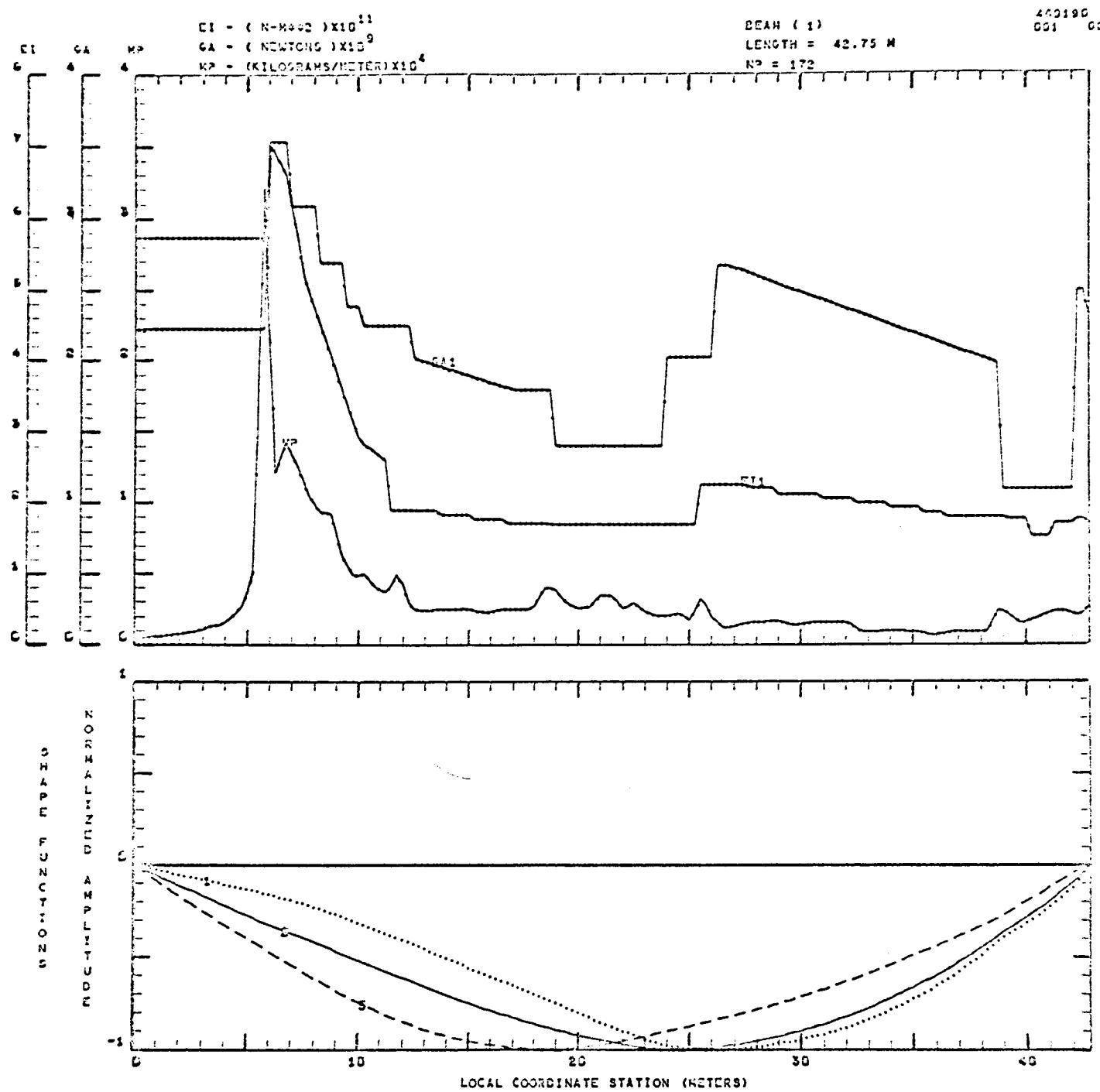
400:90
015 000

PROBLEM NO. 7

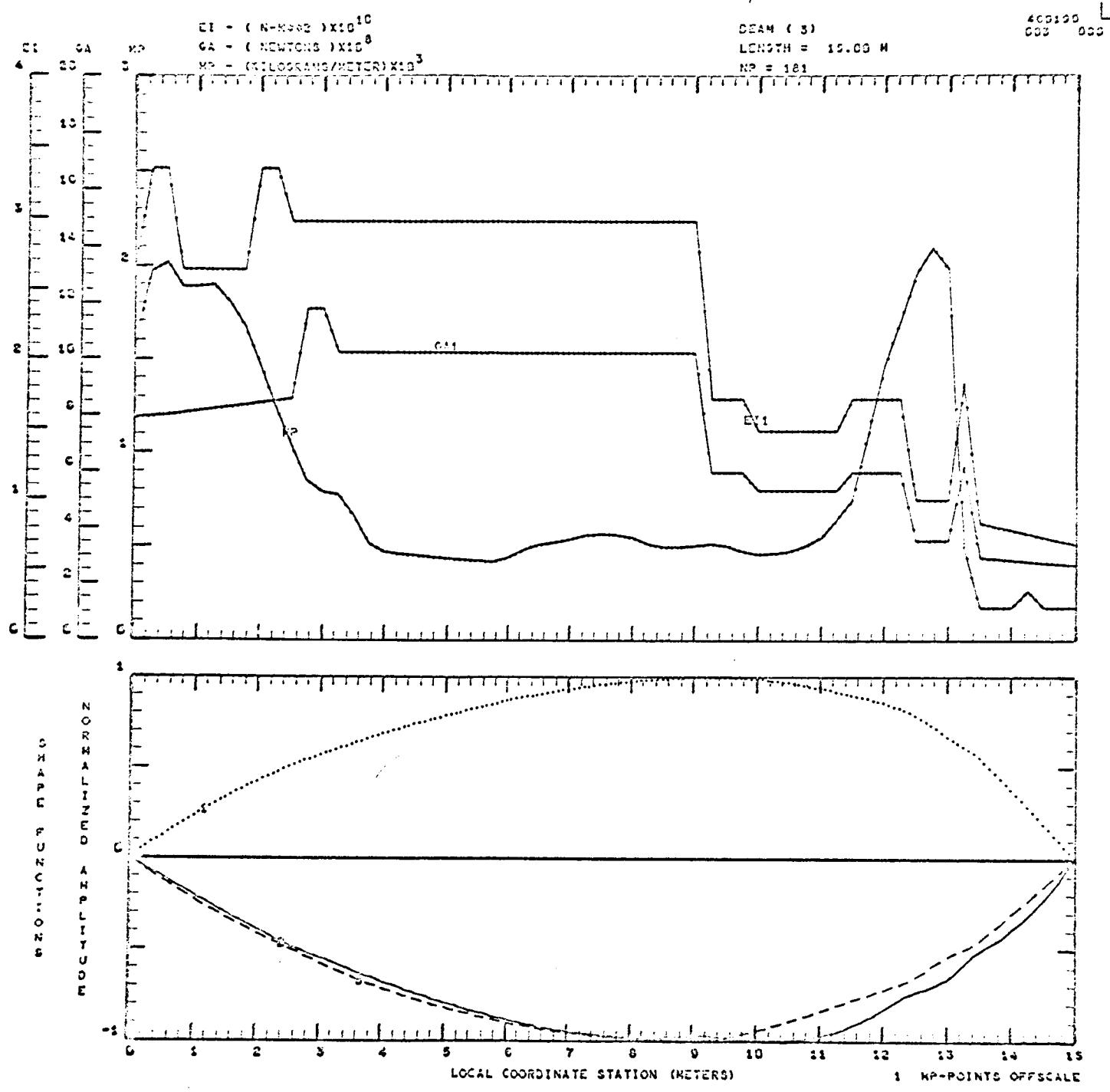
DESCRIPTION: Unfueled SA-501 (free-free). This analysis employs exactly the same mathematical model as Problem No. 6 except that the S-II/S-IVB interstage (which was modeled as one of the six Timoshenko beams in Problem No. 6) is, in this case, modeled as a massless interstage of the type discussed in Section 2.4.2. Accordingly, the present model contains only five beams. The (quasi-static) stiffness matrix characterizing the S-II/S-IVB interstage was calculated using Timoshenko beam theory. As before, the NASA-Stodola program results are listed parenthetically with the summary of results given below.

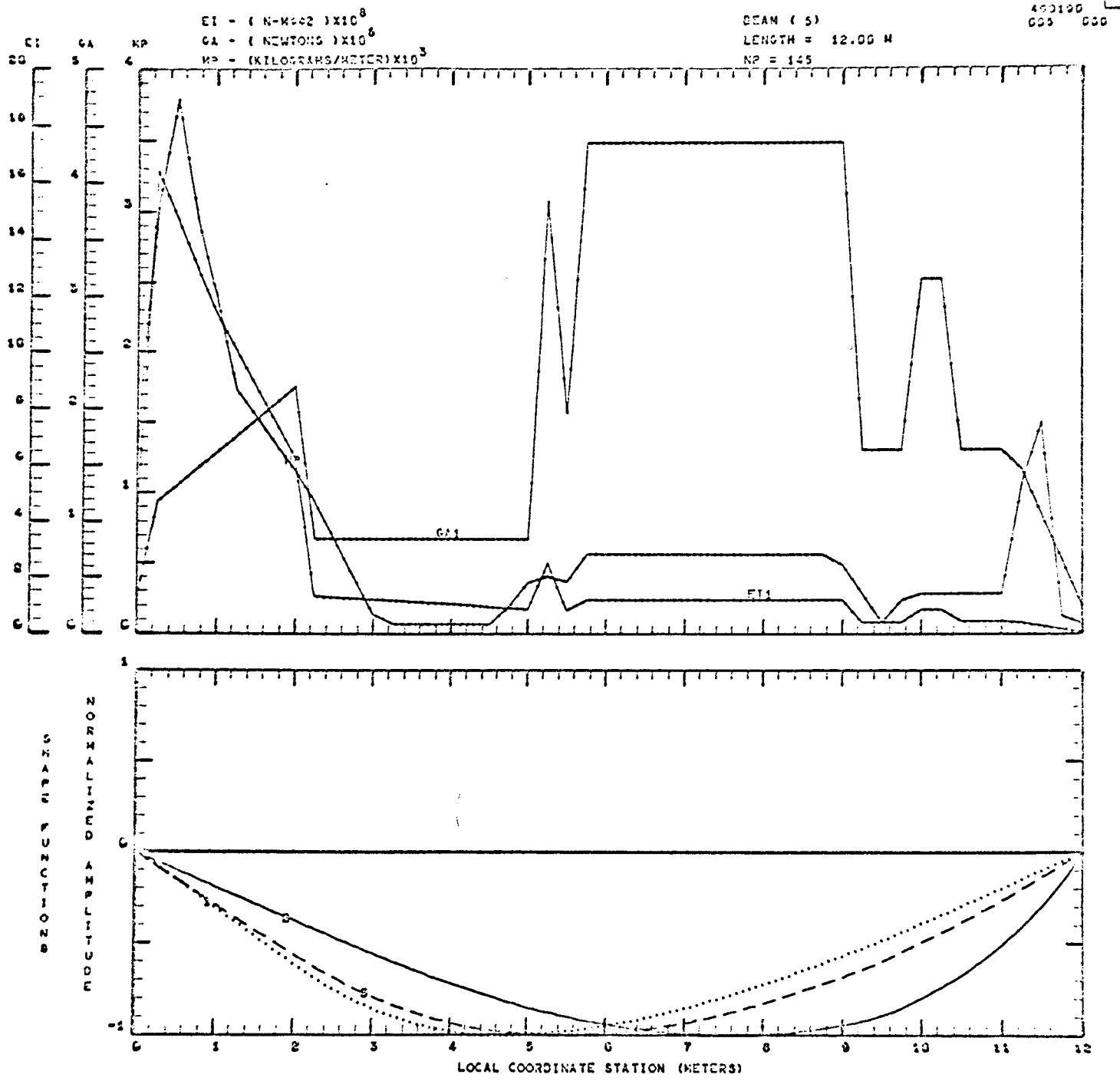
**SUMMARY OF
RESULTS:**

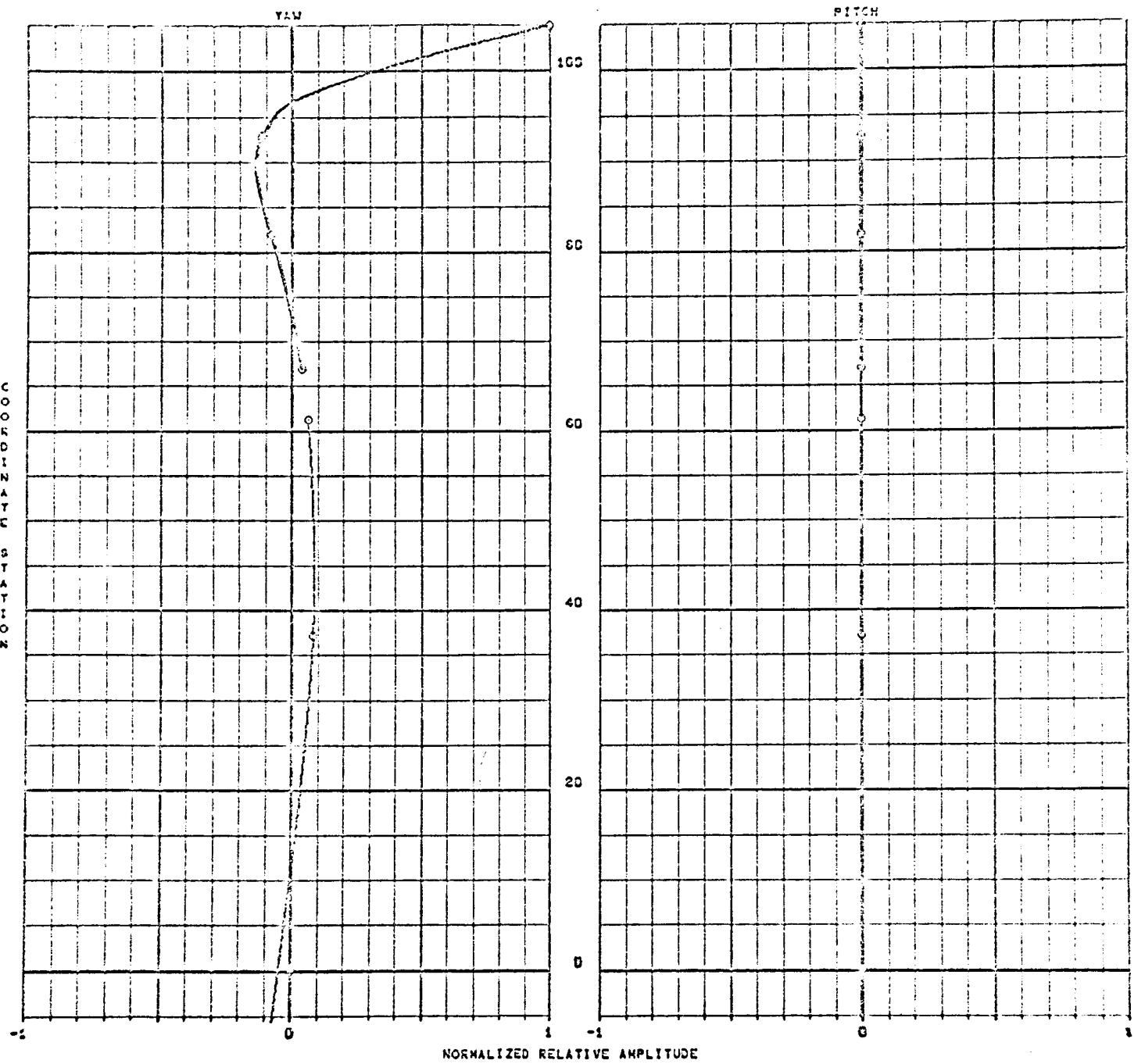
Mode	Frequency (cps)	Generalized Mass (kg)
1	1.573 (1.558)	4506 (4242)
2	2.65 (2.59)	2310 (2393)
3	4.93 (4.84)	9255 (10,027)
4	8.21 (7.99)	- - (9067)



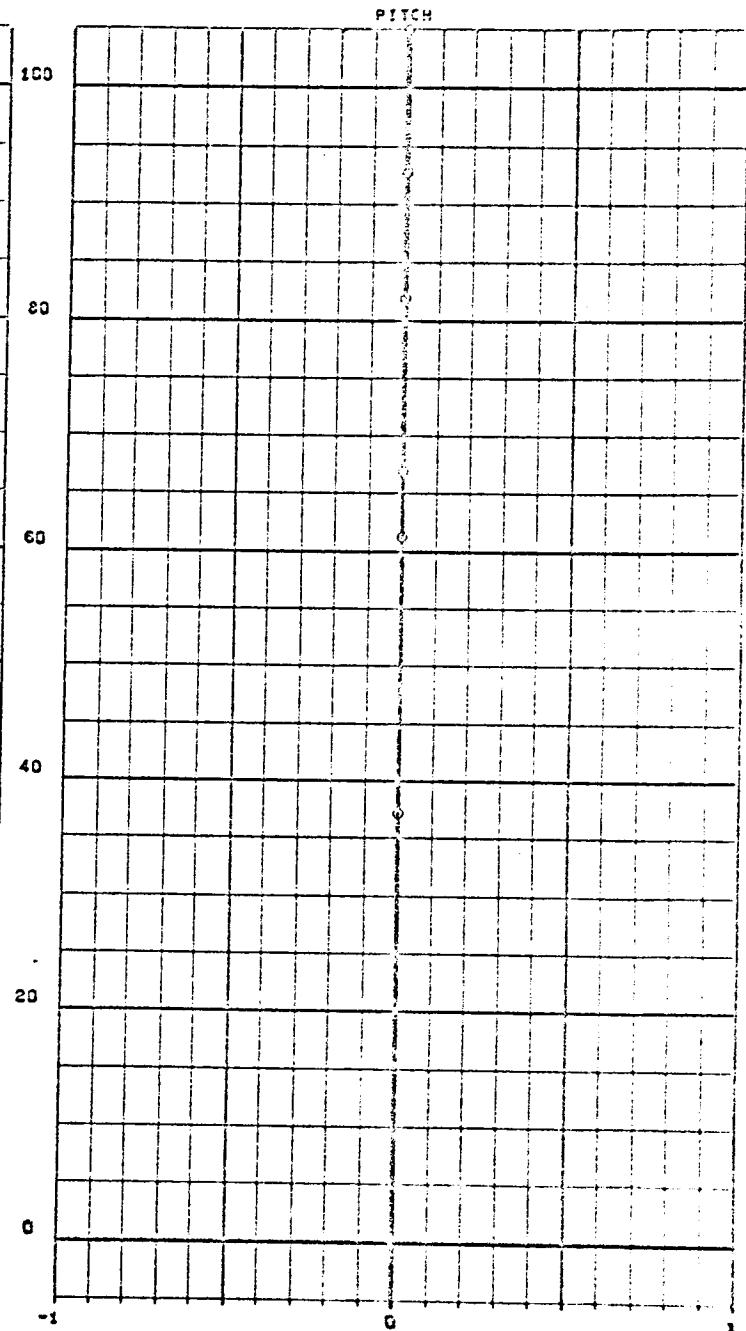
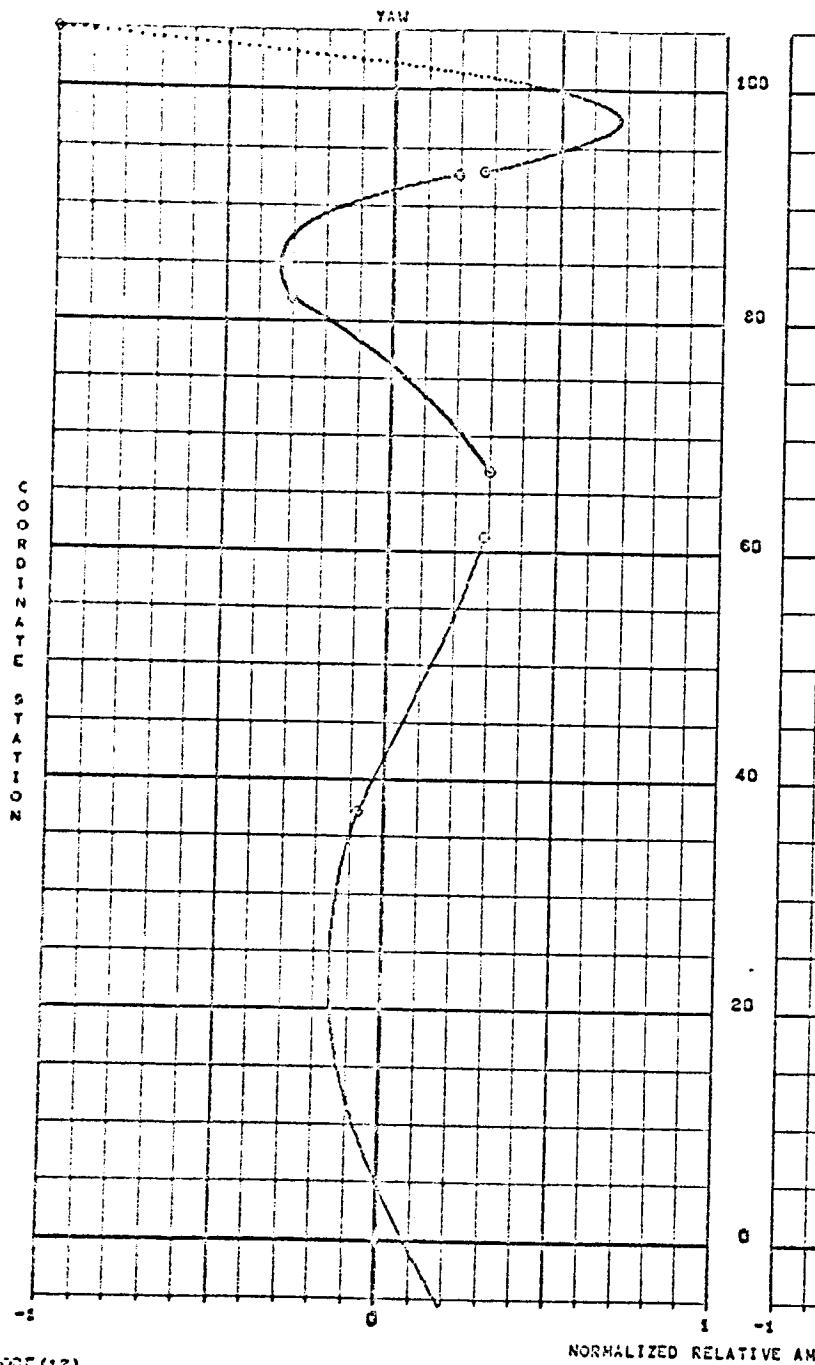
VEHICLE REFERENCE
STATION # = 5.50





400100
615 000

MODE (8)
FREQUENCY = 2.647×10^0

400193
017 000

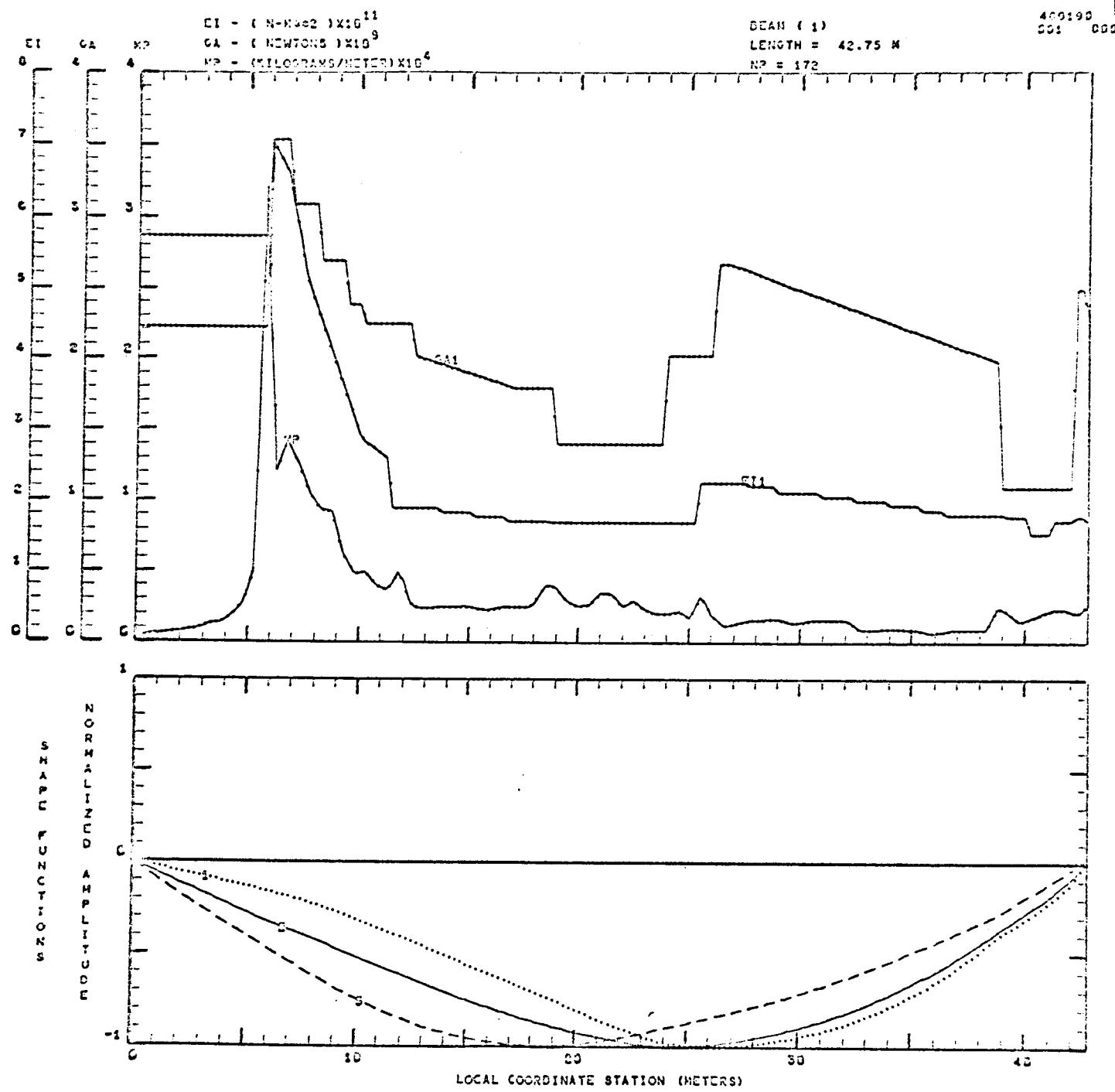
NOTE (12)
FREQUENCY = 8.210×10^{00}

PROBLEM NO. 8

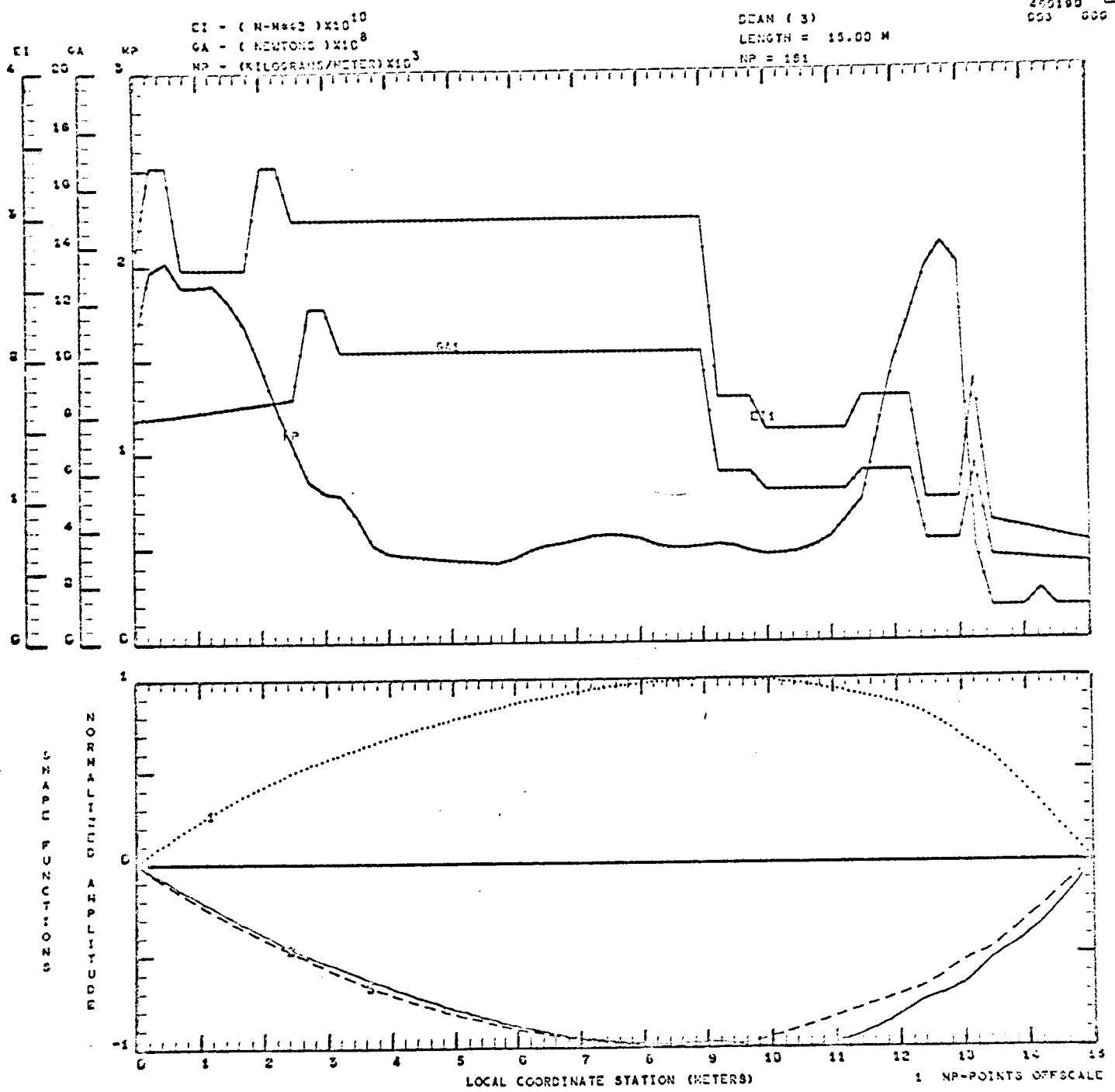
DESCRIPTION: Unfueled SA-501 (free-free). This analysis is identical to the five-beam analysis of Problem No. 7, except that the S-II/S-IVB interstage stiffness matrix was calculated using the Lockheed digital program for static analysis of arbitrary orthotropic linear shells (Reference 3). It is interesting to note that the proportions of this conical interstage are such that the sign of the moment-displacement (and force-rotation) stiffness constant is opposite from that of the corresponding quantity as computed using the Timoshenko beam postulates, and of similar magnitude in absolute value. Accordingly, it is not surprising to find that the results of this analysis differ appreciably from those of Problem No. 7. Again, the NASA-Stodola results for the empty SA-501 are listed parenthetically in the summary presented below.

**SUMMARY OF
RESULTS:**

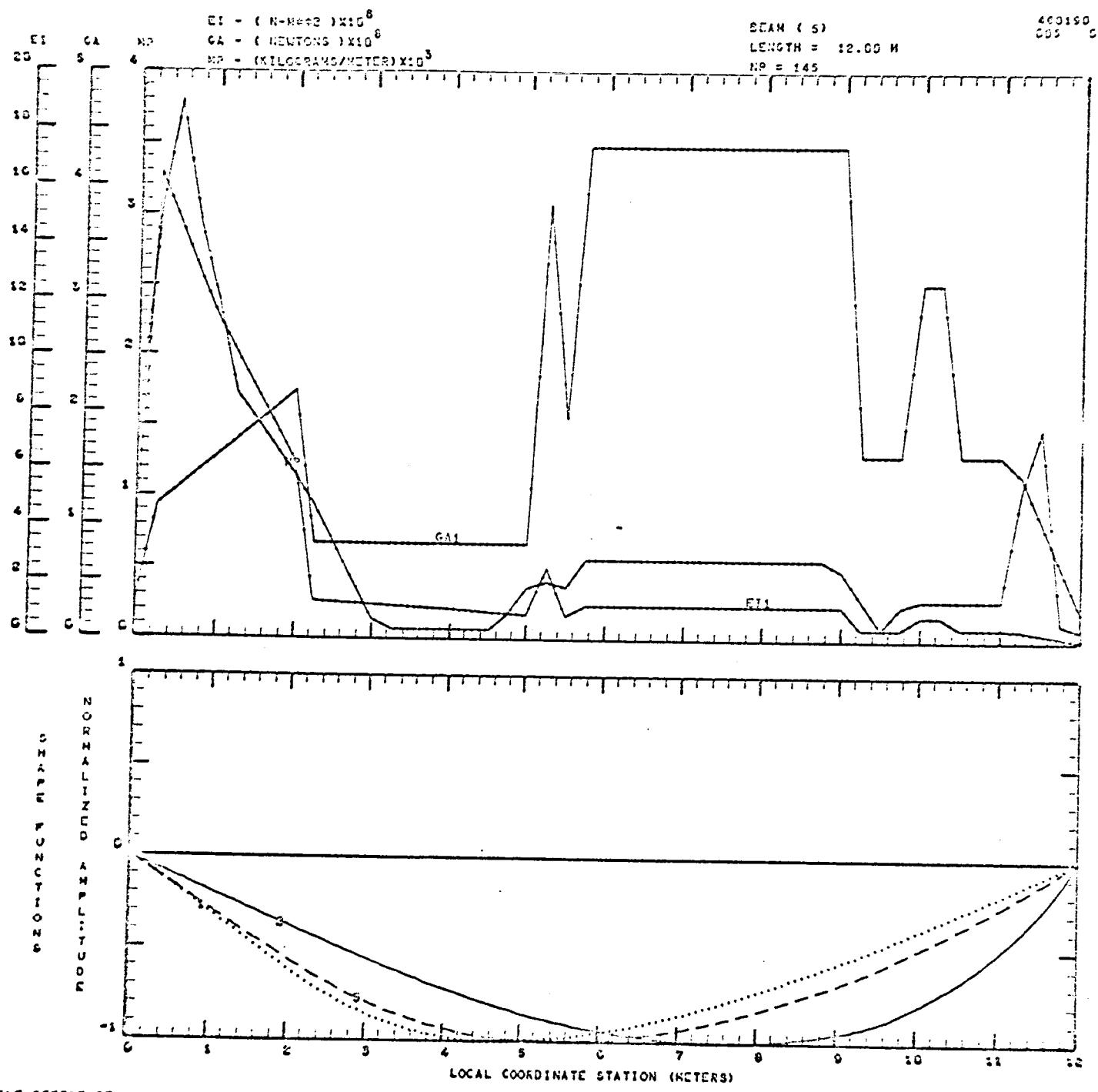
Mode	Frequency (cps)	Generalized Mass (kg)
1	1.557 (1.558)	4546 (4242)
2	2.66 (2.59)	2285 (2393)
3	4.78 (4.84)	10,891 (10,027)
4	7.80 (7.99)	-- (9067)

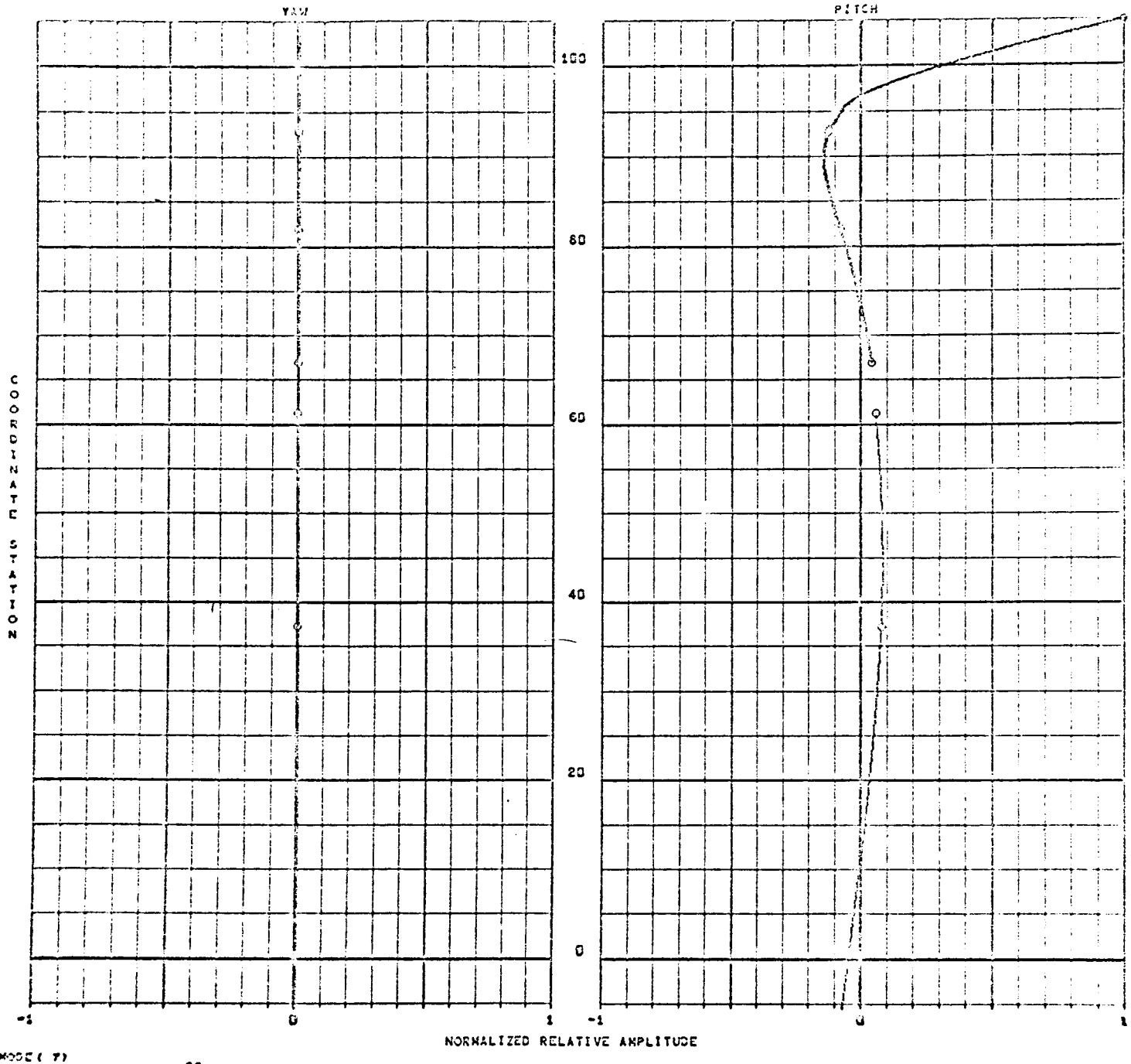


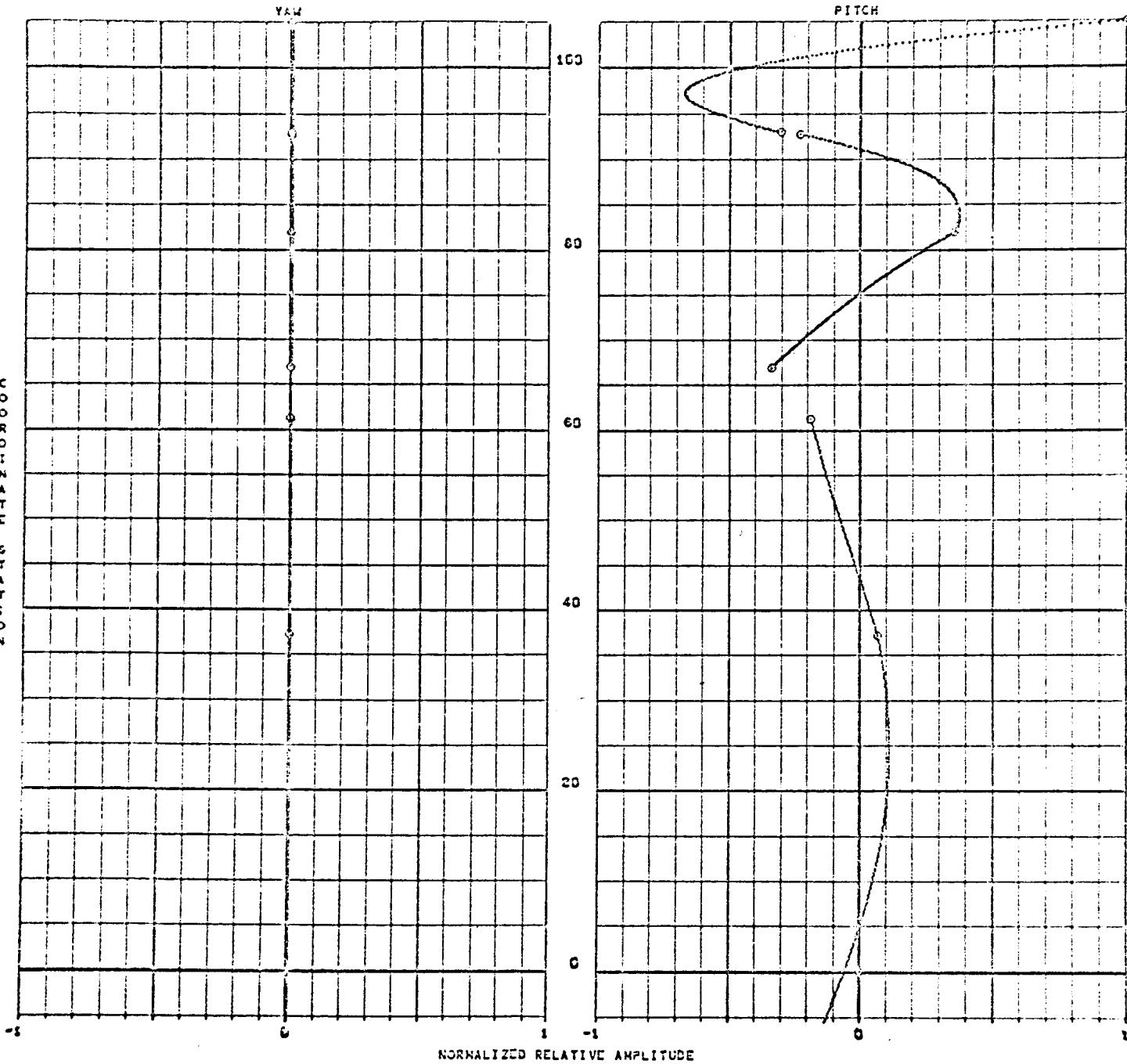
VEHICLE REFERENCE
—STATION # - 5.50



VEHICLE REFERENCE
STATION = 67.00



400129
012 000

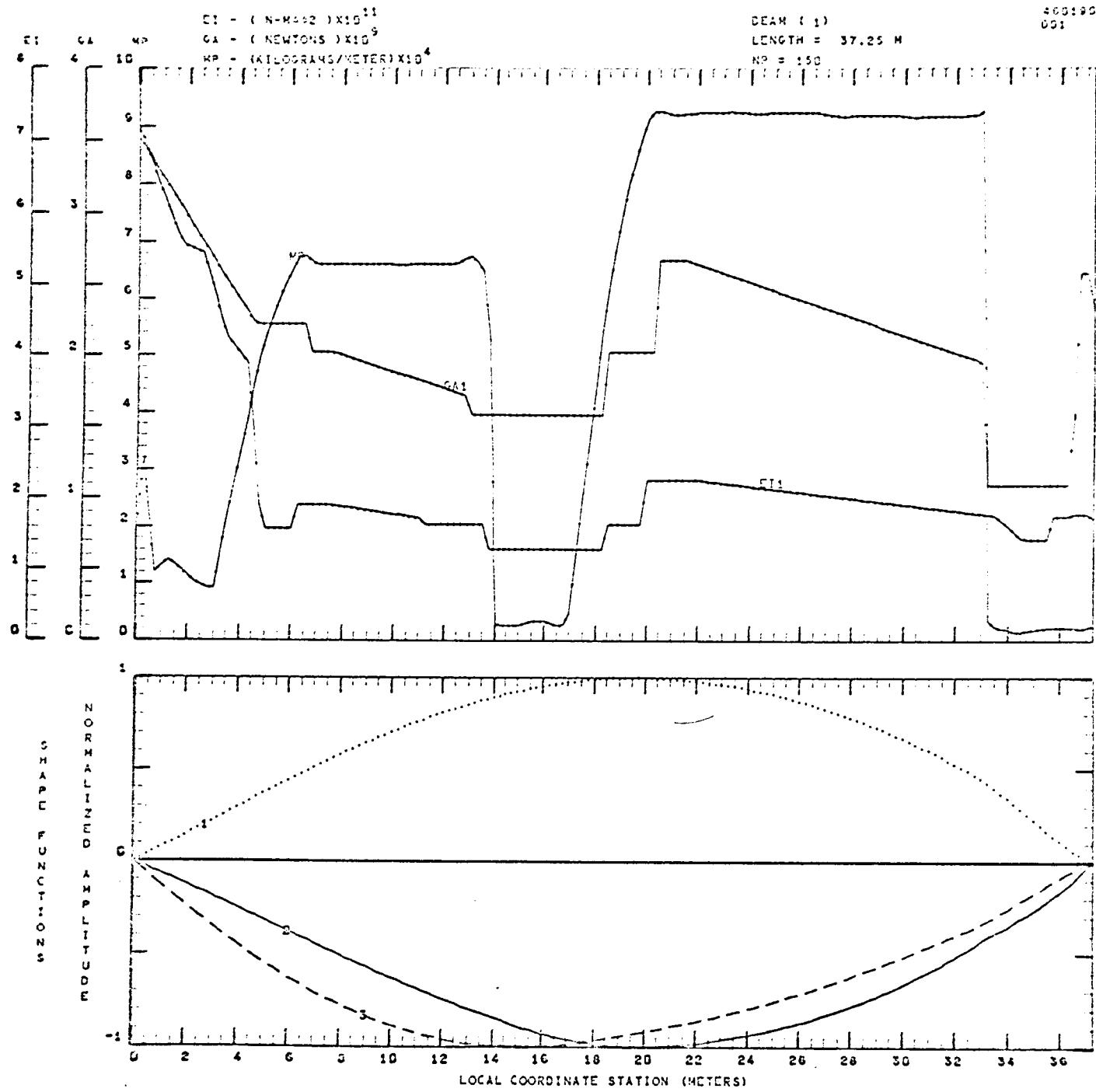
400195
016 000

PROBLEM NO. 9

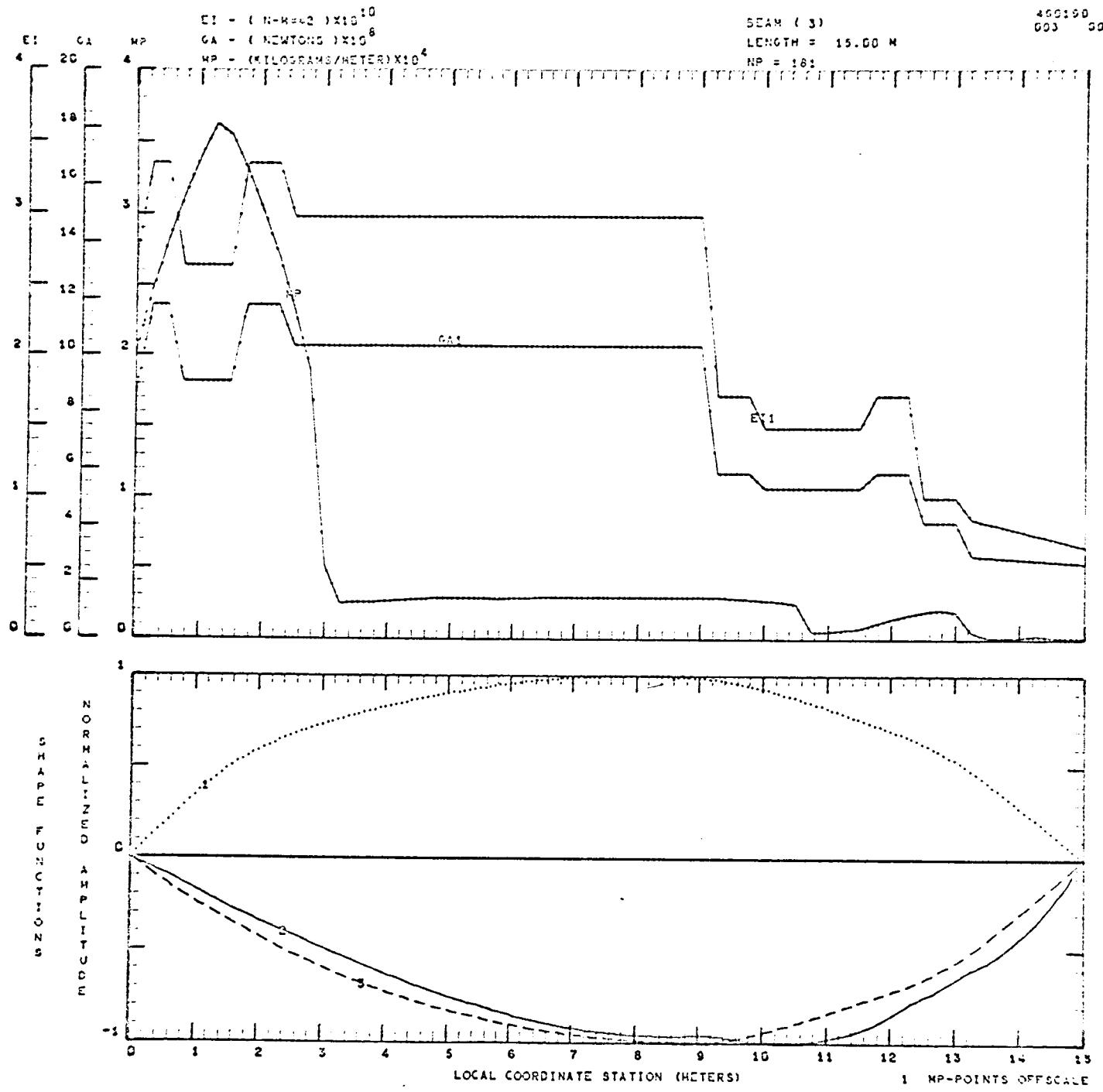
DESCRIPTION: Fully-fueled SA-501 (cantilevered). This rotationally symmetrical vehicle is modeled as six beams. All of the interstages are effectively rigid and of zero length, except for the one representing the conical interstage connecting the S-II and S-IVB. For this interstage, the same flexibility constants that were used in Problem No. 7 are used (i.e., those calculated using quasi-static Timoshenko beam theory). The data listed parenthetically in the solution summary is again the result of an execution of the NASA-Stodola program in which the vehicle was modeled as a single Timoshenko beam (no interstages). The remarkable agreement between the results reflects the validity of the "quasi-static" treatment of the interstage as well as the adequacy of the approximations of the energy method of solution.

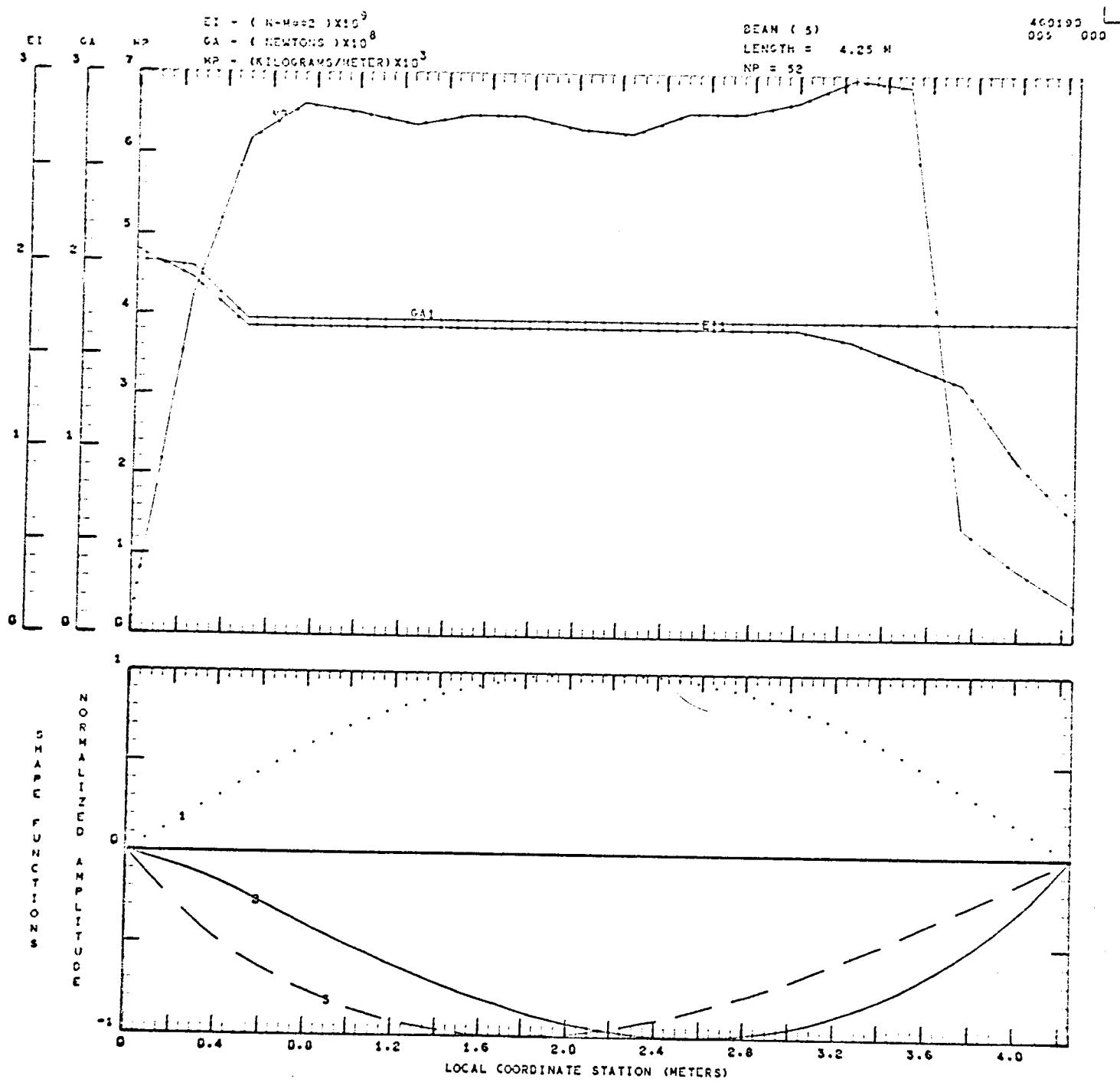
SUMMARY OF RESULTS:

Mode	Frequency (cps)	Generalized Mass (kg)
1	.323	(.321) 107,400 (107,839)
2	.907	(.901) 20,811 (20,409)
3	1.595	(1.583) 6,450 (6,201)
4	2.46	(2.42) 3,014 (3,042)

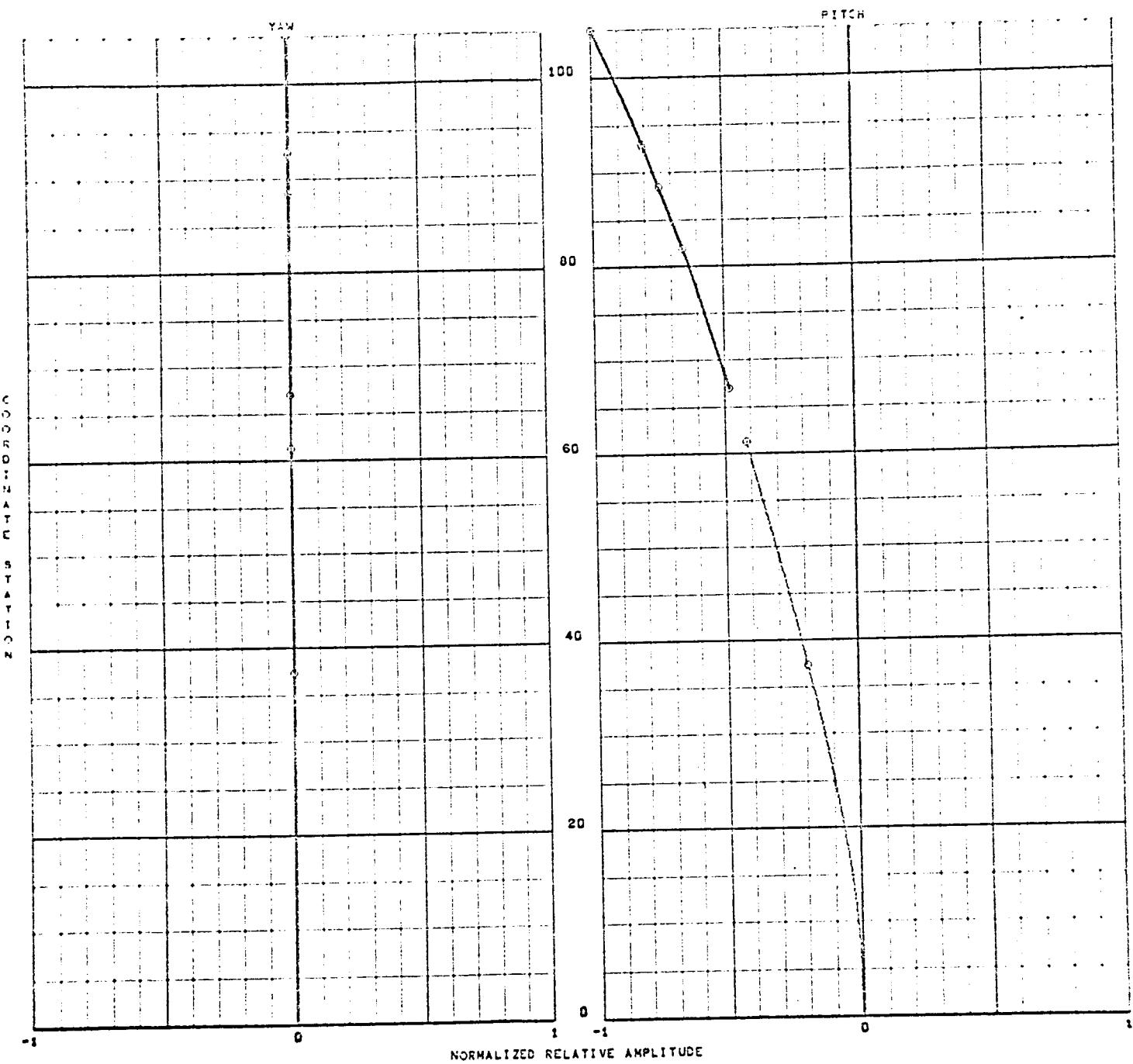


VEHICLE REFERENCE
STATION = 0.00



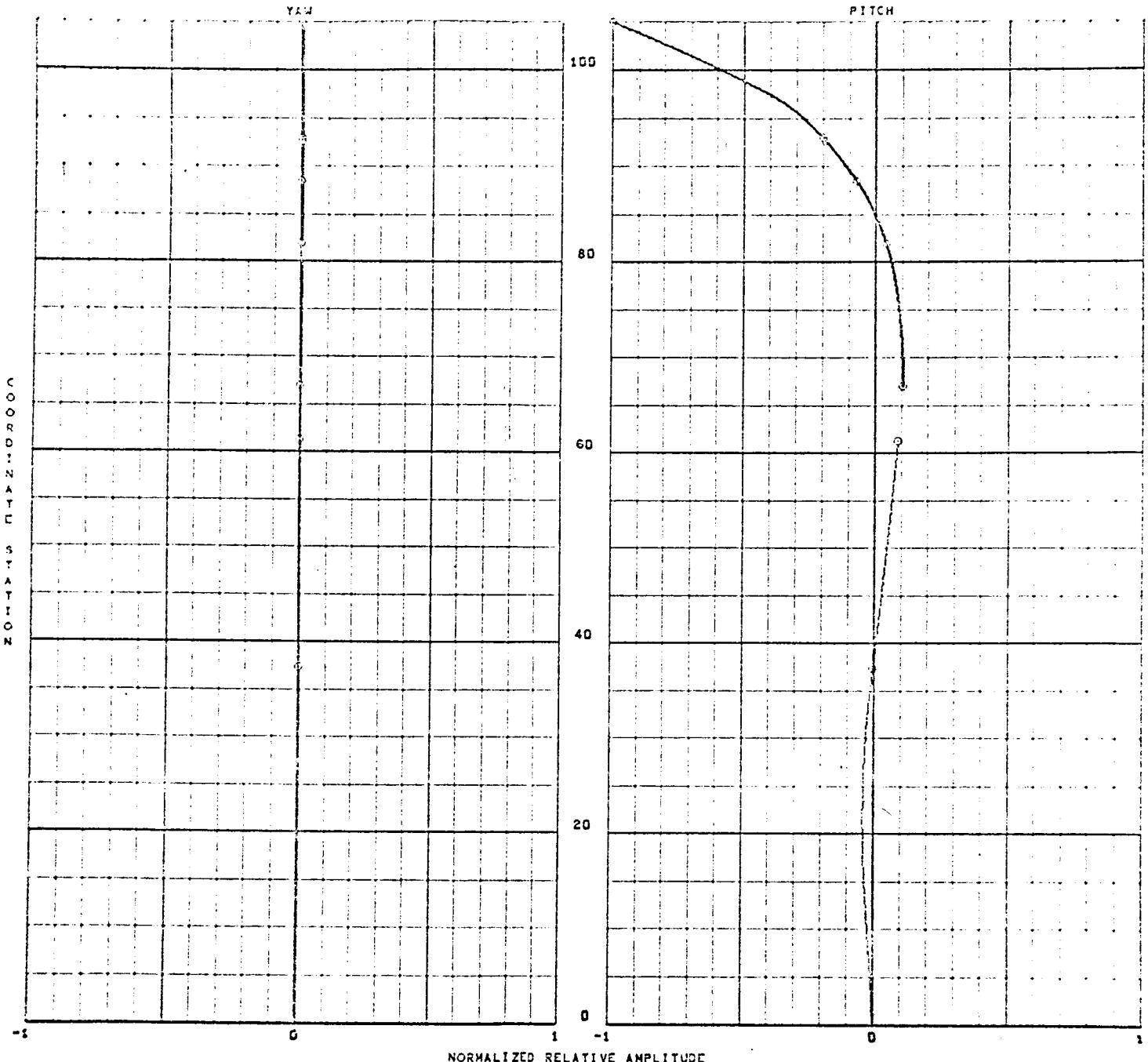


VEHICLE REFERENCE
STATION # 88.50

450:93
007 000

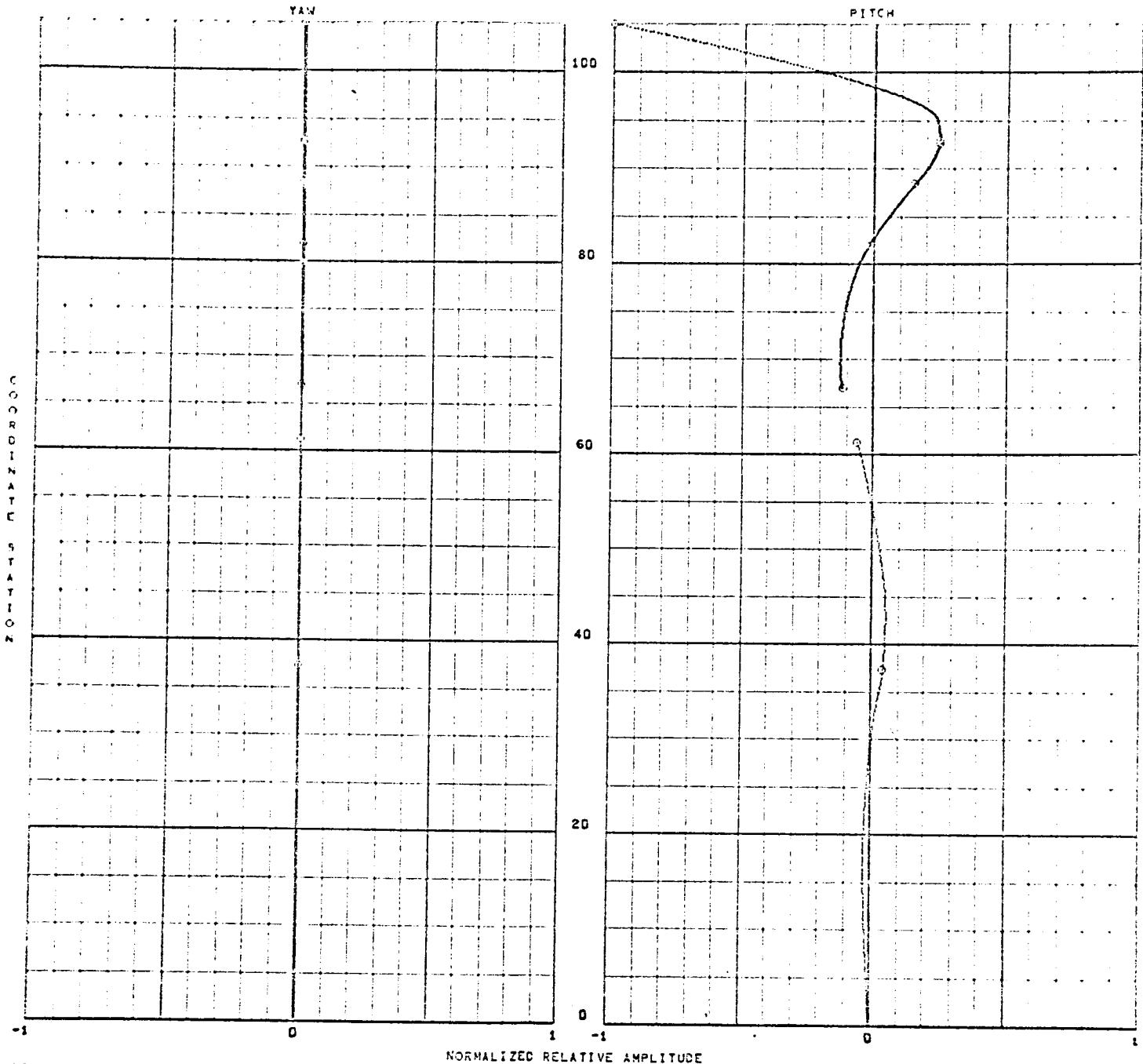
MOCC(1)

Frequency = 0.323

460190
011 000

MODE (S)

Frequency = 1.59

400:90
015 000

NOTE (9)

Frequency = 3.30

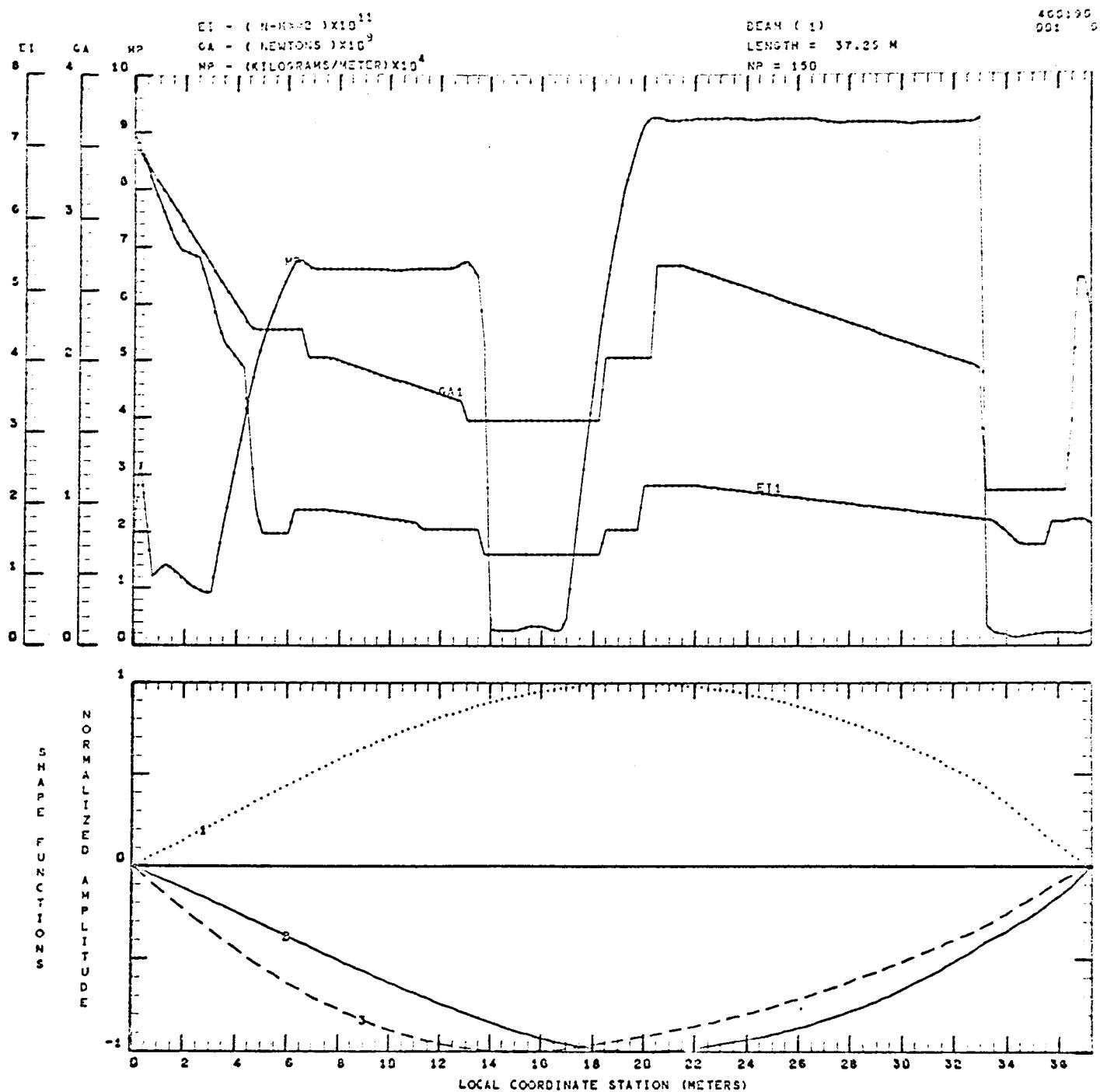
PROBLEM NO. 10

DESCRIPTION: Fully-fueled SA-501 (cantilevered). This problem is identical to Problem No. 9 except that the S-II/S-IVB interstage stiffness constants are the same as those used in Problem No. 8 (i.e., calculated using linear orthotropic shell theory). The same Stodola program results listed with the solution summary of Problem No. 9 are again given below parenthetically.

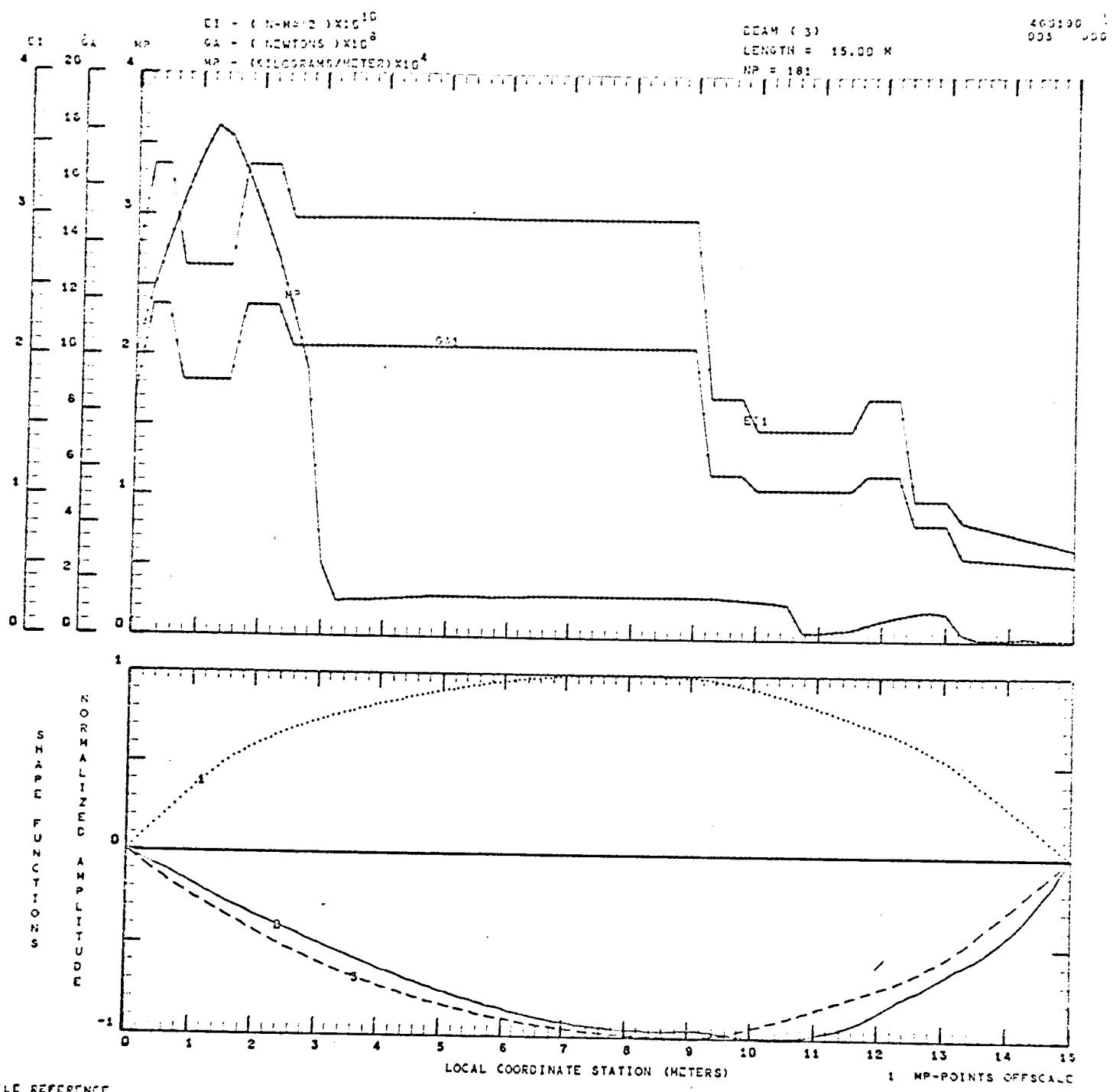
SUMMARY OF
RESULTS:

Mode	Frequency (cps)	Generalized Mass (kg)
1	.324	(.321) 108,920 (107,839)
2	.915	(.901) 19,510 (20,409)
3	1.541	(1.583) 7,177 (6,201)
4	2.49	(2.42) 3,099 (3,042)

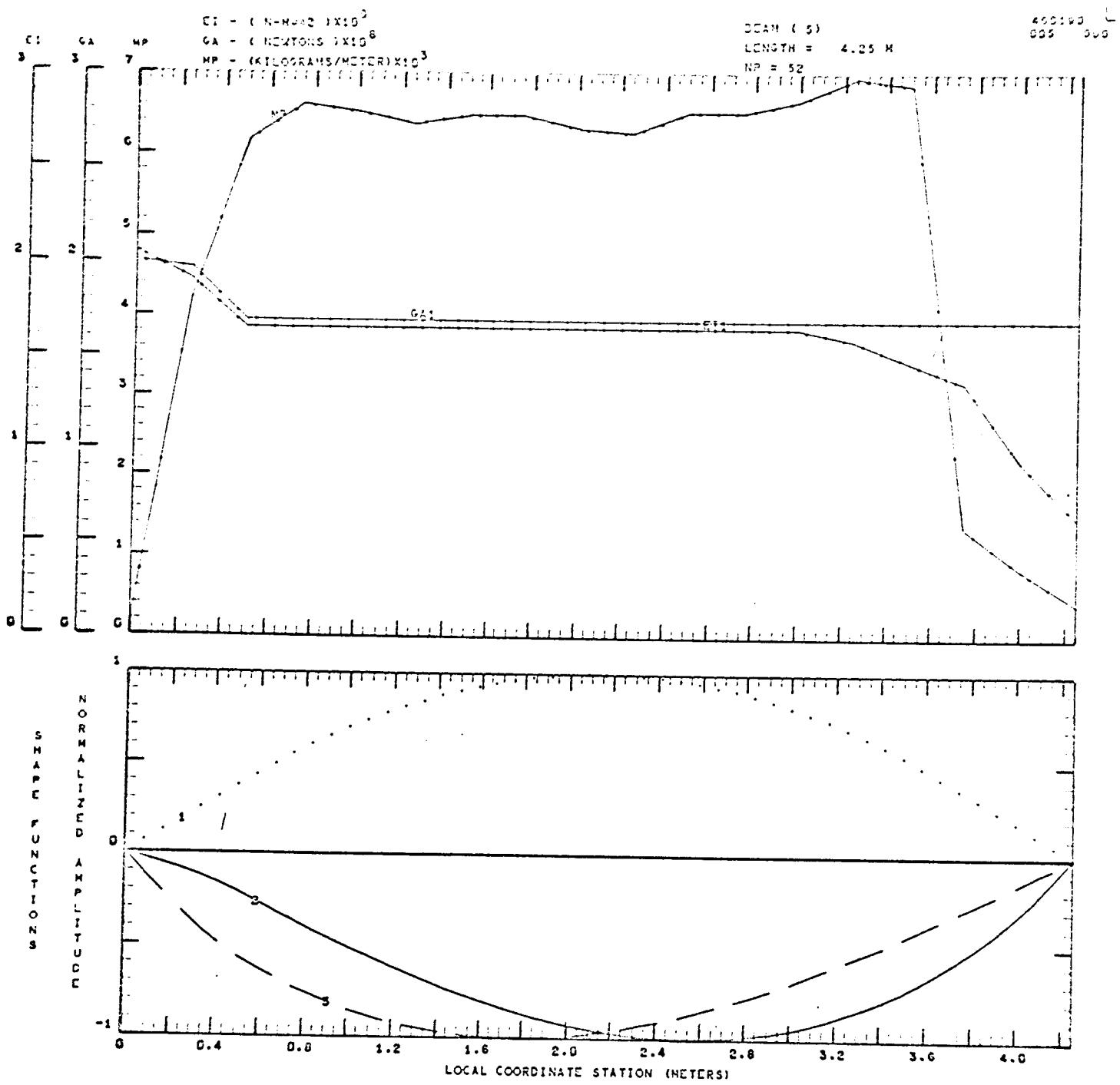
).



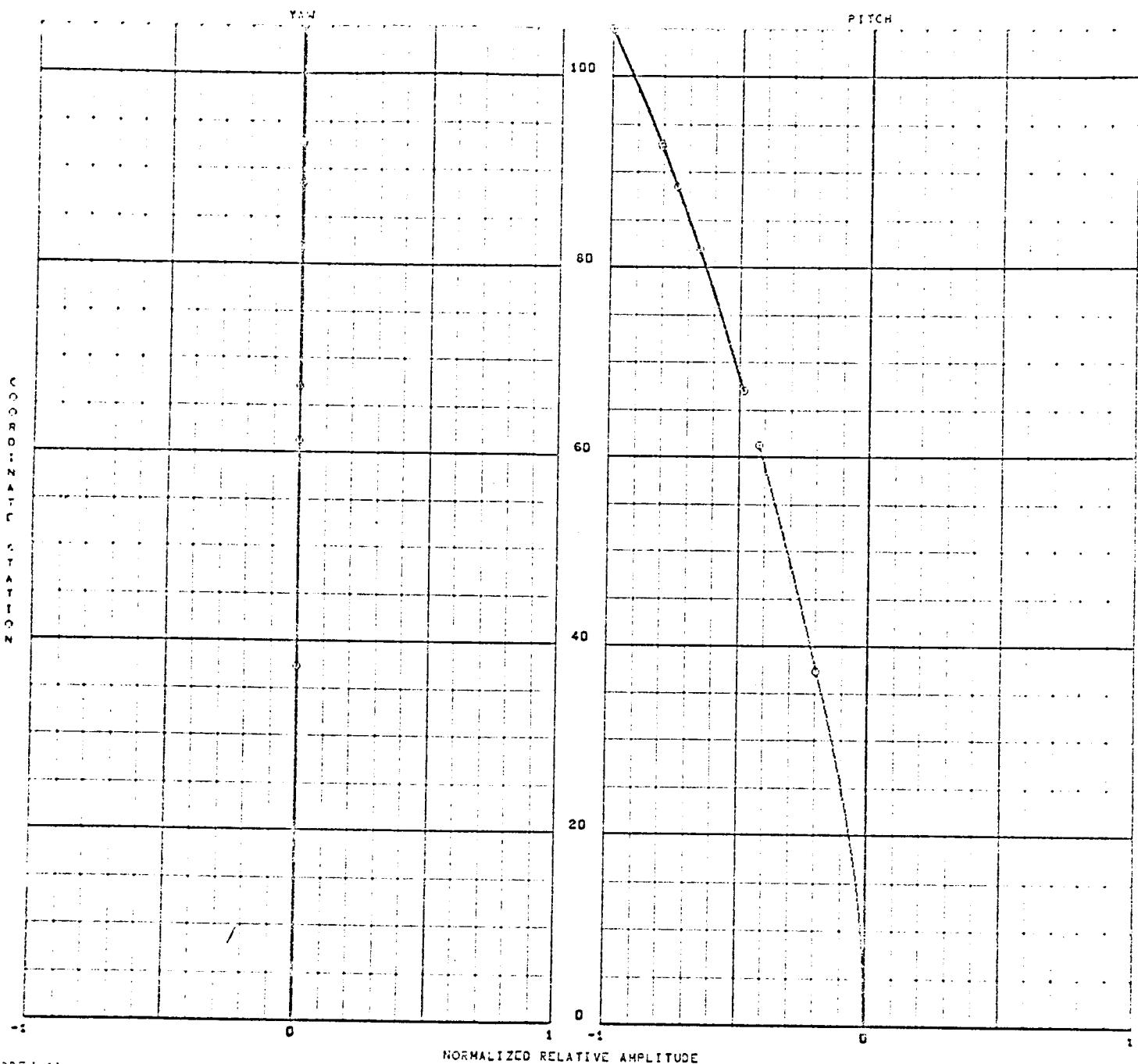
VEHICLE REFERENCE
STATION = 0.00



VEHICLE REFERENCE
 STATION = 67.00

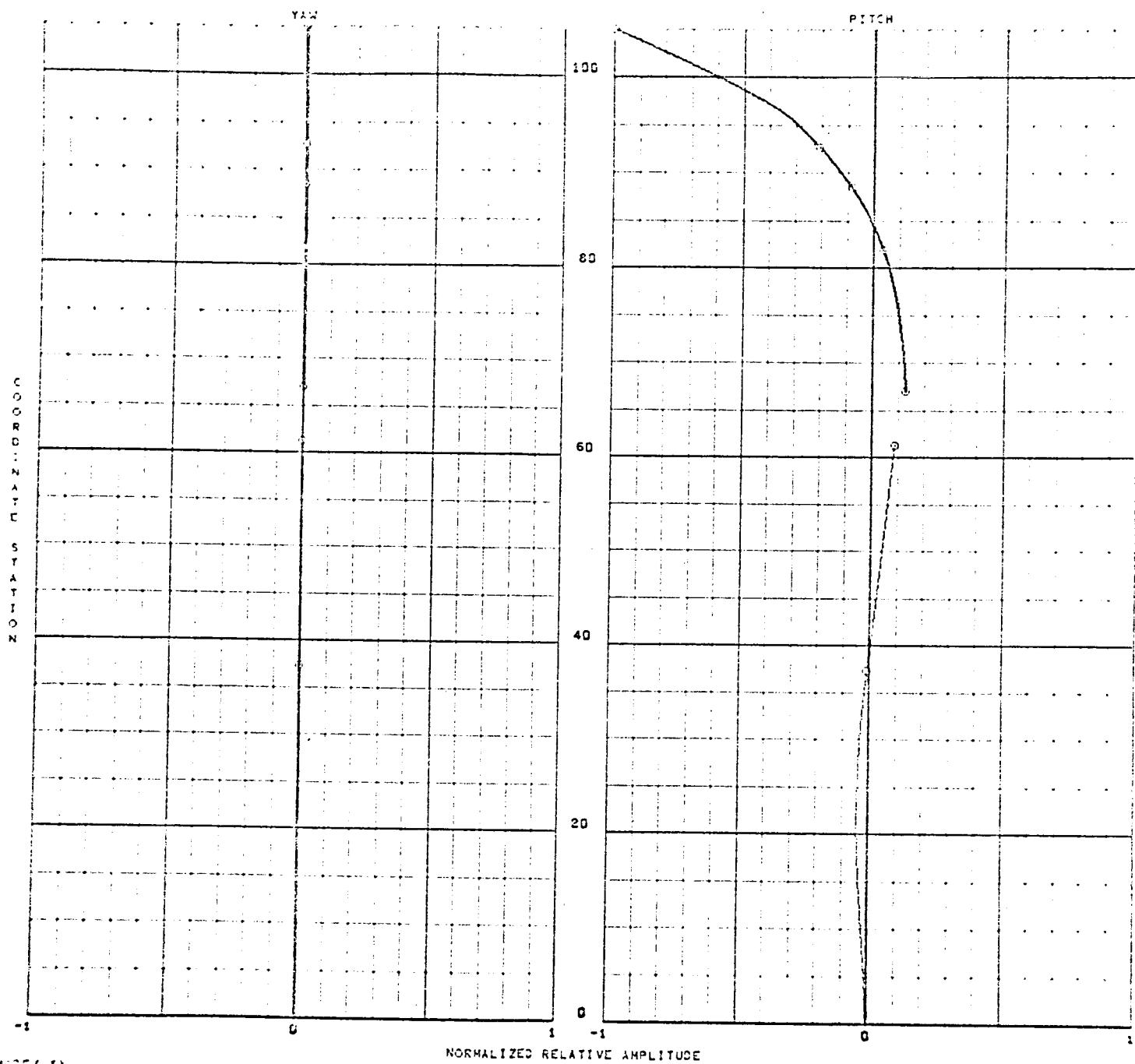


VEHICLE REFERENCE
STATION = 88.50

400195
007 006

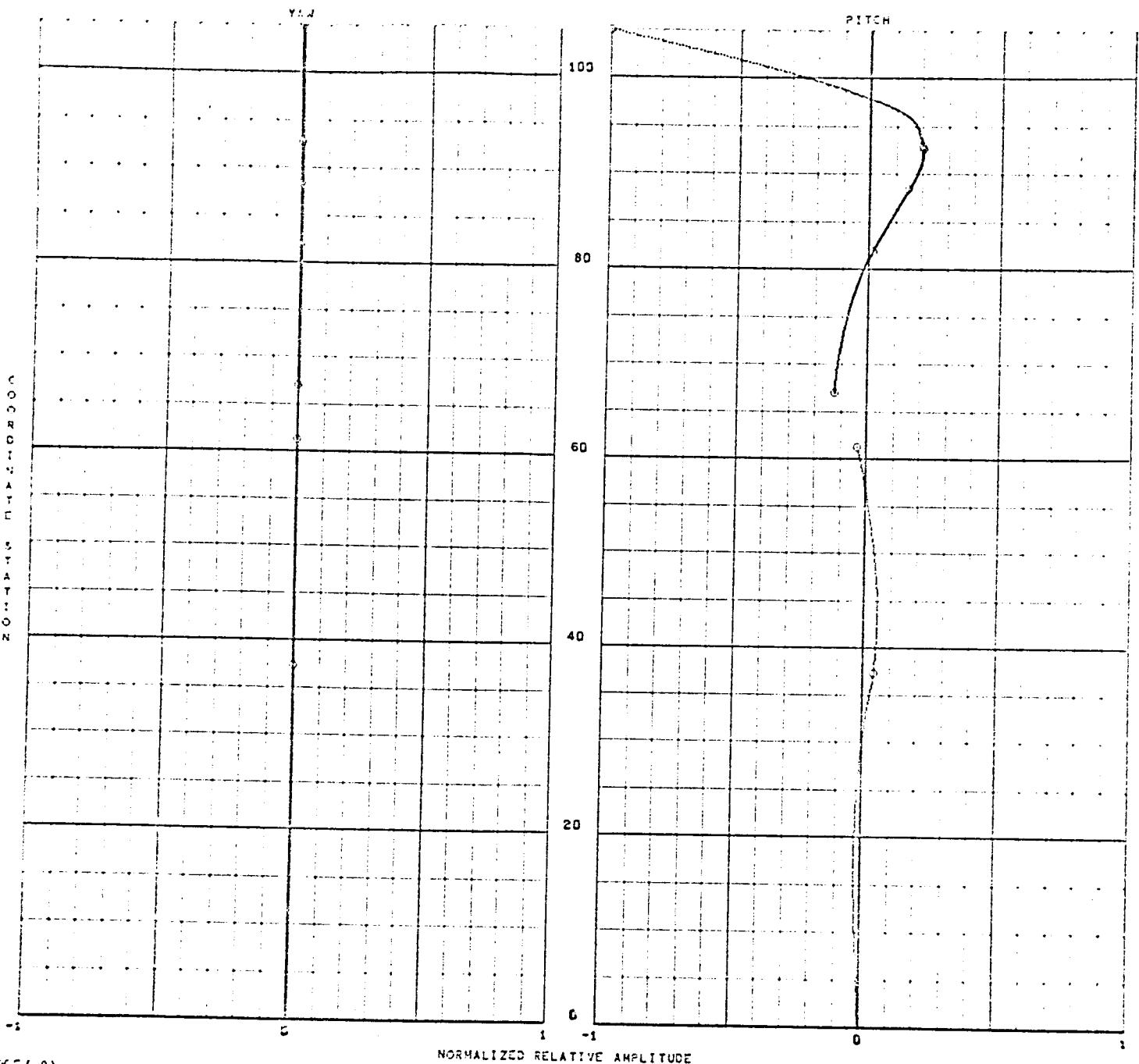
NODC (1)

Frequency = 0.324

400190
011 000

MODE (5)

Frequency = 1.541

460190
015 000

WCC(9)

Frequency = 3.05

APPENDIX B
PROGRAM LISTING AND SAMPLE PRINTED OUTPUT

LMSL MAIN - EFN SBJRCE STATEMENT - IFN(S) - 12/15/66

```

COMMON/MISC/ N, HL(12), SL(12), NP(12), NF(12), N2(12), PNU(12),
*          BM(12), BD(12), OPTI0N(12), TITLE(12), REF(12),
*          NMP(12), VPI(24), NEI(24), NGA(24), ISL(12), IBB(12),
*          NT2P, NT4P, VT31, NT8, NTT, NTP, TVM, XMC
COMMON/INTGRL/ B4(12),BJ1(12), R1(12), R2(12),V1(12,4),V2(12,4),
*          YZ1(12,4),YZ2(12,4),BYZ1(12,4),BYZ2(12,4),
*          G1(12,4,4),G2(12,4,4)
COMMON/SLOPES/ Y1PL(12,4), Y1PR(12,4), Y2PL(12,4), Y2PR(12,4)
COMMON/SPRING/ SSL1(12), SSR1(12), SSL2(12), SSR2(12),
*          RSL1(12), RSL1(12), RSL2(12), RSR2(12),
*          SK(12,4,4), SKB(12,2,2)

INTEGER OPTION
100 REMIND 1
REWIND 3
CALL INPUT
CALL COMP
CALL MATAB(IND)
IF(IND.EQ.1) GO TO 100
CALL CLVT60(NTT,IND2)
90 IF(BOPTI0N(6).EQ.0) GO TO 100
CALL GRAPH4(IND2,2)
GO TO 100
END

```

LMSL BMAT - EFN SBJRCE STATEMENT - IFN(S) - 12/15/66

```

SUBROUTINE BMAT(A,IMAX)
DIMENSION A(160,60)
L= IMAX/10
IF( (10*L).LT.IMAX) L=L+1
J1=-9
DB 200 K=1,L
J1=J1+10
J2=J1+9
IF(K.EQ.L) J2=IMAX
WRITE(6,100) (J,J=J1,J2)
100 FFORMAT(1H0// 9X,10(2X,7HCOLUMN(I2,1H)))
        WRITE(6,150)
150 FFORMAT(1H )
DB 200 I=1,IMAX
200 WRITE(6,300) I,(A(I,J),J=J1,J2)
300 FFORMAT(5H R8W(I2,1H),IX,IP1)E12.4)
RETURN
END

```

BMAT0010	
BMAT0020	
BMAT0030	
BMAT0040	
BMAT0050	
BMAT0060	
BMAT0070	
BMAT0080	
BMAT0090	
BMAT0100	12
BMAT0110	
BMAT0120	16
BMAT0130	
BMAT0140	
BMAT0150	19
BMAT0160	
BMAT0170	
BMAT0180	

B- /

L4SC
 RMAT - EFN SOURCE STATEMENT - IFN(S) - 12/15/66

```

SUBROUTINE RECMAT(A,IX,IY,IXX,IYY)
DIMENSION A(IXX,IYY)
L=IY/10
IF(IY>L).LT.IY L=L+1
J1=-9
D0 300 K=1,L
J1=J1+10
J2=J1+9
IF(K.EQ.L) J2=IY
WRITE(6,100) (J,J=J1,J2)
100 FORMAT(1H0//,9X,10(2X,7HCBLJMN([2,1H)))
WRITE(6,200)
200 FORMAT(1H )
D0 300 I=1,IX
300 WRITE(6,400) I,(A(I,J),J=J1,J2)
400 FORMAT(5H R0W([2,1H],IX,IP10E12.4)
RETURN
END

```

RMAT0010
 RMAT0020
 RMAT0030
 RMAT0040
 RMAT0050
 RMAT0060
 RMAT0070
 RMAT0080
 RMAT0090
 RMAT0100 12
 RMAT0110
 RMAT0120 16
 RMAT0130
 RMAT0140
 RMAT0150 19
 RMAT0160
 RMAT0170
 RMAT0180

L4SC
 BDAT - EFN SOURCE STATEMENT - IFN(S) - 12/14/66

```

BLOCK DATA
COMMON/SPRING/ SSL1(12), SSR1(12), SSL2(12), SSR2(12),
   RSL1(12), RSL1(12), RSL2(12), RSR2(12),
   SK(12,4,4), SK8(12,2,2)
COMMON/SHAPES/ MP(1930), IP(1930), EI(1900), GA(1900),
   MP(1930), IP(1930), EI(1900), GA(1900),
   Y(12630), YS(12630), Z(12630), YY(12630),
   FMP, FIP, FEI, FGA
DATA SK,SKB,SSL1,SSR1,SSL2,SSR2,RSL1,RSR1,RSL2,RSR2 /335*0.0/,
   SKB(3,1,1), SKB(3,2,2) /2*7.25E8/,  

   SK(1,1,1), SK(1,2,2), SK(3,1,1), SK(3,2,2)/2*1.E13,2*1.E12/,  

   SK(4,1,1), SK(4,1,2), SK(4,2,2)/47115E9,-.58894E8,.24836E9/,  

   SK(4,3,3), SK(4,3,4), SK(4,4,4)/47115E9,-.58894E8,.24836E9/
END

```

LMSC INPUT - EFN SOURCE STATEMENT - [ENESI] - 12/15/66
 SUBROUTINE INPUT
 COMMON/MISC/ N, BL(12), SL(12), NP(12), NF(12), N2(12), PNU(12),
 * BM(12), BD(12), OPTION(12), TITLE(12), REF(12),
 * NMP(12), NIP(24), NE(124), NGA(24), ISL(12), IBB(12),
 * NT2D, N4P(4), NT3, NT4, NTP, TV4, XMC
 CBMMN/SHAPES/ MP(1900), IP(1900), EI(1900), GAI(1900),
 * MP(1900), IP(1900), EI(1900), GAI(1900),
 * Y(2600), YSL(2600), Z(2600), YY(2600),
 * FMP, FIP, FEI, FGA
 COMMON/SPRING/ SSL(112), SSR1(12), SSR2(12),
 * RSL(112), RSL1(12), RSL2(12), RSR(12),
 * SK(12,4,4), SKB(12,2,2)
 COMMON/SLOPES/ YIPL(12,4), YIPR(12,4), Y2PL(12,4), Y2PR(12,4)
 DIMENSION ILEFT(2), IRIGHT(2), VALUL(2), VALUR(2)
 INTEGER OPTION, SHEAR
 REAL IP, MP, IP1, MP1, ML, MR
 REAL IP, MP, IP1, MP1, ML, MR
 !PUT HEAT PROPERTIES
 READ(*,1) TITLE
 READ(*,1) OPTION
 READ(*,1) N, PEF(1)
 1 FORMAT(1A46)
 2 FORMAT(1A14)
 14 FORMAT(1E-512.8)
 20 FORMAT(6E12.8)
 J1=1
 K1=1
 L1=1
 M1=1
 DO 50 I=1,N
 HSL(I+1)= NP(I)+NF(I)+NE(I)+N1(I)+N2(I)+NSAC(I)
 DEAL(I+1)= AL(I)+BL(I)+NP(I)+NF(I)+NE(I)
 J2=J1+NE(I)-1
 K2=K1+NT2D(I)-1
 L2=L1+NT3(I)-1
 M2=M1+NTP(I)-1
 READ(I+20) (V(I+J),J=1,J2)
 READ(I+20) (P(I+J),J=1,J2)
 MP(I+20)= (I1(I,L1)+S1(I,L1))
 READ(I+20) (S1(I,L1),I=1,I2)
 J1=J2+1
 K1=K2+1
 L1=L2+1
 M1=M2+1
 N2(I)=NPE(I)

 DB 100 I=1,N
 REF(I+1)=REF(I)+BL(I)+SL(I)
 IF(SL(I).LT.1.E-35) GO TO 100
 SK(I,1,1)= SL(I)*(SL(I)*SK(I,1,1)+SK(I,1,2))+ SL(I)*SK(I,1,2)
 SK(I,1,2)= SL(I)*SK(I,1,2)+ SK(I,2,2)
 SK(I,3,3)= SL(I)*(SL(I)*SK(I,3,3)+SK(I,3,4))+ SL(I)*SK(I,3,4)
 SK(I,3,4)= SL(I)*SK(I,3,4)+ SK(I,4,4)
 100 CONTINUE
 J1=1
 J2=1
 J3=1
 J4=1
 K1=1
 NTP=0
 DB 200 I=1,N
 NSEG=NP(I)-1
 CALL INTERP(MP(J1),MP(K1),NMP(I),NSEG,IER)
 J1=J1+NMP(I)
 140
 CALL INTERP(EI(J2),EI(K1),NE(I),NSEG,IER)
 J2=J2+NE(I)
 150
 CALL INTERP(GAI(J3),GA(K1),NGA(I),NSEG,IER)
 J3=J3+NGA(I)
 155
 CALL INTERP(IP(J4),IP(K1),NIP(I),NSEG,IER)
 J4=J4+NIP(I)
 160
 K1=K1+NPE(I)-1
 200 NTP=NTP+NSEG
 210
 WRITE(3) MP
 REWIND 3
 220
 L=1
 I1=1
 J1=1
 SHEAR=1
 IF(OPTION(3).EQ.0) SHEAR=0
 IBUT=BPTION(2)
 DB 300 I=1,N
 IF(NFI(I).EQ.C) GO TO 290
 NSEG=NP(I)-1
 FCBEF=1
 ILEFT(1)=1
 ILEFT(2)=3
 IRIGHT(1)=1
 IRIGHT(2)=3
 IF(I1.NE.N) GO TO 250
 ILEFT(2)=2
 IRIGHT(1)=4
 250 CONTINUE
 IF(I1.NE.1) GO TO 260
 IF(ALS1.NE.0) GO TO 260
 IRIGHT(2)=2
 ILEFT(1)=4
 260 CONTINUE
 VALUL(1)=0.
 VALUR(1)=0.
 VALUL(2)=0.
 VALUR(2)=0.
 J=1
 IF(IBUT.NE.0) WRITE(6,350) I,J
 CALL NUB(BL(I),NP(I),ILEFT,VALUL,IRIGHT,VALUR,EI(L),GA(L),MP(L),
 * Y(I,J),Z(J,1),YY(J,1),YS(J,1),SHEAR,FCBEF,IBUT)
 J1=J1+NPE(I)
 ILEFT(1)=1
 ILEFT(2)=3
 IRIGHT(1)=1
 IRIGHT(2)=3
 VALUL(2)=0.
 270
 280
 290
 300
 310
 320
 330
 340
 350

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 INPUT - EFN SOURCE STATEMENT - IFN(S) - 12/15/66
 VALUR(2)=1.
 FC&EF=0.
 J=2
 IF(IOUT.NE.0) WRITE(6,350) I,J
 CALL NUB (BL(I),NP(I),ILEFT,VALUL,IRIGHT,VALUR,E(I,L),GA(L),MP(L),
 * Y(J1),Z(J1),YY(J1),YS(J1),SHEAR,FC&EF,IOUT) 243
 J1=J1+NP(I)
 VALUL(2)=1.
 VALUR(2)=0.
 J=3
 IF(IOUT.NE.0) WRITE(6,350) I,J
 CALL NUB (BL(I),NP(I),ILEFT,VALUL,IRIGHT,VALUR,E(I,L),GA(L),MP(L),
 * Y(J1),Z(J1),YY(J1),YS(J1),SHEAR,FC&EF,IOUT) 259
 J1=J1+NP(I)
 263
 290 L=L+NP(I)-1
 300 CONTINUE
 350 FORMAT(16HIBeam,,I1,13H) FJNCTION,,I1,1H)
 READ(3) MP
 REWIND 3
 RETURN
 END

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SUBROUTINE INTERP(P,R,NG,NSEG,IER)
  ROUTINE FOR GENERATING AN ARRAY OF ARBITRARY SIZE CONTAINING
  INTERPOLATED VALUES WHEN GIVEN THE INPUT IN THE FORM OF X,Y PAIRS NTRP0030
  P ARRAY CONTAINS THE INPUT X,Y PAIRS -- P(1)=X(1), P(2)=Y(1), ETC. NTRP0040
  R ARRAY CONTAINS THE INTERPOLATED VALUES NTRP0050
  NG = NUMBER OF INPUT POINTS 2*(NE OF PAIRS) NTRP0060
  NSEG=NUMBER OF INTERPOLATED VALUES REQUESTED NTRP0070
  IER= ERROR INDICATOR NTRP0080
  NTRP0090
  NTRP0100
  DIMENSION P(1), PX(250), PY(250), R(1), A(500), ERROR(21) NTRP0110
  DATA ERROR / * NTRP0120
  * 6HNUMBER,6H BF IN,6HPUT PA,6HRS IS,6H GREAT,6HHER THA,6HN 250 , NTRP0130
  * 6HX VALU,6HES ARE,6H NBT I,6HN INCR,6HEASING,6H BRDER,6H , NTRP0140
  * 6HINITIA,6HL X VA,6HLUE IS,6H NET Z,6HBR ,6H ,6H /NTRP0150
  NTRP0160
  C ERROR CHECK NTRP0170
  C IF THE INPUT DATA IS [INVAL], A STATEMENT DESCRIBING THE ERROR IS NTRP0180
  PRINTED AND A RETURN IS MADE TO THE CALLING PROGRAM WITH THE ERROR NTRP0190
  INDICATOR SET (IER=1) NO ARRAY WILL BE GENERATED NTRP0200
  NTRP0210
  IER=0 NTRP0220
  IND=0 NTRP0230
  IF(NG.LT.500) GO TO 10 NTRP0240
  IND=1 NTRP0250
  GO TO 300 NTRP0260
  10 M=NG/2 NTRP0270
  DO 20 I=1,M NTRP0280
  PY(I)=P(2*I) NTRP0290
  20 PX(I)=P(2*I-1) NTRP0300
  DO 30 I=2,M NTRP0310
  IF(PX(I).LT.PX(I-1)) GO TO 40 NTRP0320
  30 IF(PX(I).GT.1.E-35) IND=3 NTRP0330
  40 IF(IND.NE.0) GO TO 300 NTRP0340
  50 IF(IND.NE.0) GO TO 300 NTRP0350
  NTRP0360
  NTRP0370
  C CONSTRUCT ARRAY CONTAINING VALUES AT THE LEFT END OF EACH SEGMENT NTRP0380
  UX=PX(1)/FLBAT(1*SEG) NTRP0390
  DX2=DX*2. NTRP0400
  X=0. NTRP0410
  J=1 NTRP0420
  DO 100 I=1,NSEG NTRP0430
  IF(PX(J+1).GT.X) GO TO 80 NTRP0440
  J=J+1 NTRP0450
  GO TO 60 NTRP0460
  60 A(I)=PY(I) + (PY(J+1)-PY(J))*(X-PX(J))/(PX(J+1)-PX(J)) NTRP0470
  100 X=DX*FLBAT(I) NTRP0480
  A(1*SEG+1)=PY(M) NTRP0490
  NTRP0500
  C CONSTRUCT THE R ARRAY OF INTERPOLATED VALUES NTRP0510
  NTRP0520
  X=0. NTRP0530
  J=2 NTRP0540

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DB 200 I=1,NSEG NTRP0550
IF(PX(I).GT.(X+DX)) GO TO 100 NTRP0560
K(I)=(A(I)+PY(J)+(PX(J)-X)) NTRP0570
120 J=J+1 NTRP0580
IF(I.J.LE.M) GO TO 140 NTRP0590
IF(I.I.EQ.NSEG) GO TO 170 NTRP0600
IER=1 NTRP0610
NWRITE(6,130) I,J NTRP0620
130 FFORMAT(40HDEERRR *** INTERP ROUTINE *** AT SEGMENT,I4,36H THE LASTNTRPC630
  * INPUT PAIR WAS REACHED (I=13,1H)) NTRP0640
  GO TO 310 NTRP0650
140 IF(PX(I).GT.(X+DX)) GO TO 160 NTRP0660
  R(I)=R(I)+(PY(J-1)+PY(J))*(PX(J)-PX(J-1)) NTRP0670
  GO TO 120 NTRP0680
160 R(I)=R(I)+(PY(J-1)+A(I+1))*(X+DX-PX(J-1)) NTRP0690
170 R(I)=R(I)/DX2 NTRP0700
  GO TO 200 NTRP0710
180 K(I)=(A(I)+A(I+1))/2. NTRP0720
200 X=DX*FLBAT(I) NTRP0730
  GO TO 310 NTRP0740
300 IER=1 NTRP0750
  I1= 7*(IND-1) + 1 NTRP0760
  I2=I1+6 NTRP0770
  WRITE(6,305) (ERROR(I),I=I1,I2) NTRP0780
  305 FFORMAT(30HDEERRR *** INTERP ROUTINE *** ,746,14H NOT ALLOWED) NTRP0790
  310 RETURN NTRP0800
  END NTRP0810

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      LMSC      - EFN  SJRCE STATEMENT - IFN(S) - 12/15/66

      SUBROUTINE NUB (BL,VSTA,ICX,XRARI,ICCY,YBAR1,ET,GA,QQ,
                     Y,PSI,PSI(PRM,ALPHA,SHEAR,FCDEF,I8UT)

C STATIC DEFLECTION ANALYSIS -- ARBITRARY TIMOSHENKO BEAMS
C IDCX, IDCY SPECIFY WHICH QUANTITIES ARE PRESCRIBED  1-Y 3-MOM
C AS BOUNDARY CONDITIONS AT THE LEFT AND RIGHT ENDS  2-PSI 4-V
C XBAR1, YBAR1 CONTAIN THE VALUES OF THESE QUANTITIES
C SHEAR=1 IF DEFLECTIONS DUE TO SHEAR ARE TO BE INCLUDED IN ANALYSIS
C THE ELEMENTS OF THE DISTRIBUTED LOAD ARRAY QQ ARE MULTIPLIED BY
C FCDEF (FCDEF=0, IF NO DISTRIBUTED LOAD IS REQUIRED)
C
C DIMENSION IDCX(2), IDCY(2), XBAR1(2), XBAR2(2), YBAR1(2),
C          C(4,4,2), E(4,2), S(4,2), T(4,4), R(4), PRD(2), VECT(2),
C          E(11), GA(1), QO(1), Y(1), PSI(1), ALPHAI(1), PSIPRM(1),
C          YPRIME(200), M0M(200), V(200), AG(200), NAME(12)
C
C DATA NAME /6H LEFT , 6H RIGHT, 6HCLAMPE, 6HPINNED, 6H
C          6HGUIDED, 6H FREE , 6HD , 4*H /
C
C INTEGER BLD, P, Q, TEMP, SHEAR
C REAL MM
C
C CHECK FOR VALIDITY OF BOUNDARY CONDITIONS
C
C KL=J
C KR=J
C I=IDCX(1)
C J=IDCX(2)
C IF (((I.EQ.1.AND.J.EQ.4).AND.(J.EQ.2.OR.J.EQ.3)).OR.
C     ((J.EQ.1.OR.J.EQ.4).AND.(I.EQ.2.OR.I.EQ.3))) KL=1
C I=IDCY(1)
C J=IDCY(2)
C IF (((I.EQ.1.OR.I.EQ.4).AND.(J.EQ.2.OR.J.EQ.3)).OR.
C     ((J.EQ.1.OR.J.EQ.4).AND.(I.EQ.2.OR.I.EQ.3))) KR=1
C
C IF(KL.EQ.Q) WRITE(6,60) NAME(1)
C IF(KR.EQ.Q) WRITE(6,60) NAME(2)
C 40 FORMAT(55H***ERROR*** INVALID BOUNDARY CONDITIONS SPECIFIED FOR
C          *A6,12H END OF BEAM/1X,25H0 SOLUTION WILL BE FOUND)
C          *IF(KL.EQ.0.OR.KR.EQ.0) GO TO 400
C
C PRINT END CONDITION DESCRIPTIONS
C
C IX=IDCX(1) + IDCX(2)
C IY=IDCY(1) + IDCY(2)
C WRITE(6,60) NAME(IX),NAME(IY+5),NAME(IY),NAME(IY+5)
C 60 FORMAT(1H0,A6,A2,A6,A2,5H BEAM) 25
C
C EVALUATE THE MATRIX C AND THE VECTOR E AT RIGHT END OF BEAM
C
C DO 110 I=1,4
C DO 110 J=1,4
C VALUE=0.
C IF(I.EQ.J) VALUE=1.
C C(I,J,1)=VALUE

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100 C(I,J,2)=0.
E(I,I)=0.
110 T(I,I)=1.

C NSEG=NSTA-1
DLT=BL/FLBAT(NSEG)
DLT2=DLT**2/2.
DLT3=DLT**3/6.
DLT4=DLT**4/24.
T(1,2)=DLT
T(3,4)=DLT
R(3)=DLT2
R(4)=DLT
C
2LD=1
NEW=2
DB 150 K=1,NSEG
AG(K)=0.
IF(SHEAR.EQ.1) AG(K)=1./GA(K)
C
C COMMENT *** THE AG ARRAY CONTAINS THE RECIPROCAL VALUES OF THE SHEAR
C STIFFNESS GA WHEN THE DEFLECTIONS DUE TO SHEAR ARE TO BE
C INCLUDED IN THE ANALYSIS AND CONTAINS ZEROS WHEN SHEAR
C IS NEGLECTED
C
QO(K)=QO(K)*FCDEF
T(1,3)=DLT2/E(I,K)
T(1,4)=DLT3/E(I,K) - DLT*AG(1)
T(2,3)=DLT/E(I,K)
T(2,4)=T(1,3)
R(1)=DLT4/E(I,K) - DLT2*AG(K)
R(2)=DLT3/E(I,K)
C
DB 140 I=1,4
E(I,NEW)=0.
DB 130 J=1,4
C(I,J,NEW)=0.
DB 120 L=I,BLD
120 C(I,J,NEW)=C(I,J,NEW) + T(I,L)*C(L,J,BLD)
130 E(I,NEW)=E(I,NEW) + T(I,J)*E(J,BLD)
140 E(I,NEW)=E(I,NEW) + QO(K)*R(I)
TEMP=BLD
BLD=NEW
150 NEW=TEMP
C
C EVALUATE THE TWO UNKNOWN ELEMENTS OF THE STATE AT LEFT END OF BEAM
C
I=IDCY(1)
J=IDCY(2)
M=IDCX(1)
N=IDCX(2)
C
K=5-I
L=5-J
M=5-M
O=5-V

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C
C     PR00(1)=C(I,M,BLD)*XBARI(1) + C(I,N,BLD)*XBARI(2)
C     PR00(2)=C(J,M,BLD)*XBARI(1) + C(J,N,BLD)*XBARI(2)
C
C     VECT(1)=YBARI(1) - E(I,BLD) - PR00(1)
C     VECT(2)=YBARI(2) - E(J,BLD) - PR00(2)
C     DET=C(I,P,BLD)*C(J,Q,BLD) - C(I,Q,BLD)*C(J,P,BLD)
C
C     XBARI(1)=(C(J,Q,BLD)*VECT(1) - C(I,Q,BLD)*VECT(2))/DET
C     XBARI(2)=(C(I,P,BLD)*VECT(2) - C(J,P,BLD)*VECT(1))/DET
C
C     S(M,1)=XBARI(1)
C     S(V,1)=XBARI(2)
C     S(P,1)=XBARI(2)
C     S(U,1)=XBARI(2)
C
C     GENERATE THE FIELD SOLUTION
C
C     JLD=1
C     NEW=2
C     DB 190 K=1,NSTA
C     Y(K)=S(I,BLD)
C     PSI(K)=S(I2,BLD)
C     MM(K)=S(I3,BLD)
C     V(K)=S(I4,BLD)
C     ALPHA(K)=V(K)*AG(4)
C     PSIPRM(K)=MM(K)/E(I,K)
C     YPRIME(K)=PSI(K)-ALPHA(K)
C
C     T(1,3)=DLT2/E(I,K)
C     T(1,4)=DLT3/E(I,K) - DLT*AG(4)
C     T(2,3)=DLT/E(I,K)
C     T(2,4)=T(1,3)
C     R(1)=DLT4/E(I,K) - DLT2*AG(4)
C     R(2)=DLT3/E(I,K)
C     DB 192 I=1,4
C     S(I,NEW)=0..
C     DB 172 J=1,4
C     170 S(I,NEW)=S(I,NEW) + T(I,J)*S(J,BLD)
C     180 S(I,NEW)=S(I,NEW) + QQ(K)*R(I)
C
C     TEMP=JLD
C     OLD=NEW
C     190 NEW=TEMP
C     ALPHA(NSEG+1)=V(NSEG+1)*AG(VSEG)
C     PSIPRM(NSEG+1)=MM(NSEG+1)/E(I,VSEG)
C     YPRIME(NSEG+1)=PSI(NSEG+1)-ALPHA(NSEG+1)
C     IF(IOUT.EQ.0) GO TO 191
C     WRITE(6,300) (I,Y(I),PSI(I),MM(I),V(I),ALPHA(I),YPRIME(I),
C     *           PSIPRM(I),E(I,I),QQ(I) ,I=1,NSTA)
C
C     COORDINATE TRANSFORMATION -- ZERO END DISPLACEMENTS
C
C     191 SL0PE=Y(NSTA)-Y(1)/BL
C     DLTY=SL0PE*DLT

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YLIN=Y(1)
DB 195 I=1,NSTA
PSI(I)=PSI(I)-SL0PE
Y(I)=Y(I)-YLIN
195 YLIN=YLIN+DLTY
C
C     NORMALIZATION
C
C     YMAX=ABSY(I)
C     DB 200 I=2,NSTA
C     200 YMAX=AMAX1(ABS(Y(I))),YMAX
C     DB 210 I=1,NSTA
C     Y(I)=Y(I)/YMAX
C     PSI(I)=PSI(I)/YMAX
C     PSIPRM(I)=PSIPRM(I)/YMAX
C     ALPHA(I)=ALPHA(I)/YMAX
C     210 YPRIME(I)=PSI(I)-ALPHA(I)
C
C     IF(IOUT.EQ.0) GO TO 400
C     WRITE(6,223)
C     220 FORMAT(77HNORMALIZED FUNCTION -- MAXIMUM DISPLACEMENT OF UNITY,
C     *        240
C     *        =ZERO END DISPLACEMENTS)
C
C     WRITE(6,300) (I,Y(I),PSI(I),MM(I),V(I),ALPHA(I),YPRIME(I),
C     *           PSIPRM(I),E(I,I),QQ(I) ,I=1,NSTA)
C     241
300 FORMAT(1HO/
*20K10HCRSS SECT,14X,21SHSHEAR,7X),5HTOTAL,7X,3HPSI,33X,4HL0AD/
*5H STA.,3X,10HDEFLECT18N,2X,8HBTAT18N,4X,6HM0MEYT,6X,5HFRCE,7X,
*5HANGLE,7X,5HSL0PE,7X,5HPRIME,7X,2HE1,10X,2HCA,1DX,9HINTENSITY//,
*(I4,2X,1P1DE12-4))
400 RETURN
END

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LMSD C56D - EFN SOURCE STATEMENT - IFN(S) - 12/15/66

SUBROUTINE COMP
COMMON/MISC/ N, BL(12), SL(12), NP(12), NF(12), V2(12), PVU(12),
BM(12), BD(12), PPTBN(12), TITLE(12), REF(12),
NP(12), VP(24), NEI(24), NGA(24), ISL(12), IBB(12),
NTZP, NTZP, NTB, NTT, NTP, TVM, XMC
COMMON/SHAPES/ MPI(900), IP(900), EI(900), SA(900),
MP(900), IP(1000), EI(1000), SA(1000),
Y(2600), YS(2600), Z(2600), YY(2600),
FMP, FIP, FEI, FGA
COMMON/INTGRLY/ R1(12), BJ(12), R2(12), Y1(12,4), Y2(12,4),
Y1(12,4), Y2(12,4), BYZ1(12,4,4), BYZ2(12,4,4),
S1(12,4,4), S2(12,4,4)
COMMON/SL0PES/ Y1PL(12,4), Y1PR(12,4), Y2PL(12,4), Y2PR(12,4)
COMMON/SPRING/ SSL1(12), SS1(12), SSL2(12), SSR2(12),
RSL1(12), RS1(12), RSL2(12), RSR2(12),
SK(12,4,4), SK8(12,2,2)
INTEGER OPT124
REAL IP, MP, IPI, MPI
COMPUTATION OF INTEGRALS INVOLVED IN THE KINETIC AND POTENTIAL ENERGY MATRICES
NTP=0
NBINT=0
DO 50 I=1,N
NBINT=NBINT + VP(I)-1
50 NTP=NTP+NP(I)
LL1=0
LL3=0
LL4=0
RK=1.0
IF(IOPFI(NN1).EQ.0) RR=0.0
KS=1.0
IF(IOPFI(N3).EQ.0) RS=0.0
DO 600 I=1,N
NP=NP(I)
NP1=NP(I-1)
NF=NF(I)
NPF=NP1-NF
DX=BL(I)/FL0AT(VP(I))
UX2=DX/2.0
DX4=DX/4.0
UM(I)=0.0
BJ(I)=0.0
DJX=0.0
R11=0.0
R12=0.0
C

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DO 95 L=1,NPI1
L1=L+LL1
L2=L1
X=DX*FL0AT(L)-DX2
UM(I)=UM(I) + MP(L1)*DX
BJ(I)=BJ(I) + MP(L1)*X*DX
BJX=BJX + MP(L1)*X*2*DX
K11=R11 + IP(L1)*DX
95 R12=R12 + IP(L2)*DX
R1(I)=BJX+R11*RR
R2(I)=BJX+R12*RR
IF(INFI.EQ.0) GO TO 550
DO 500 J=1,NF1
Y1(I,J)=0.0
Y1X=0.0
RZ1=0.0
RZ2=0.0
DO 200 L=1,NPI1
L1=L+LL1
L2=L1
L3=L+LL3
X=DX*FL0AT(L)-DX2
Y1(I,J)=Y1(I,J) + MP(L1)*(Y(L3)+Y(L3+1))*DX2
Y1X=Y1X + MP(L1)*(Y(L3)+Y(L3+1))*X*DX2
RZ1=RZ1 + IP(L1)*(Z(L3)+Z(L3+1))*DX2
200 RZ2=RZ2 + IP(L2)*(Z(L3)+Z(L3+1))*DX2
Y2(I,J)=Y1(I,J)
Y2L(I,J)=Y1PL(I,J)
Y2PL(I,J)=Y1PL(I,J)
Y2PR(I,J)=Y1PR(I,J)
LL5=0
DO 400 K=1,NF1
YY1=0.0
RZZ1=0.0
RZZ2=0.0
G18ND=0.
G28ND=0.
G1SH=0.
G2SH=0.
DO 300 L=1,NPI1
L1=L+LL1
L2=L1
L3=L+LL3
T1 -

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L4=L+LL4+LL5
G1BND = G1BND + E1(I1)*(YV(L3)+YV(L4)+YV(L3+1)*YV(L4+1))*DX2
G2BND = G2BND + E1(I2)*(YV(L3)+YV(L4)+YV(L3+1)*YV(L4+1))*DX2
G1SHR = G1SHR + GA(I1)*(YS(L3)+YS(L4)+YS(L3+1)*YS(L4+1))*DX2
G2SHR = G2SHR + GA(I2)*(YS(L3)+YS(L4)+YS(L3+1)*YS(L4+1))*DX2
YY1=YV1 + MP(I1)*(Y(L3)+Y(L4)+Y(L3+1)*Y(L4+1))*DX2
RZZ1=RZZ1+P(I1)*(Z(L3)+Z(L4)+Z(L3+1)*Z(L4+1))*DX2
300 RZZ2=RZZ2+P(I2)*(Z(L3)+Z(L4)+Z(L3+1)*Z(L4+1))*DX2
G1IJ,J,K) = G1BND + G1SHR*RS
G2IJ,J,K) = G2BND + G2SHR*RS
BYZ1(I,J,K)=YY1 + RZZ1*RR
BYZ2(I,J,K)=YY1 + RZZ2*RR
400 LL5=LL5+NPI
500 LL3=LL3+NPI
550 LL1=LL1+NPI
600 LL4=LL4+NPF
IVN=C,
VM0=J,
VN0=L,
DB 700 I=1,V
TVM=TVM + BW(I) + BM(I)
VM0=VM0 + BJ(I) + REF(I)*RW(I) + BM(I)*(REF(I)-BD(I))
XC1=B(I)/BW(I)
700 VN0=VN0 + RI(I) + BW(I)*(REF(I)+XC1)**2 - XC1**2
I + BM(I)*(REF(I)-BD(I))**2
      WRITE(1) MPI,IPI,EII,GAI,MP,IP,EI,GA
      WRITE(1) Y
      WRITE(1) YY
      WRITE(1) Z
      WRITE(1) VS
      REWIND 1
      CLVT2160 187
      DPUTPUT STATEMENTS FOR DATA INPUT AND COMPUTED TERMS
      NM1=V-1
      99 FORMAT(1H1)
      100 FORMAT(1H0)
      WRITE(6,101) TITLE
      101 FORMAT(25H1)PUT DATA F0LL3W * * *,12A6) 188
      WRITE(6,102) V
      102 FORMAT(//5H0V = I2) 190
      WRITE(6,103) #PTION 191
      103 FORMAT(8H0OPT1#VS,12I6)
      WRITE(6,105)
      105 FORMAT(5H0BEAM,9X,2HUL,15X,2HSL,15X,2HBM,15X,2HBD,15X,3HPU,8X,2HV
      11,3X,2HV2,3X,2HVP,2X,3HNP,2X,3HNP,2X,3HNE1,2X,3HNGA)
      WRITE(6,106)
      DB 10 I=1,V
      106 WRITE(6,107)I,BL(I),SL(I),BM(I),BD(I),PNU(I),VF(I),N2(I),NP(I),NMP
      I(I),NIP(I),NE(I),NGA(I) 194
      107 FORMAT(14,IX,5(2X,E15.8),7I5) 198

```

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```

      WRITE(6,99)
      J2=0
      DB 184 J=1,N
      WRITE(6,100)
      WRITE(6,101) J
      182 FORMAT(7H0BEAM I,12,1H)
      WRITE(6,183) J,VP(J) 218
      183 FORMAT(4H0NP(I,13,4H) = I3//8H STATION,12X,2HMP,18X,2HIP,18X,2HEI,
      *18X,2HGA)
      I=0
      J2=J2+NP(J)-1
      J1=J2-NP(J)+2
      DM 184 II=J1,J2
      I=I+
      184 WRITE(6,185) I,WP(I),IP(I),EI(I),GA(I) 227
      185 FORMAT(2X,13,2X,4(5X,E15.8))
      WRITE(6,100)
      WRITE(6,101)
      110 FORMAT(//28HICOMPUTED TERMS F0LL3W * * */5H0BEAM,11X,2HBM,17X,2HBJ
      1,17X,2HRL,17X,2H2)
      WRITE(6,100)
      DB 15 I=1,N
      15 WRITE(6,112)I,BW(I),BJ(I),RI(I),R2(I) 240
      112 FORMAT(4,IX,4(4X,E15.8))
      WRITE(6,100)
      WRITE(6,710) REF(I)
      710 FORMAT(27H0VEHICLE REFERENCE LOCATION/6H0REF *,E15.8//)
      XMC=VM0/TVM
      WRITE(6,720) TVN,XMC,VM0,VN0
      720 FORMAT(19H0TOTAL VEHICLE MASS/6H0TVW *,E15.8//38HDISTANCE TO CG F
      *RM VEHICLE REFERENCE/6H0XMC *,E15.8//37H0FIRST MOMENT ABOUT VEHIC
      *LE REFERENCE/6H0VMO *,E15.8//42H0MOMENT OF INERTIA ABOUT VEHICLE R
      *EFERENCE/6H0VMO *,E15.8)
      WRITE(6,100)
      WRITE(6,113) FMP,FIP,FEI,FGA
      113 FORMAT(34H0CONVERSION FACTORS FOR INPUT DATA//6H FMP *,E15.8/6H0FI
      *P *,E15.8/6H0FEL *,E15.8/6H0FGA *,E15.8) 249
      WRITE(6,115)
      115 FORMAT(33HILATERAL SUPPORT SPRING CONSTANTS/
      *5H0BEAM,10X,4HSSL1,15X,4HSSL2,15X,4HSSR1,15X,4HSSR2)
      WRITE(6,100)
      DB 29 I=1,N
      20 WRITE(6,112)I,SSL1(I),SSL2(I),SSR1(I),SSR2(I) 256
      WRITE(6,100)
      WRITE(6,116)
      116 FORMAT(36HROTATIONAL SUPPORT SPRING CONSTANTS/
      *5H0BEAM,10X,4HRSL1,15X,4HRSL2,15X,4HRSR1,15X,4HRSR2)
      WRITE(6,100)
      DB 21 I=1,N
      21 WRITE(6,112)I,RSL1(I),RSL2(I),RSR1(I),RSR2(I) 268
      WRITE(6,100)
      WRITE(6,118)
      118 FORMAT(29H BRANCH BEAM SPRING CONSTANTS//11HOSKB(I,J,K),18X,20H
      I=INTERSTAGE NUMBER)
      WRITE(6,100)
      WRITE(6,119)

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 119 FORMAT(3X,IHI,13X,7H(I,1,1),12X,7H(I,1,2),12X,7H(I,2,1),12X,7H(I,2,2))
 WRITE(6,100)
 DB 25 I=1,N
 25 WRITE(6,112)I,SKB(I,1,1),SKB(I,1,2),SKB(I,2,1),SKB(I,2,2)
 IF(N.LE.5) GO TO 27
 WRITE(6,99)
 27 WRITE(6,100)
 WRITE(6,123)
 291
 292
 293
 123 FORMAT(/2BH0INTERSTAGE SPRING CONSTANTS,/1DH0SK(I,J,K),19X,21HI =
 1INTERSTAGE NUMBER)
 WRITE(6,100)
 WRITE(6,151)
 DB 33 I=1,NM1
 WRITE(6,154) I
 DB 33 J=1,4
 33 WRITE(6,155)J,SK(I,J,1),SK(I,J,2),SK(I,J,3),SK(I,J,4)
 WRITE(6,117)
 309
 312
 315
 117 FORMAT(5HIBEAM,3X,7HSHP FCN,BX,2HY1,17X,2HY2,17X,3HY1,17X,3HY2)
 WRITE(6,100)
 DB 30 I=1,N
 WRITE(6,120) I
 DB 30 J=1,4
 30 WRITE(6,125) J,Y1(I,J),Y2(I,J),YZ1(I,J),YZ2(I,J)
 120 FORMAT(1H ,13)
 125 FORMAT(11X,I1,4(4X,E15.8))
 IF(N.LE.5) GO TO 31
 WRITE(6,99)
 31 WRITE(6,100)
 WRITE(6,127)
 325
 326
 327
 127 FORMAT(5H0BEAM,3X,7HSHP FCY,TX,4HY1PL,15X,4HY2PL,15X,4HY1PR,15X,4H
 1YZPK)
 WRITE(6,100)
 DB 40 I=1,N
 WRITE(6,120) I
 DB 40 J=1,4
 40 WRITE(6,125) J,Y1PL(I,J),Y2PL(I,J),Y1PR(I,J),Y2PR(I,J)
 334
 341
 150 FORMAT(10H1G(I,J,K),27X,15I = BEAM NUMBER,8X,28HJ,K = SHAPE FUNC
 1T18N NUMBERS)
 WRITE(6,100)
 342
 343
 151 WRITE(2X,1HI,3X,1HJ,4X,14H = 1,18X,1H2,18X,1-3,18X,1H4)
 DB 45 I=1,N
 WRITE(6,154) I
 346
 154 FORMAT(1H ,12)
 DB 45 J=1,4
 45 WRITE(6,155) J,G1(I,J,1),G1(I,J,2),G1(I,J,3),G1(I,J,4)
 155 FORMAT(16X,I1,5X,4(4X,E15.8))
 IF(N.LE.5) GO TO 51
 WRITE(6,99)
 51 WRITE(6,100)
 WRITE(6,160)
 359
 360
 361
 160 FORMAT(10H0G2(I,J,K),27X,15I = BEAM NUMBER,8X,28HJ,K = SHAPE FUNC
 1T18N NUMBERS)
 WRITE(6,100)
 362

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 C56D - EFN SOURCE STATEMENT - IFN(S) - 12/15/66
 WRITE(6,151)
 DB 60 I=1,N
 WRITE(6,154) I
 DB 60 J=1,4
 60 WRITE(6,155) J,G2(I,J,1),G2(I,J,2),G2(I,J,3),G2(I,J,4)
 WRITE(6,170)
 369
 376
 170 FORMAT(12H1BYZ1(I,J,K),25X,15HI = BEAM NUMBER,8X,28HJ,K = SHAPE FU
 INCT18N NUMBERS)
 WRITE(6,100)
 DB 70 I=1,N
 WRITE(6,154) I
 DB 70 J=1,4
 70 WRITE(6,155) J,BYZ1(I,J,1),BYZ1(I,J,2),BYZ1(I,J,3),BYZ1(I,J,4)
 IF(N.LE.5) GO TO 71
 WRITE(6,99)
 71 WRITE(6,100)
 WRITE(6,180)
 383
 393
 394
 395
 180 FORMAT(12H0BYZ2(I,J,K),25X,15HI = BEAM NUMBER,8X,28HJ,K = SHAPE FU
 INCT18N NUMBERS)
 WRITE(6,100)
 WRITE(6,151)
 DB 80 I=1,N
 WRITE(6,154) I
 DB 80 J=1,4
 80 WRITE(6,155) J,BYZ2(I,J,1),BYZ2(I,J,2),BYZ2(I,J,3),BYZ2(I,J,4)
 RETURN
 END

LMSC
 C56A - EPV SOURCE STATEMENT - EPV(S) - 12/15/66
 SUBROUTINE MATA8(IND) C56D0010
 CONSTRUCTION OF KINETIC AND POTENTIAL ENERGY COEFFICIENT MATRICES C56D0020
 CBMM8V/MISC/ N, BL(12), SL(12), NP(12), NI(12), V2(12), PNU(12), C56D0030
 * BN(12), BD(12), OPT10(NI12), TITLE(12), REF(12), C56D0040
 * NNP(12), NIP(24), NEI(24), VGA(24), ISL(12), IBB(12), C56D0050
 * NT2P, NT4P, NT81, NT8, NT7, NTP, TWM, XMC
 COMMON/SL0PES/ Y1PL(12,4), Y1PR(12,4), Y2PL(12,4), Y2PR(12,4) C56D0070
 COMMON/INTGRAL/ BW(12), BJ(12), R1(12), R2(12), Y1(12,4), Y2(12,4), C56D0090
 * YZ1(12,4), YZ2(12,4), BY1(12,4,4), BY2(12,4,4),
 * G1(12,4,4), G2(12,4,4)
 COMMON/SPRING/ SSL1(12), SSL1(12), SSL2(12), SSR2(12), C56D0130
 * RSL1(12), RSL1(12), RSL2(12), RSL2(12),
 * SK(12,4,4), SX(12,2,2)
 DIMENSION A(60,60), B(60,60) C56D0160
 DIMENSION C(44,60), PNU(12), CNU(12), SNU(12), S(44,44), Q(60,60) C56D0170
 DIMENSION B11(12), B12(12) C56D0180
 INTEGER OPTION C56D0190
 NUL=N-1 C56D0200
 DO 100 I=1,NUL C56D0210
 PNU(I)=ABS(PNU(I))-PNU(I+1) C56D0220
 CNU(I)=COS(PNU(I)) C56D0230
 100 SNU(I)=SIN(PNU(I)) C56D0240
 10 SNU(I)=SIN(PNU(I)) C56D0390 10
 WRITE(6,200) PNU, CNU, SNU C56D0400 14
 200 FORMAT(8H1PNU(1),5X,6E18.8/13X,6E18.8/7HOCNU(1),6X,6E18.8/13X, C56D0280 17
 * 6E18.8/7HOSNU(1),6X,6E18.8/13X,6E18.8) C56D0290
 DEFINITIONS C56D0300
 IND=0 C56D0310
 NTR=0
 KT1=0
 IF(NU1.EQ.0) GO TO 1010
 DO 1000 I=1,NUL
 ISL(I)=0
 NN=4
 IF((SL(I)/BL(I)).GT.1.E-10) GO TO 1000
 ISL(I)=1
 KT1=KT1+1
 NN=2
 1000 NTR=NTR+NN
 1010 NB1=0
 NB2=0
 KT2=0
 DO 1050 I=1,N
 B11(I)=0.

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 C56A - EPV SOURCE STATEMENT - EPV(S) - 12/15/66
 B12(I)=0.
 NB1=NB1+NI(I)
 NB2=NB2+N2(I)
 IBB(I)=0
 IF(BM(I).LT.1.E-35) GO TO 1050
 IBB(I)=1
 KT2=KT2+1
 1050 CONTINUE
 NT2P=2*N-KT1
 NT4P=2*NT2P
 NTB1=NT4P+NB1
 NTB=NTB1+NB2
 NTT=NTB+2*KT2
 IF(VTT.GT.60) GO TO 2300
 CONSTRUCTION OF THE KINETIC ENERGY MATRIX, A
 TERMS IN THE POTENTIAL ENERGY MATRIX, B, DUE TO SUPPORT SPRINGS,
 BRANCH BEAMS, AND BEAM BENDING WILL BE INSERTED AT THIS TIME
 DO 1100 J=1,NTT
 DO 1100 I=1,NTT
 A(I,J)=0.0
 1100 A(I,J)=0.0
 I1=1
 I2=NT2P+1
 I3=NTB+1
 J1C=NT4P
 J2C=NT4P+NB1
 DO 1200 I=1,
 R1BL=R1(I)/BL(I)**2
 R2BL=R2(I)/BL(I)**2
 BJBL=2.0*BJ(I)/BL(I)
 RSLR1=(RSL1(I)+RSL1(I))/BL(I)**2
 RSLR2=(RSL2(I)+RSL2(I))/BL(I)**2
 BMD1=BM(I)*BD(I)**2 + B(I(I))
 BMD2=BM(I)*BD(I)**2 + B(I2(I))
 BMBL= BM(I)*BD(I)/BL(I)
 BLSQ =BL(I)**2
 A(I1,I1)=A(I1,I1) + BM(I) + R1BL - BJBL
 A(I1+1,I1+1)=R1BL
 A(I2,I2)=A(I2,I2) + BM(I) + R2BL - BJBL
 A(I2+1,I2+1)=R2BL
 A(I1,I1+1)=-R1BL + R1BL/2.0
 A(I2,I2+1)=-R2BL + R2BL/2.0
 B(I1,I1)=B(I1,I1) + RSLR1 + SSL1(I)
 B(I1+1,I1+1)=B(I1+1,I1+1) + RSLR1 + SSR1(I)
 B(I1,I1+1)=B(I1,I1+1) - RSLR1
 B(I2,I2)=B(I2,I2) + RSLR2 + SSL2(I)
 B(I2+1,I2+1)=B(I2+1,I2+1) + RSLR2 + SSR2(I)
 B(I2,I2+1)=B(I2,I2+1) - RSLR2

BRANCH BEAM TERMS

2) - 1)

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```
C      IF(I1BB(I),EQ.0) G0 T0 1110
      A(I1,I1)=A(I1,I1) + BM(I) + BMDII/BLSQ + BM8DL*2.
      A(I2,I2)=A(I2,I2) + BM(I) + BMDI2/BLSQ + BM8DL*2.
      A(I1+1,I1+1)=A(I1+1,I1+1) + BMDII/BLSQ
      A(I2+1,I2+1)=A(I2+1,I2+1) + BMDI2/BLSQ
      A(I1,I1+1)=A(I1,I1+1) - BMDII/BLSQ - BM8DL
      A(I2,I2+1)=A(I2,I2+1) - BMDI2/BLSQ - BM8DL
      A(I3,I3)=BMDII
      A(I3+1,I3+1)=BMDII
      A(I1,I3)=BMDII/BL(I) + BM(I)*BD(I)
      A(I2,I3)=BMDI2/BL(I) + BM(I)*BD(I)
      A(I1+1,I3)=BMDII/BL(I)
      A(I2+1,I3)=BMDI2/BL(I)

C      B(I3,I3)=SKB(I,1,1)
      B(I3+1,I3+1)=SKB(I,1,2)
      B(I3+1,I3+1)=SKB(I,2,2)

C      1110 N1=I1(N1)
      N2=N2(N1)
      IF(N111.EQ.0) G0 T0 1140
      D0 1130 J=1,N1
      J1=J1C+J
      A(I1,J1)=Y1(I,J)-YZ1(I,J)/BL(I)
      A(I1+1,J1)=YZ1(I,J)/BL(I)
      TRM1=Y1PL(I,J)*RSL1(I) + Y1PR(I,J)*RSR1(I)
      B(I1,J1)=B(I1,J1) - TRM1/BL(I)
      B(I1+1,J1)=B(I1+1,J1) + TRM1/BL(I)
      IF(I1BB(I),EQ.0) G0 T0 1120
      A(I1,J1)=A(I1,J1) - Y1PL(I,J)*(BMDII/BL(I) + BM(I)*BD(I))
      A(I1+1,J1)=A(I1+1,J1) + Y1PL(I,J)*BMDII/BL(I)
      A(I1,J1)=Y1PL(I,J)*BMDII
      A(J1,I3)=Y1PL(I,J)*BMDII
      K1=J1C*K
      B(J1,K1)=B(J1,K1) + Y1PL(I,J)*Y1PL(I,K)*RSL1(I)
      + Y1PR(I,J)*Y1PR(I,K)*RSR1(I) + G1(I,J,K)
      1130 A(I1,K1)= BYZ1(I,J,K) + Y1PL(I,J)*Y1PL(I,K)*BMDII
      J1C=J1C+N1(I)

C      1140 IF(N21.EQ.0) G0 T0 1170
      D0 1160 J=1,N21
      J2=J2C+J
      A(I2,J2)=Y2(I,J) - YZ2(I,J)/BL(I)
      A(I2+1,J2)=YZ2(I,J)/BL(I)
      TRM2=Y2PL(I,J)*RSL2(I) + Y2PR(I,J)*RSR2(I)
      B(I2,J2)=B(I2,J2) - TRM2/BL(I)
      B(I2+1,J2)=B(I2+1,J2) + TRM2/BL(I)
      IF(I1BB(I),EQ.0) G0 T0 1150
      A(I2,J2)=A(I2,J2) - Y2PL(I,J)*(BMDI2/BL(I) + BM(I)*BD(I))
      A(I2+1,J2)=A(I2+1,J2) + Y2PL(I,J)*BMDI2/BL(I)
      A(J2,I3)=Y2PL(I,J)*BMDI2
      D0 1160 K=J2,N21
      K2=J2C+K
      B(J2,K2)=B(J2,K2) + Y2PL(I,J)*Y2PL(I,K)*RSL2(I)
      + Y2PR(I,J)*Y2PR(I,K)*RSR2(I) + G2(I,J,K)
```

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```
I1BB(I).EQ.1) G0 T0 1180
      I1=I1+2
      I2=I2+2
      G0 T0 1200
      I1=I1+1
      I2=I2+1
      1200 IF(I1BB(I).EQ.1) I3=I3+2
C      DB 1300 I=1,NTT
      DB 1300 J=1,I
      B(I,J)=B(I,J)
      1300 A(I,J)=A(J,I)

C      CONSTRUCTION OF THE ANGULAR DISPLACEMENT COEFFICIENT MATRIX, C
C      DB 1400 J=1,NTT
      DB 1400 I=1,NTR
      1400 C(I,J)=0.0

C      RIGID BODY ROTATION TERMS
C      I1=1
      J1=1
      J2=NT2P+1
      J1K=NT4P
      J2K=NT81
      IF(YU1.EQ.0) G0 T0 2000
      DM 1600 K=1,NU1
      CBL=CNU(K)/BL(K+1)
      SBL=SNU(K)/BL(K+1)
      TERM=(1./SL(K)+1./BL(K+1))
      IF(I1SL(K).EQ.0) G0 T0 1450
      I=I1
      C(I,J1)=1./BL(K)
      C(I,J1+1)=-1./BL(K)-1./SL(K)
      C(I,J1+2)=CNU(K)/SL(K)
      C(I,J2+2)=SNU(K)/SL(K)

C      I=I1+1
      C(I,J1+1)=1./SL(K)
      C(I,J1+2)=-TERM*CNU(K)
      C(I,J1+3)=CBL
      C(I,J2+2)=-TERM*SNU(K)
      C(I,J2+3)=SBL

C      I=I1+2
      C(I,J1+2)=-SNU(K)/SL(K)
      C(I,J2)=1./BL(K)
      C(I,J2+1)=-1./BL(K)-1./SL(K)
      C(I,J2+2)=CNU(K)/SL(K)

C      I=I1+3
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      C(I,J1+2)=TERM*SNU(K)
      C(I,J1+3)=-SBL
      C(I,J2+1)=1./SL(K)
      C(I,J2+2)=-TERM*CNU(K)
      C(I,J2+3)=CBL
      G# T# 1500

      C
      1450 I=I1
      C
      C(I,J1)=1./BL(K)
      C(I,J1+1)=-1./BL(K) - CBL
      C(I,J1+2)=CBL
      C(I,J2+1)=-SBL
      C(I,J2+2)=SBL

      C
      I=I1+1
      C(I,J1+1)=SBL
      C(I,J1+2)=-SBL
      C(I,J2)=1./BL(K)
      C(I,J2+1)=-1./BL(<) - CBL
      C(I,J2+2)=CBL

      C
      TERMS DUE TO BENDING

      1500 I=I1
      NIK=N1(K)
      IF(N1(K).EQ.0) G# T# 1520
      D# 1510 L=1,NIK
      J=J1K+L
      1510 C(I,J)=-Y1PR(K,L)

      C
      1520 I=I1+2
      IF(1SL(K).EQ.0) I=I1+1
      N2K=N2(K)
      IF(N2(K).EQ.0) G# T# 1540
      D# 1530 L=1,N2K
      J=J2K+L
      1530 C(I,J)=-Y2PR(K,L)

      C
      1540 I=I1+1
      I1=I1+2
      IF(1SL(K).EQ.0) G# T# 1550
      I=I1
      I1=I1+1
      I1=I1+1
      1550 IF(N1(K+1).EQ.0) G# T# 1570
      NIK=N1(K+1)
      D# 1560 L=1,NIK1
      J=J1K+N1K+L
      C(I,J)= CNU(K)*Y1PL(K+1,L)
      1560 C(I1,J)=-SNU(K)*Y1PL(K+1,L)

      C
      1570 IF(N2(K+1).EQ.0) G# T# 1590
      N2K1=N2(K+1)
      D# 1580 L=1,N2K1
      J=J2K+N2K+L
      C(I,J)= SNU(<)*Y2PL(K+1,L)

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      LMSG          - EFN  SJRCE STATEMENT - IFN(S) -           12/15/66
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      1580 C(I1,J)= CNU(<)*Y2PL(K+1,L)

      C
      1590 J1K=J1K+N1(K)
      J2K=J2K+N2(K)
      I1=I1+2
      J1=J1+1
      J2=J2+1
      IF(1SL(K).EQ.0) G# T# 1600
      I1=I1+2
      J1=J1+1
      J2=J2+1
      1600 CONTINUE

      C
      WRITE(6,1610)
      1610 FORMATTISHITHE ANGULAR DISPLACEMENT COEFFICIENT MATRIX, C FOLLOWS)
      CALL RECMAT(C,NTX,NTY,44,63)                                518

      C
      CONSTRUCTION OF STIFFNESS MATRIX, S                         519

      JSK=0
      D# 1620 J=1,NTR
      D# 1620 I=1,NTR
      1620 S(I,J)=0.0
      D# 1660 I=1,NU1
      L=4
      IF(1SL(I).EQ.0) L=2
      D# 1650 J=1,L
      D# 1650 K=J+L
      JS=JSK+J
      KS=JSK+K
      1650 S(JS,KS)=SK(I,J,K)
      JSK=JSK+
      IF(1SL(L).EQ.0) JSK=JSK-2
      1660 CONTINUE
      D# 1700 I=1,JS
      D# 1700 J=1,I
      1700 S(I,J)=S(J,I)

      C
      WRITE(6,1710)
      1710 FORMATTISHITHE STIFFNESS MATRIX, S FOLLOWS)
      CALL RECMAT(S,JS,JS,44,44)

      C
      CONSTRUCTION OF THE POTENTIAL ENERGY MATRIX, B

      C
      TERMS DUE TO SPRINGS                                     567

      D# 1800 J=1,NTB
      D# 1800 I=1,NTR
      Q(I,J)=0.0
      D# 1800 K=1,NTR
      1800 Q(I,J)+Q(I,J) + S(I,K)*C(K,J)

      C
      D# 1850 J=1,NTB
      D# 1850 I=1,NTB
      D# 1850 K=1,NTR

```

LMSL
C56A - EFN SOURCE STATEMENT - IFN(S) - 12/15/66

C
1850 B(I,J)=B(I,J)+C(K,I)*Q(K,J)
C CONSTRUCTION OF A AND B IS COMPLETE C56D3293
C56D3213
2000 WRITE(6,2250)
2250 FORMAT(2TH1THE K.E. MATRIX, A FOLLOWING)
CALL OUTMAT(A,NTT)
WRITE(6,2200)
2200 FORMAT(2TH1THE P.E. MATRIX, B FOLLOWING)
CALL OUTMAT(B,NTT)
C
WRITE(3) ((A(I,J),J=1,I),I=1,NTT), ((B(I,J),J=1,I),I=1,NTT)
REWIND 3
C
2300 GO TO 2500
IND=1
WRITE(6,2400)
2400 FORMAT(61HMATRIX DIMENSION IS GREATER THAN 60, EXECUTION IS TERMINATED)
*NATED)
2500 RETURN
END

```

LMSG          - EFN  SJRCE STATEMENT - IFN(S) -      12/15/66

C SOLUTION OF THE SYSTEM -BMEGA**2*A*EX + B*EX = 0 BY CHOLESKI TRANS. CLVTD010
C INPUT -- A AND B MATRICES CLVTD020
C OUTPUT-- NORMIALIZED SYSTEM EIGENVECTORS, SYSTEM FREQUENCIES IN CPS, CLVTD030
C AND GENERALIZED MASS FOR EACH MODE CLVTD040
C SUBROUTINE CLVTG02(N,IND)
C DOUBLE PRECISION AA, DD, DW, EV, CLM, OCC CLVTD050
C INTEGER OPTION CLVTD060
C COMMON/MISC/ NB,BL(12), SL(12), NP(12), NL(12), N2(12), PNU(12), CLVTD070
C * BM(12), BD(12), OPTION(12), TITLE(12), REF(12),
C * NMP(12), NIP(24), NEI(24), NG(124), ISL(12), IBB(12),
C * NTZP, NT4P, NT3L, NTB, NTI, NTP, TVM, XMC CLVTD080
C COMMON/TRANS/ DD(60,60), DW(60), AA(60,60), DUM1(120), CLM(60), CLVTD090
C * DUM2(540) CLVTD100
C DIMENSION E(60,60), W(60), GMV(60) CLVTD110
C DIMENSION A(60,60), B(60,60), EV(60,60), QU(60,60), QL(60,60) CLVTD120
C EQUIVALENCE (A,A), (A,QL), (A(360),B), (AA(1,2),EV), (AA,E), CLVTD130
C * (IS1360),QUL), (W,DUM2), (GMV,DUM2(61)) CLVTD140
C DIMENSION NAME(4) CLVTD150
C DATA(NAME(I),I=1,4)/4HUL1/, 4HUR1/, 4HUL2/, 4HUR2/ CLVTD160
C CLVTD170
C IND=0 CLVTD180
C READ (3) ((A(I,J),J=1,I),I=1,N), ((B(I,J),J=1,I),I=1,N) CLVTD190
C CLVTD220
C NN=N CLVTD230
C DO 100 I=1,N CLVTD240 2
C DO 100 J=1,I
C 100 B(J,I)=B(I,J) CLVTD250
C COMPUTE P INVERSE (A=PP*) CLVTD260
C CLVTD270
C 105 DO 106 J=1,NN CLVTD280
C 106 AA(I,J)=A(I,J) CLVTD290
C CALL DPCHOL(AA,NN,IN,60) CLVTD300
C IF(I<4.EQ.0) GO TO 115 CLVTD310
C IND=1
C INN=IN+N-NN
C WRITE(6,110) INN,AA(IN,IN) CLVTD320
C 110 FORMAT(15H0**F8.2** MATRIX A IS NOT POSITIVE DEFINITE. DIAGONAL CLVTD330
C IN0.13,53H IS NEGATIVE WHICH INDICATES NEGATIVE KINETIC ENERGY./ CLVTD340
C 212X,24HEXECUTION IS SUPPRESSED./,1H0,11X, 8HDIAG = ,D15.9) CLVTD350
C
C RAT=AA(IN,IN)/AA(IN,IN) 45
C IF(I<5,NEQ.0) WRITE(6,111) RAT,INN
C 111 FORMAT(1H0,11X,8HRRATI0 = ,E15.8,3BH THIS INDICATES THAT COORDINA 51
C * TE NO. 13,14H IS REDUNDANT//)
C
C IF IN IS NOT ZERO DELETE THE ROW AND COLUMN OF MATRIX A CORRESPONDING
C TO IN AND ATTEMPT THE CHOLESKY TRANSFORMATION AGAIN. REPEAT THIS
C PROCESS UNTIL A SUCCESSFUL TRANSFORMATION IS MADE. AT THIS POINT
C EXIT FROM THE ROUTINE WITH THE ERROR INDICATOR SET EQUAL TO ONE.
C
C LIM=NN-1
C DO 113 I=IN,LIM

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LMSG          - EFN  SJRCE STATEMENT - IFN(S) -      12/15/66

C IP1=I+1
C DO 112 J=IP1,NN CLVTD390
C 112 AA(I,J)=AA(I,J) CLVTD400
C DO 113 J=1,I CLVTD410
C 113 AA(I,J)=A(I+1,J)
C NN=NN-1
C DO 115 TO 105
C 115 IF(IND.EQ.1) GO TO 5100
C COMPUTE P(-1) B P*(-1) = F      (PP*=A) CLVTD420
C CLVTD430
C DO 120 I=1,N CLVTD440
C DO 120 J=1,I CLVTD450
C EV(I,J)=0.0 CLVTD460
C DO 120 K=1,I CLVTD470
C 120 EV(I,J)=EV(I,J)+AA(I,K)*B(K,J) CLVTD480
C DO 130 I=1,N CLVTD490
C DO 130 J=1,I CLVTD500
C DD(I,J)=C*OC CLVTD510
C DO 125 K=1,J CLVTD520
C 125 DD(I,J)=DD(I,J)+EV(K,I)*AA(J,K) CLVTD530
C 130 DD(I,J)=DD(I,J) CLVTD540
C WRITE(6,135) CLVTD550 116
C 135 FORMAT(13H2H1P(-1) B P*(-1) = F      (PP*=A))
C CALL OUT2(DD,N)
C
C WRITE (3) ((AA(I,J),J=1,I),I=1,N) CLVTD560 117
C REMIND 3 CLVTD570 118
C READ(3) DUM CLVTD580 129
C
C COMPUTE EIGEN-SYSTEM OF F MATRIX. VECTORS IN DD
C CALL SCLWK1(D1,TIME1,ESEC1,02) CLVTD590
C CALL DEIGEN(N) CLVTD600
C CALL SCLWK1(D1,TIME2,ESEC2,02) CLVTD610 130
C NSEC=ESEC2-ESEC1
C WRITE(6,137) TIME1,TIME2,NSEC 131
C 137 FORMAT(//35H TIME CHECK FOR EIGENVALUE SOLUTION/10H TIME IN A/6/
C * 10H TIME BUT A/6/14H DELAPSED TIME 13,8H SECONDS) 133
C * WRITE(6,140) CLVTD620
C 140 FORMAT(24H1EIGENVALUES OF F MATRIX//) CLVTD630 138
C WRITE(6,145)(1,DW(I)),I=1,N) CLVTD640
C 145 FORMAT(4H DW([2,4H]) = D23.16) CLVTD650 139
C IND=0 CLVTD660
C DO 160 I=1,N CLVTD670
C IF(DW(I).GE.0.) GO TO 160 CLVTD680
C WRITE(6,155) I, DW(I) CLVTD690 153
C 155 FORMAT(12H ERROR-- DW([2,2H])=,1PE15.7,49H, ABSOLUTE VALUE OF DW CLVTD700
C USED CALCULATIONS CONTINUE)
C DW(I)=DAUS(DW(I)) CLVTD710
C IND=1 CLVTD720
C 160 W(I)=DSORT(DW(I))/6.2831853 CLVTD730 159
C WRITE(6,153) CLVTD740
C 150 FORMAT(25H1EIGENVECTORS OF F MATRIX) CLVTD750 162
C CALL OUT2(DD,N) CLVTD760
C CALL OUTH(DD,N) CLVTD770 163
C CLVTD780

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      LMSC          CLVT      - FPN  SOURCE STATEMENT  IFV(S) -  12/15/66
      : COMPUTE SYSTEM EIGENVECTORS - ?*(-1) TIMES VECTORS 2F F
      : READ P*(-1) AND STORE IN AA
      :   READ (3) ((AA(J,I),J=1,1),I=1,N)
      :   REWIND 3
      :   DO 170 I=1,N
      :     DO 165 J=1,N
      :       CLM(J)=0.00
      :       DO 165 K=1,N
      :         165 CLM(J)=CLM(J) + AA(I,K)*DO(I,J)
      :         DO 170 J=1,N
      : 170 AA(I,J)=CLM(J)
      : NORMALIZE VECTORS
      :   DO 200 J=1,N
      :     DCC=ABS(AA(1,J))
      :     DO 190 I=2,N
      : 190 DCC=MAX1(DCC,ABS(AA(I,J)))
      :     DCC=1./DCC
      :     GMV(J)=DCC*I2
      :     DO 200 I=1,N
      : 200 E(I,J)=AA(I,J)*DCC
      : REVERSE ORDER OF MODES
      :   ND2=N/2
      :   DO 205 J=1,ND2
      :     N=N-J+1
      :     DCC=W(J)
      :     W(J)=W(NJ)
      :     W(NJ)=DCC
      :     DCC=GMV(J)
      :     GMV(J)=GMV(NJ)
      :     GMV(NJ)=DCC
      :     DCC=0.0
      :     DM(J)=DM(NJ)
      :     DM(NJ)=DCC
      :     DO 205 I=1,N
      :       CLM(I)=E(I,J)
      :       E(I,J)=E(I,NJ)
      : 205 E(I,NJ)=CLM(I)
      : J6=NNT
      : WRITE(6,3400)
3400 FORMAT(36H1SYSTEM EIGENVALUES AND EIGENVECTORS)
      NBLBK= J6/9
      IF((9*NBLBK).LT.J6)  NBLBK=NBLBK+1
      M1=1
      DO 4300 MBLBK=1,NBLBK
      M2=M1+8
      IF(MBLBK.EQ.NBLBK)  M2=J6
      WRITE(6,3700) (I,I=M1,M2)
3700 FORMAT(2(IH//15HD0UE,1X,9(12)

```

```

      LMSC          CLVT      - FPN  SOURCE STATEMENT  - IFV(S) -  12/15/66
      : WRITE(6,3800) (W(I),I=M1,M2)
3800 FORMAT(6H0REQ.,6X,9F12.6)
      : WRITE(6,3850) (GMV(I),I=M1,M2)
3850 FORMAT(10H GEN. MASS,2X,1P9E12.4)
      : WRITE(6,1265)
1265 FORMAT(1H )
      : MN=0
      : IR=1
      : DO 4020 L=1,2
      :   DO 4010 I=1,NB
      :     DO 4000 J=1,2
      :       JMN=J-MN
      :       WRITE(6,4030) NAME(JMN),I,(E(IR,K),K=M1,M2)
4000 IR=IR+1
      : IF(ILSL(I).EQ.1) IR=IR-1
4010 WRITE(6,1265)
4020 FORMAT(1H ,A4,I1,1H),5X,9F12.6)
      : MN=2
4020 IR=IR+1
      : IR=IR+2P+1
      : I3=NT4P+1
      : I4=NTB1+1
      : I5=NTB+1
      : DO 4110 I=1,NB
      :   K1=N1(I)
      :   IF(K1.EQ.0) GO TO 4110
      :   DO 4100 K=1,K1
      :     WRITE(6,3910) I,K,(E(I3,J),J=M1,M2)
4100 I3=I3+1
      : WRITE(6,1265)
4110 CONTINUE
3910 FORMAT(7H BLMD1(I,I1,1H,,I1,1H),1X,9F12.6)
      : DO 4210 I=1,NB
      :   L1=N2(I)
      :   IF(L1.EQ.0) GO TO 4210
      :   DO 4200 L=1,L1
      :     WRITE(6,3920) I,L,(E(I4,J),J=M1,M2)
4200 I4=I4+1
      : WRITE(6,1265)
4210 CONTINUE
3920 FORMAT(7H BLMD2(I,I1,1H,,I1,1H),1X,9F12.6)
      : DO 4250 I=1,NB
      :   IF((BB(I)).EQ.0) GO TO 4250
      :   WRITE(6,3930) I,(E(I5,J),J=M1,M2)
      :   WRITE(6,3940) I,(E(I5+1,J),J=M1,M2)
      :   WRITE(6,1265)
      :   I5=I5+2
4250 CONTINUE
3930 FORMAT(7H BETA1(I,I1,1H),3X,9F12.6)
3940 FORMAT(7H BETA2(I,I1,1H),3X,9F12.6)
4300 M1=M2+1
      : CALCULATION OF CHECK MATRICES
      : READ (3) ((A(I,J),J=1,1),I=1,N), ((B(I,J),J=1,1),I=1,N)

```

LMSC
 CLVT - EFN SOURCE STATEMENT - IFN(S) - 12/15/66
 REWIND 3 CLVT1830 378
 WRITE(3) E,W,GMV CLVT1830 379
 REWIND 3 CLVT1830 383
 DB 4350 I=1,N
 DB 4350 J=1,I
 A(I,J)=A(I,J)
 4350 B(I,J)=B(I,J)
 4390 DB 4500 J=1,J6 CLVT1840
 DB 4500 I=1,J6 CLVT1850
 QU(I,J)=0 CLVT1863
 DB 4400 K=1,J6 CLVT1873
 4400 QU(I,J)=QU(I,J)+ A(I,K)*E(K,J) CLVT1880
 4500 QU(I,J)=QU(I,J)+DB(I,J) CLVT1890
 DB 4550 J=1,J6 CLVT1890
 DB 4550 I=1,J6 CLVT1900
 QU(I,J)=0 CLVT1900
 DB 4400 K=1,J6 CLVT1910
 4400 QU(I,J)=QU(I,J)+ A(I,K)*E(K,J) CLVT1920
 4500 QU(I,J)=QU(I,J)+DB(I,J) CLVT1930
 DB 4550 J=1,J6 CLVT1940
 DB 4550 I=1,J6 CLVT1950
 QU(I,J)=0 CLVT1960
 DB 4550 K=1,J6 CLVT1970
 4550 QU(I,J)=QU(I,J)+ B(I,K)*E(K,J) CLVT1980
 DB 4600 I=1,J6 CLVT1990
 DB 4600 J=1,J6 CLVT2000
 E(I,J)=ABS(QU(I,J)-QL(I,J)) CLVT2010
 4600 WRITE(6,4700) CLVT2020
 4700 F8RMAT(3H14INACCURACY CHECK MATRICES FOLLOW/13H00MEGA**2*A*X) CLVT2033 452
 CALL BUTMAT(QU,J6) CLVT2043
 WRITE(6,4800) CLVT2053 453
 4800 F8RMAT(12H8*B*X VECTORS) CLVT2060 454
 CALL BUTMAT(QU,J6) CLVT2073
 WRITE(6,4900) CLVT2083 455
 4900 F8RMAT(27H18MEGA**2*A*X - B*X VECTORS) CLVT2093 456
 CALL BUTMAT(E,J6) CLVT2103
 WRITE(6,5000) CLVT2113 457
 5000 F8RMAT(24H16NORMALIZED ERROR MATRIX) CLVT2123 458
 CALL BUTMAT(B,J6) CLVT2130
 5100 RETURN CLVT2140 459
 END CLVT2173
 CLVT2180

LMSC
 CHBL - EFN SOURCE STATEMENT - IFN(S) - 12/15/66
 CHOLESKI REDUCTION AND TRIANGULAR INVERSION
 INPUT IS LOWER TRIANGULAR PART OF SYMMETRIC MATRIX B
 COMPUTATION IS B*PP*
 OUTPUT IS LOWER TRIANGULAR MATRIX P INVERSE
 SUBROUTINE DPCHBLA,IX,IS,IXX
 DIMENSION A(IXX,IXX)
 DOUBLE PRECISION A,DSQRT
 IS=J
 DB 40 ID=1,IX
 IDM1=ID-1
 IDP1=ID+1
 IF (IDM1) 10,20,10
 10 DB 15 I=ID,IX
 DB 15 K=1,IDM1
 15 A(I,1)=A(I,1)-A(ID,K)*A(I,K)
 20 IF (SNGL(A(I,1,1))) 25,25,30
 25 IS=10
 GO TO 75
 30 A(ID,1)=DSQRT(A(ID,1))
 IF (IDP1-IX) 35,35,45
 35 DB 40 I=IDP1,IX
 40 A(I,1)=A(I,1)/A(ID,1D)
 45 DB 55 ID=2,IX
 IDM1=ID-1
 DB 50 J=1,1DM1
 50 A(ID,J)=A(ID,J)/A(ID,1D)
 55 A(ID,1)=1.DC/A(ID,1D)
 A(1,1)=1.DD/A(1,1)
 IXM1=IX-1
 DB 70 I=1,IXM1
 IP1=I+1
 IM1=I-1
 DB 70 L=IP1,IX
 IF (IM1) 70,70,60
 60 DB 65 J=1,IM1
 65 A(L,J)=A(L,J)-A(L,I)*A(I,J)
 70 A(L,I)=-A(L,I)*A(I,I)
 75 RETURN
 END

28

CH0T0010
 CH0T0020
 CH0T0030
 CH0T0040
 CH0TC073
 CH0T0080
 CH0T0090
 CH0T0100
 CH0T0110
 CH0T0120
 CH0TC130
 CH0T0140
 CH0T0150
 CH0T0160
 CH0T0170
 CH0T0190
 CH0T0200
 CH0T0210
 CH0T0220
 CH0T0230
 CH0T0240
 CH0T0250
 CH0T0280
 CH0T0290
 CH0T0300
 CH0T0310
 CH0T0320
 CH0T0330
 CH0T0340
 CH0T0350
 CH0T0360
 CH0T0370
 CH0T0380

LMSC E56G - EFV SOURCE STATEMENT - IFN(S) - 12/15/66

EIGENVALUES AND EIGENVECTORS OF A REAL SYMMETRIC MATRIX DEGN001
 GIVES METHOD, DECK MODIFIED BY IRA HANSON AT LOCKHEED MISSILES DEGN002
 USE AS... CALL EIGEN(A,VALUE,N,M) WHERE A(N,N) AND VALUE(M) AND DEGN003
 A IS DESTROYED. IF M=0, IT WILL COMPUTE EIGENMATRIX DEGN004
 DEGN005
 SUBROUTINE DEIGEN (N) DEGN006
 DOUBLE PRECISION DSQRT DEGN007
 DOUBLE PRECISION A,B,VALU,DIAG,SUPERD,Q,VALL,S,C,D,U,PRBDS DEGN011
 1,T,SMALLD,(ANBRM,ANBRM2),T1,T2,COS,SIN,TAU,BETA,P DEGN012
 CMMN0/NTRANS/(A(60,60),VALU(60),B(60,60),DIAG(60),SUPERD(60), DEGN013
 Q(60),VALL(60),C(60),IND(60),DM(120)) DEGN014
 DIMENSION S(60), D(60), U(60) DEGN017
 FUJIVALENCE (VALL,D),(Q,S),(IND,U),(II,MATCH),(TAU,BETA),(P,PRBDS) DEGN020
 1,(T,SMALLD),(ANBRM,ANBRM2) DEGN021
 ABSF(X)=DABS(X) DEGN022
 SORF(X)=DSQRT(X) DEGN023
 MDUM=1 DEGN024
 M=1 DEGN025
NPBV MODIFICATION DEGN026
CALCULATE NORM OF MATRIX DEGN027
 3 ANBRM2=0.0 DEGN028
 4 DB 6 J=1,N DEGN029
 5 DB 6 J=1,N DEGN030
 6 ANBRM2=ANBRM2+A(I,J)**2 DEGN031
 7 ANBRM=SQR(ANBRM2) DEGN032
GENERATE IDENTITY MATRIX DEGN033
 9 IF (M) 10, 45, 10 DEGN034
 10 DB 40 I=1,N DEGN035
 12 DB 40 J=1,N DEGN036
 20 IF(I-J) 35, 25, 35 DEGN037
 25 B(I,J)=1.0 DEGN038
 30 GO TO 40 DEGN039
 35 B(I,J)=0.0 DEGN040
 40 CONTINUE DEGN041
PERFORM ROTATIONS TO REDUCE MATRIX TO JACOBI FORM. DEGN042
 45 JEXIT=1 DEGN043
 50 NN=N**2 DEGN044
 52 IF (NN) 890, 170, 55 DEGN045
 55 DB 160 I=1,NN DEGN046
 60 II=I+2 DEGN047
 65 DB 160 J=II,N DEGN048
 70 T1=A(I,I+1) DEGN049
 75 T2=A(I,J) DEGN050
 80 GO TO 900 DEGN051
 90 DB 105 K=I,N DEGN052
 95 T2=COS*A(K,I+1)+SIN*A(K,J) DEGN053

LMSC C56G - EFN SBJRCE STATEMENT - IFN(S) - 12/15/66
 100 A(I,K,J)=COS*A(I,K,J)-SIN*A(K,I+1) DEGN055
 105 A(K,I+1)=T2 DEGN056
 110 DO 125 K=I,N DEGN057
 115 T2=COS*A(I+1,K)+SIN*A(J,K) DEGN058
 120 A(I,J,K)=COS*A(J,K)-SIN*A(I+1,K) DEGN059
 125 A(I+1,K)=T2 DEGN060
 128 IF (M) 130, 160, 130 DEGN061
 130 D0 150 K=1,N DEGN062
 135 T2=COS*B(I,K,I+1)+SIN*B(K,J) DEGN063
 140 B(I,J,K)=COS*B(K,J)-SIN*B(K,I+1) DEGN064
 150 B(K,I+1)=T2 DEGN065
 160 CONTINUE DEGN066

 MOVE JACOBI FORM ELEMENTS AND INITIALIZE EIGENVALUE BOUNDARY DEGN067
 170 DB 200 I=1,N DEGN068
 180 DIAG(I)=A(I,I) DEGN069
 190 VALU(I)=ANORM DEGN070
 200 VALL(I)=ANORM DEGN071
 210 D0 230 I=2,N DEGN072
 220 SUPERD(I-1)=A(I-1,I) DEGN073
 230 Q(I-1)=(SUPERD(I-1))**2 DEGN074

 DETERMINE SIGNS OF PRINCIPAL MINORS DEGN075
 235 TAU=0.0 DEGN076
 240 I=1 DEGN077
 260 MATCH=0 DEGN078
 270 T2=0.0 DEGN079
 275 TI=1.0 DEGN080
 277 D0 450 J=1,N DEGN081
 280 P=DIAG(IJ)-TAU DEGN082
 290 IF(T2) 300, 330, 300 DEGN083
 300 IF(TI) 310, 370, 310 DEGN084
 310 T=P+TI-Q(J-1)*T2 DEGN085
 320 G# T# 410 DEGN086
 330 IF(TI) 335, 350, 350 DEGN087
 335 TI=-1.0 DEGN088
 340 T=-P DEGN089
 345 G# T# 410 DEGN090
 350 TI=1.0 DEGN091
 355 T=P DEGN092
 360 G# T# 410 DEGN093
 370 IF(Q(J-1)) 380, 350, 380 DEGN094
 380 IF(T2) 400, 390, 390 DEGN095
 390 T=-1.0 DEGN096
 395 G# T# 410 DEGN097
 400 T=1.0 DEGN098

 CBUNT AGREEMENTS IN SIGN DEGN100
 410 IF(TI) 425, 420, 420 DEGN105
 420 IF(T) 440, 430, 430 DEGN106
 425 IF(T) 430, 440, 440 DEGN107
 430 MATCH=MATCH+1 DEGN108
 440 T2=TI/ABSF(TI) DEGN109

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      LMSC          - EFN  SJRCE STATEMENT - IFN(S) -      12/15/66
      C56G

      450 T1=T/ABSF(T1)
      C      ESTABLISH TIGHTER BOUNDS ON EIGENVALUES
      C
      460 DB 530 K=1,N
      465 IF (K=MATCH) 470, 470, 520
      470 IF(TAU-VALL(K)) 530, 530, 480
      480 VALL(K)=TAU
      490 G0 TB 530
      520 IF(TAU-VALU(K)) 525, 530, 530
      525 VALU(K)=TAU
      530 CANTIQUE
      540 IF(VALU()==VALL()==5.0-16) 570, 570, 550
      550 IF(VALU()==560, 580, 560
      560 IF(ABSF(VALL())>VALU()-1.0)-5.0-16) 570, 570, 580
      570 I=I+1
      575 IF(I=N) 540, 540, 590
      580 TAU=(VALL()>VALU())/2.0
      585 G0 TB 260
      C      JACOBI EIGENVECTORS BY ROTATIONAL TRIANGULARIZATION
      C
      590 IF (M) 593, 890, 593
      593 IEXIT=2
      595 DB 610 J=1,N
      600 DB 610 J=1,N
      610 A(I,J)=0.0
      615 DB 850 I=1,N
      620 IF ((I-1) 625, 625, 621
      621 IF (VALU(I-1)-VALU(I))-5.0-15) 730, 730, 622
      622 IF (VALU(I-1)) 623, 625, 623
      623 IF (ABSF(VALU(I)/VALU(I-1)-1.0)-5.0-15) 730, 730, 625
      625 C05=1.0
      628 SIN=0.0
      630 DB 700 J=1,N
      635 IF(J-1) 680, 680, 640
      640 G0 TB 900
      650 S(J-1)=SIN
      660 C(J-1)=C05
      670 D(I,J)=I1*C05+T2*SIN
      680 I1=(DIAG(I))-VALU(I))*C05-BETA*SIN
      690 T2=SUPERD(IJ)
      700 BETA=SUPERD(J)*C05
      710 D(I,J)=T1
      720 DB 725 J=1,N
      725 IND(J)=0
      730 SMALLD=ANORM
      735 DB 790 J=1,N
      740 IF ((IND(J)-1) 750, 780, 780
      750 IF (ABSF(SMALLD)-ABSF(D(I,J))) 780, 780, 760
      760 SMALLD=D(J)
      770 NN=J
      780 CANTIQUE
      790 IND(NN)=1
      800 PRD05=1.0
      835 IF (NN-1) 810, 850, 810
      DEGN111
      DEGN112
      DEGN113
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      DEGN192

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      LMSC          - EFN  SJRCE STATEMENT - IFN(S) -      12/15/66
      C56G

      810 DB 840 K=2,N
      820 I=NN+1-K
      830 A(I,I,J)=C(I)+PR05
      840 PR05=-PR05+S(I,I)
      850 A(I,I,J)=PR05
      C      FORM MATRIX PRODUCT OF ROTATION MATRIX WITH JACOBI VECTOR MATRIX
      C
      855 DB 885 J=1,N
      860 DB 885 K=1,N
      865 U(K)=A(K,J)
      870 DB 885 I=1,N
      875 A(I,J)=0.0
      880 DB 885 K=1,N
      885 A(I,J)=U(I,K)*U(K)+A(I,J)
      890 RETURN
      C      CALCULATE SINE AND COSINE OF ANGLE OF ROTATION
      C
      900 IF (T2) 910, 940, 910
      910 T=SQRT(T1**2+T2**2)
      920 C05=T1/T
      925 SIN=T2/T
      930 G0 TB (90,650), IEXIT
      940 G0 TB (160,910), IEXIT
      END
      DEGN167
      DEGN168
      DEGN169
      DEGN170
      DEGN171
      DEGN172
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      DEGN192

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LMSC C56H - EFN SOURCE STATEMENT - IFN(S) - 12/15/66
 SUBROUTINE OUT2(A,IMAX)
 DIMENSION A(60,60)
 DOUBLE PRECISION A
 L= IMAX/10
 IF((10*L).LT.IMAX) L=L+1
 J1=9
 DO 200 K=1,L
 J1=J1+10
 J2=J1+9
 IF(K.EQ.L) J2=IMAX
 WRITE(6,100) (J,J=J1,J2)
 100 FORMAT(1H0// 9X,10(2X,THCBLUMN(I2,1H)))
 WRITE(6,150)
 150 FORMAT(1H)
 DO 200 I=1,IMAX
 200 WRITE(6,300) I,(A(I,J),J=J1,J2)
 300 FORMAT(5H RWM(I2,1H),IX,1P1E12.4)
 RETURN
 END

DMAT0010	
DMAT0020	
DMAT0030	
DMAT0040	
DMAT0050	
DMAT0060	
DMAT0070	
DMAT0080	
DMAT0090	
DMAT0100	12
DMAT0110	
DMAT0120	
DMAT0130	15
DMAT0140	
DMAT0150	
DMAT0160	19
DMAT0170	
DMAT0180	
DMAT0190	

LMSC C56J - EFN SOURCE STATEMENT - IFN(S) - 12/15/66
 SUBROUTINE BRTM0 (R,N)
 DOUBLE PRECISION R
 COMMON/TRANS/ DUM1 7320!, S(60,60)
 DIMENSION R(60,60)
 DO 10 I=1,N
 DO 10 J=1,N
 S(I,J)=0.
 DO 10 K=1,N
 10 S(I,J)+S(I,J)*R(K,I)*R(K,J)
 WRITE(6,20)
 20 FORMAT(13H1 BRTM0 CHECK)
 CALL OUTMAT(S,4)
 RETURN
 END

18	
19	

LMSL C56K - EFN SBJRCE STATEMENT - IFN(S) - 12/15/66

SUBROUTINE GRAPH4(IND,NDATA)

COMMON/MISC/ N, BL(12), SL(12), NP(12), NF(12), N2(12), PNU(12), GRPH0020

 BM(12), BD(12), OPTION(12), TITLE(12), REF(12),

 NMP(12), NIP(12), NEI(12), NGA(12), ISL(12), IBB(12),

 NT2P, NT4P, NT8I, NTB, NTT, NTP, TV4, XMC

COMMON/SPRING/ SSL1(12), SSL2(12), SSR1(12), SSR2(12),

 RS1(12), RS2(12), RSL2(12), RSR2(12),

 SK(12,4,4), SKB(12,2,2)

COMMON/SHAPE1/ MPI(1930), IP(1900), EI(1900), GAI(1900),

 MP(1900), IP(1000), EI(1000), GAI(1000),

 F(2600)

DIMENSION A1(1000), A2(1000), AP(1000), AY(1000), B(1000)

DIMENSION E(160,60), W(60), GMV(60)

DIMENSION X(300), Y(300)

DIMENSION ZP(1000), YSP(1000), YYP(1000)

EQUIVALENCE (E,NPI), (A1,MP), (A2,MP(501)), (AP,EI), (AY,GA),

 (ZP,IP), (YSP,GA)

DIMENSION TPWRD(2)

DATA TPWRD/6MIS NBT,6H IS /

REAL MP,IP,MP1,IP1

INTEGER OPTIBN

CALL SCL0CK(1,TIME,ESEC,02)

WRITE(6,1) TIME

FORMAT(14H1BEG1V GRAPH ,A6)

NAM=9

CALL CAMRAV(NAM)

KEMIND 1

READ(1) MPI,IP1,EI,GAI,MP,IP,EI,GA

READ(1) F

INITIALIZE VALUES

XL=0.0

YL=0.0

KNP=0

KIP1=0

KIP2=0

NBINT=0

KEI1=0

KEI2=0

KGAI=0

KGAAZ=0

DE 5 I=1,N

NBINT=NBINT+NP(I)-1

KIP2=KIP2+NIP(I)

KGAAZ=KGAAZ+NGA(I)

KEI2=KEI2+NEI(I)

K1=0

K2=0

DO 150 I=1,N

NPI=NP(I)

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GRPH9220

GRPH9230

GRPH9240

GRPH9250

GRPH9260

GRPH9270

GRPH9280

GRPH9290

GRPH9300

GRPH9310

GRPH9320

GRPH9330

GRPH9340

GRPH9350

GRPH9360

GRPH9370

GRPH9380

GRPH9390

GRPH9400

GRPH9410

GRPH9420

GRPH9430

GRPH9440

GRPH9450

GRPH9460

GRPH9470

GRPH9480

GRPH9490

GRPH9500

GRPH9510

GRPH9520

GRPH9530

GRPH9540

GRPH9550

GRPH9560

GRPH9570

GRPH9580

GRPH9590

GRPH9600

GRPH9610

GRPH9620

GRPH9630

GRPH9640

GRPH9650

GRPH9660

GRPH9670

GRPH9680

GRPH9690

GRPH9700

GRPH9710

GRPH9720

GRPH9730

GRPH9740

GRPH9750

GRPH9760

GRPH9770

GRPH9780

GRPH9790

GRPH9800

GRPH9810

GRPH9820

GRPH9830

GRPH9840

GRPH9850

GRPH9860

GRPH9870

GRPH9880

GRPH9890

GRPH9900

GRPH9910

GRPH9920

GRPH9930

GRPH9940

GRPH9950

GRPH9960

GRPH9970

GRPH9980

GRPH9990

GRPH10000

LMSC C56K - EFN SOURCE STATEMENT - IFN(S) - 12/15/66

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    NCHAR=1          GPH0910  133
    NX0=756          GPH0932
    NY0=1015         GPH0940
    IF(I-LT.10) GB T0 70  GPH0950
    NCHAR=2          GPH0960
    NX0=748          GPH0973
    70 FLI=FL0AT(I)  GPH0980
    CALL LABLV(FLI,NX0,NY0,NCHAR,I,NCHAR)  GPH0990  143
    CALL LABLVBLC(I,764,997,1,1,4)          GPH1000  145
    FLNP1=FL0AT(NPI)
    NCNP3          GPH1013
    IF(IFLP1/10.C.LT.10.0) NCNP=2        GPH1020
    CALL LABLV(FLNP1,740,979,NCNP,1,NCNP)  GPH1030
    NCNP4          GPH1040
    CALL PLBT SHAPE FUNCTIONS            GPH1053
    GPH1063
    GPH1073  151
    IF(IFN1.EU.0) GB T0 120
    DO 110 J=1,NFI
    YT=0.0          GPH1080
    DO 80 K=1,NPI
    KK=KK+2          GPH1090
    Y(K)=F(KK)
    80 YT=AMAX1(YT,ABS(Y(K)))
    DO 90 K=1,NPI
    90 Y(K)=Y(K)/YT          GPH1100
    GPH1110
    GPH1120
    GPH1130
    91 CALL APL0TV(NPI,X,Y,1,1,1,42,IER)  174
    92 CALL LINEIL(NPI,X,Y,1)
    GPH T0 105          GPH1140
    93 NSPACE=3          GPH1150
    GPH TD 96          GPH1160
    94 NSPACE=9
    96 DO 100 K=1,NPI,NSPACE
    NX0=NXV(X(K))
    NY0=NYV(Y(K))
    NLIM=NSPACE-1
    IF(IK+NLIM).GT.NPI) NLIM=NPI-K
    IF(NLIM.EQ.0) GB T0 100
    DO 98 L=1,NLIM
    LL=L+K
    NX1=NXV(X(LL))
    NY1=NYV(Y(LL))
    CALL LINEV(NX0,NY0,NX1,NY1)
    NX0=NX1
    98 NY0=NY1
    100 CONTINUE
    105 KJ=J+NPI/2
    NX0=NXV(X(KJ))
    NY0=NYV(Y(KJ))
    CALL LABLV(FL0AT(J),NX0,NY0,1,2,1)
    110 KZ=K2+NPI
    GPH T0 123          GPH1290
    120 CALL PRINTV(-5,SHRIGID,550,246)      GPH1300  215
    GPH1310  218
    GPH1320  221
    GPH1330
    GPH1350
  
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LMSC C56K - EFN SOURCE STATEMENT - IFN(S) - 12/15/66

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    X(1)=KINC/2.          GPH1360  227
    DO 125 K=2,NPI1
    125 X(K)=X(K-1)+XINC          GPH1370
    GPH1380
    GPH1390
    GPH1400
    GPH1410
    GPH1420
    130 CALL LABMAX(MPI(KMP+1),MPI((KMP+1),NMP()),NMP(I),1,YT,N10,NCHAR,NC,GPH1430
    * IS(GV)          GPH1443  238
    FN10=FL0AT(N10)
    LSP=400          GPH1450
    LST=130
    IF(NC.EQ.2) LST=122
    IF(IISIGN.EQ.0) GB T0 135
    FN10=-FN10
    LSP=LSP*8
    CALL LABLV(FN10,LSP,987,NCHAR,1,NCHAR)  GPH1470
    CALL YSCALV(YB,YT,444,52)          GPH1480
    CALL DXYVV(2,YB,YT,DY,M,J,NY,15,.IER)
    IF(IERR.NE.0) CALL PRINTV(-19,19HERRR == (MP) SCALE,200,470)
    DOY=DY*FL0AT(M)
    CALL LINRV11, 0, 444, 971, XL , XR , XR, 0, 0, 1, 8)  GPH1490
    CALL LINEV11004,444,1004,971)          GPH1500
    CALL LINRV12, 0 , 140,1004, YB , YT , YT, 0, 0, 1,10)  GPH1510
    CALL LINRV12,LST , 140, 150, YB , YT , DY, 0, 0, J,NC,10)
    CALL LINRV12, 0 , 140, 156, YB + YT , DDY, 1, 0, 1,10)
    YT=YT+1.**FN10
    CALL YSCALV(YB,YT,444,52)
    CALL APL0TV(NPI1,X,MP(KI+1),1,1,1,42,IER)
    IF(IFDATA.EQ.1) CALL LINEIL(NPI1,X,MP(KI+1),1)
    WRITE(6,137) IER
    137 FORMAT(5H0IEH=,I2)
    IF(IER.EQ.0) GB T0 136
    CALL LABLV(FL0AT(IER),830,40,3,1,3)
    CAL PRINTV(-19,19H MP-P0INTS BFFSCALE,862,40)  GPH1520
    136 NX0=NXV(X(YP1))-4          GPH1530  250
    NY0=NYV(MP(IY1))+6          GPH1540  252
    CALL PRINTV(-2,2*NMP,NX0,NY0)
    CALL PLBT2L(MPI(KMP+1),NMP())
    KMP=KMP+NMP()
    NK1=NB1NT*K1          GPH1550  254
    GPH1560
    GPH1570  256
    GPH1580  261
    GPH1590  263
    GPH1600  265
    GPH1610  267
    GPH1620  269
    GPH1630  270
    GPH1640  272
    GPH1650  274
    GPH1660  276
    GPH1670  278
    GPH1680  280
    GPH1690  282
    GPH1700  284
    GPH1710  286
    GPH1720
    GPH1740
    CALL LABMAX(GAI(KGA1+1),GAI(KGA2+1),NGA(I),NGA(IPV),1,YT,N10,NCHAR
    * ,NC,ISIGN)          GPH1750  303
    FN10=FL0AT(N10)
    LSP=352
    LST=82
    IF(NC.EQ.2) LST=74
    IF(IISIGN.EQ.0) GB T0 140
    FN10=-FN10
    LSP=LSP*8
    140 CALL LABLV(FN10,LSP,1005,NCHAR,1,NCHAR)
    CALL YSCALV(YB,YT,444,52)          GPH1770
    GPH1780
    GPH1790
    GPH1800
    GPH1810
    GPH1820
    GPH1830
    GPH1840  316
    GPH1850  318
  
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LMSC C56K - EFN SBURCE STATEMENT - IFN(S) - 12/15/66
 CALL DXDYYV(2,YB,YT,DY,M,J,NY,15,,IERR) GPH1860 320
 IF(IERR.NE.0) CALL PRINTV(-19,19HERRRR == (GA) SCALE,200,486) GPH1870 323
 DDY=DY*FLBAT(M) GPH1880
 CALL LINEV(92,446,92,971) GPH1890 325
 CALL LINEV(92,446,92,971) GPH1900 327
 CALL LINRV(2,LST, 92,102, YB , YT , DY, D, J,NC,10) GPH1910 329
 CALL LINRV(2, D , 92,108, YB , YT , DDY, 1, D, 1,10) GPH1920 331
 YT=Y+YT*10.**#FRI0 GPH1930 333
 CALL YSCALV(YB,YT,444,52) GPH1940 334
 CALL APL0TV(NPI1,X,GA(K1+1),1,1,1,42,IER) GPH1950 336
 IF(IFDATA.EQ.0) CALL LINEIL(NPI1,X,GA(K1+1),1) GPH1960 340
 IF(IER.EQ.0) G0 TB 141
 CALL LABLV(FL8AT(IER),830,30,3,1,3) 346
 CALL PRINTV(-19,19HGA1-PBINTS BFFSCALE,862,30) 348
 141 IYD=K1+2*NPI6 GPH1963
 NX0=NXV(X12+NPI6))-8 GPH1970 351
 NY0=NYV(GAI(IYD))+6 354
 CALL PRINTV(-3,3HGA1,NX0,NY0) 357
 CALL PL0T2L(GAI(KGA1+1),NGA1)) 359
 IF(IFPT18N(4),EQ.0) G0 TB 143 GPH2380 366
 CALL APL0TV(NPI1,X,GA(NK1+1),1,1,1,42,IER1) 368
 IF(IER.EQ.0) G0 TB 142 372
 CALL LABLV(FL8AT(IER),830,20,3,1,3) 374
 CALL PRINTV(-19,19HGA2-PBINTS BFFSCALE,862,20) 374
 142 IYD=NK1+3*NPI6 GPH2010
 NX0=NXV(X13+NPI6))-8 GPH2020 377
 NY0=NYV(GAI(IYD))+6 380
 CALL PRINTV(-3,3HGA2,NX0,NY0) 383
 IPN=1+N GPH2060 386
 CALL PL0T2L(GAI(KGA2+1),NGA(IPN))
 143 KGA1=KGA1+NGA1) 386
 KGA2=KGA2+NGA(IPN)
 C PL0T STIFFNESS (EI) DISTRIBUTION GPH2100
 C CALL LAHMAX(EII(KE1+1),EII(KE1+1),NEI(I),NEI(IPV),1,YT,N10,NCHAR GPH2110
 C ,N,ISIGN) GPH2120
 FN10=FL8AT(N10) GPH2130 395
 LSP=344 GPH2140
 LST=34 GPH2150
 IF(NC.EQ.2) LST=26 GPH2160
 IF(ISIGN.EQ.0) G0 TB 145 GPH2170
 FN10=-FN10 GPH2180
 LSP=LSP+8 GPH2190
 145 CALL LABLV(FN10,LSP,1023,NC4AR,1,NCHAR) GPH2200
 CALL YSCALV(Yd,YT,444,52) GPH2210
 CALL DXDYYV(2,YB,YT,DY,M,J,NY,15,,IERR) GPH2220 408
 IF(IERR.NE.0) CALL PRINTV(-19,19HERRRR == (EI) SCALE,200,502) GPH2230 410
 DDY=DY*FLBAT(M) GPH2240 412
 CALL LINEV(44,444,44,971) GPH2250 415
 CALL LINEV(44,444,44,971) GPH2260
 CALL LINRV(2,LST, 44, 54 , YB , YT , DY, D, J,NC,10) GPH2270 417
 CALL LINRV(2, D , 44, 60 , YB , YT , DDY, 1, D, 1,10) GPH2280 419
 YT=Y+YT*10.**#FRI0 GPH2290 421
 CALL YSCALV(YB,YT,444,52) GPH2300 423
 CALL APL0TV(NPI1,X,EI(K1+1),1,1,1,42,IER) GPH2310 425
 CALL PRINTV(-19,19HEI1-PBINTS BFFSCALE,862,10) GPH2320 426
 146 IYD=NK1+4*NPI6 GPH2330 428

LMSC C56K - EFN SBURCE STATEMENT - IFN(S) - 12/15/66
 IF(IFDATA.EQ.0) CALL LINEIL(NPI1,X,EI(K1+1),1) 432
 IF(IER.EQ.0) G0 TB 146
 CALL LABLV(FLBAT(IER),830,10,3,1,3) 438
 CALL PRINTV(-19,19HEI1-PBINTS BFFSCALE,862,10) 440
 146 IYD=NK1+4*NPI6 GPH2340
 NX0=NXV(X14+NPI6))-8 GPH2350 443
 NY0=NYV(EII(IYD))+6 GPH2360 446
 CALL PRINTV(-3,3HEI1,NX0,NY0) GPH2370 449
 CALL PL0T2L(EII(KE1+1),NEI(I)) GPH2430 452
 IF(IFPT18N(4),EQ.0) G0 TB 148 GPH2380 458
 CALL APL0TV(NPI1,X,EI(NK1+1),1,1,1,42,IER) 458
 IF(IER.EQ.0) G0 TB 147
 CALL LABLV(FLBAT(IER),830, 3,1,3) 464
 CALL PRINTV(-19,19HEI2-PBINTS BFFSCALE,862, 0) 466
 147 IYD=NK1+5*NPI6 GPH2390
 NX0=NXV(X15+NPI6))-8 GPH2400 459
 NY0=NYV(EII(IYD))+6 GPH2410 472
 CALL PRINTV(-3,3HEI2,NX0,NY0) GPH2420 475
 CALL PL0T2L(EII(KE1+1),NEI(IPV)) GPH2440 477
 148 KEI1=KEI1+NEI(I) 477
 KEI2=KEI2+NEI(IPV)
 150 K1=K1+NPI1 GPH2460
 C IF(IND.EQ.1) G0 TB 810 GPH2470
 C PL0T MODAL DISPLACEMENT FUNCTIONS GPH2480
 READ(3) EW,GMV 490
 WRITE(3) EI 494
 REWIND 3 496
 C
 DO 190 J=1,NTT,2
 IF(ABS(EINT2P(J)).GT.1.E-35) G0 TB 190
 DO 182 I=1,NTT
 TEMP=E(I,J)
 E(I,J)=E(I,J+1)
 E(I,J+1)=TEMP
 180 CONTINUE
 C
 TL=0.D
 DO 200 I=1,N
 200 TL=TL+BL(I)+SL(I)
 YB=REF()
 YT=YB+TL
 DC=25.
 C
 CALL DXDYYV(2,YB,YT,DY,MG,JG,NYC,DC,IER) 523
 CALL YSCALV(YB,YT,60,50) 525
 C
 NM0DES=OPT18N(6)
 MKBUNT=0
 INBUUT=J
 NM0UT=IBS(OPTIONN(7))
 IF(NM0UT.EQ.0) REWIND 1 531
 MTAPE=0
 IF(OPT18N(7).GT.0) MTAPE=1

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      LMSC          - EFN  SOURCE STATEMENT - IFN(S) -           12/15/66
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      BLNGTH=TL
      IF(NMBUT.GT.0) WRITE(6,203) TPWBRD(MTAPE+1),BLNGTH,NMBJT,REF(1),
      *                                         XMC,TVM
      203 FFORMAT(21H1SPECIAL OUTPUT TAPE ,A6,10H GENERATED//9M BLNGTH =E15.8
      *9M NMOUT =15/9M REF =E15.8/9M XMC =E15.8/9M TVM =E15.8)
      IF(MTAPE.EQ.0) GO TO 205
      KENIND 10
      WRITE(1C)BLNGTH,NMBUT,REF(1),XMC,TVM
      205 DB 800 M=1,NMDES
      IF((NMOUT.EQ.1) READ(1) F
      INDBUT=0
      J1=0
      K1=0
      I1=1
      I2=NT2P+1
      I3=NT6P+1
      I4=NT8L+1
      AA=0.0
      C
      DB 300 I=1,N
      NPI=NPI()
      NFI=NFI()
      XINC=BL(I)/FLBAT(NPI-1)
      CPNU=CBSP(VU(I))
      SPNU=SIN(PNU(I))
      C
      DB 210 K=1,NPI
      KK=K1*K
      X=XINC*FLBAT(K-1)
      B(KK)=REF(I)*X
      A1(K)=E(I1,M)*(E(I1+1,M)-E(I1,M))+X/BL(I)
      210 A2(K)=E(I2,M)*(E(I2+1,M)-E(I2,M))+X/BL(I)
      C
      IF(NFI.EQ.0) GO TO 240
      DB 230 J=1,NFI
      DB 220 K=1,NPI
      JJ=J1*K
      A1(K)=A1(K)+F(JJ)*E(I3,M)
      A2(K)=A2(K)+F(JJ)*E(I4,M)
      220 CONTINUE
      C
      J1=J1+NPI
      I3=I3+1
      230 I4=I4+1
      C
      DB 250 K=1,NPI
      KK=K1*K
      AP(KK)=A1(K)*CPNU - A2(K)*SPNU
      AY(KK)=A1(K)*SPNU + A2(K)*CPNU
      250 AA=AMAX1(ABS(A1(K)),ABS(A2(K)),AA)
      I1=I1+1
      I2=I2+1
      IF(ISL(I).EQ.0) GO TO 300
      K1=K1+1
      I1=I1+1
      C
      300 DB 250 K1=K1+NPI-1
      C
      K1=K1+1
      DB 310 K=1,K1
      AP(K)=AP(K)/AA
      310 AY(K)=AY(K)/AA
      C
      CALL FRAMEV
      CALL XSCALV(-1.0,1.0,30,523)
      CALL LINRVL1(50,60,973,-1.0,1.0,0.1,5,10,1,8)
      CALL LINRVL2(510,30,500,YB,YT,DY,MG,NYC,10)
      CALL APLBTW(K1,AY,B,1,1,1,42,IER)
      I1=1
      DB 330 I=1,N
      I=I+NPI()-1
      CALL P8INTV(AY(I1),B(I1),-1)
      IF(ISL(I).EQ.0) GO TO 330
      I=I+1
      CALL P8INTV(AY(I1),B(I1),-1)
      330 CONTINUE
      C
      CALL XSCALV(-1.0,1.0,545,8)
      CALL LINRVL1(1,50,60,973,-1.0,1.0,0.1,5,10,1,8)
      CALL LINRVL2(0,545,1015,YB,YT,DY,MG,0,NYC,10)
      CALL APLBTW(K1,AP,B,1,1,1,42,IER)
      I1=1
      DB 350 I=1,N
      I=I+NPI()-1
      CALL P8INTV(AP(I1),B(I1),-1)
      IF(ISL(I).EQ.0) GO TO 350
      I=I+1
      CALL P8INTV(AP(I1),B(I1),-1)
      350 CONTINUE
      C
      CALL PRINTV(-29,Z9HNORMALIZED RELATIVE AMPLITUDE,406,30)
      CALL APRNTVU,-14,-18,18HCORDINATE STAT104,10,643)
      CALL PRINTV(-3,3HYAN,253,983)
      CALL PRINTV(-5,5HPITCH,760,983)
      CALL PRINTV(-8,8HMHDDEI 1,6,15)
      HMDE=0
      CALL LABLV(BMDE,46,15,2,1)
      CALL PRINTV(-12,12MFREQUENCY = ,6,0)
      FREQ=W(M)
      CALL LABLV(FREQ,100,0,-4,1,1)
      C
      IF(M.GT.2=NMBUT) GO TO 800
      IF((M/2).GT.2=NEM) GO TO 800
      IF(NSL1.NE.0) GO TO 360
      IF(M.LE.4) GO TO 800
      360 NMOUT=NMOUT+1
      INDBUT=1
      C
      C@STRUCTURE THE PSIPRM ARRAY

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      LMSC          - EFN  SOURCE STATEMENT - IFN(S) -           12/15/66
      C56K

      IF(NMBUT.GT.0) GO TO 800
      IF((M/2).GT.2=NEM) GO TO 800
      IF(NSL1.NE.0) GO TO 360
      IF(M.LE.4) GO TO 800
      360 NMOUT=NMOUT+1
      INDBUT=1
      C
      C@STRUCTURE THE PSIPRM ARRAY

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LMSL
      C56K      - EFN  SOURCE STATEMENT - IFV(S) -          12/15/66
      READ(1) F
      J1=0
      K1=0
      I3=NT4P+1
C
      DB 700 I=1,N
      NPI=NPI()
      NFI=NFI()
      DB 610 K=1,NPI
      610 AI(K)=0,
      IF(NFI.EQ.0) GO TO 640
C
      DB 630 J=1,NFI
      DB 620 K=1,NPI
      JJ=J1+K
      620 AI(K)=AI(K) + F(JJ)*E(I3,M)
      JI=J1+NPI
      630 I3=I3+1
C
      DB 650 K=1,NPI
      KK=K1+K
      650 YYP(KK)=AI(K)/AA
C
      IF(ISL().EQ.0) K1=K1+1
      700 K1=K1+NPI-1
C  CONSTRUCT THE CROSS SECTION ROTATION (PSI) ARRAY
C
      READ(1) F
      J1=0
      K1=0
      I1=1
      I3=NT4P+1
C
      DB 500 I=1,N
      NPI=NPI()
      NFI=NFI()
      DB 410 K=1,NPI
      410 AI(K)=(E(I1+1,M)-E(I1,M))/B_(1)
      IF(NFI.EQ.0) GO TO 440
      DB 430 J=1,NFI
      DB 420 K=1,NPI
      JJ=J1+K
      420 AI(K)=AI(K) + F(JJ)*E(I3,M)
      JI=J1+NPI
      430 I3=I3+1
C
      440 DB 450 K=1,NPI
      KK=K1+K
      450 ZP(KK)=AI(K)/AA
C
      I1=I1+1
      I2=I2+1

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LMSL
      C56K      - EFN  SOURCE STATEMENT - IFV(S) -          12/15/66
      IF(ISL().EQ.1) GO TO 500
      I1=I1+1
      I2=I2+1
      K1=K1+1
      500 K1=K1+NPI-1
C  CONSTRUCT THE SHEAR ANGLE ARRAY
C
      READ(1) F
      REWIND 1
      READ(1) DUMREC
      J1=0
      K1=0
      I3=NT4P+1
C
      DB 600 I=1,N
      NPI=NPI()
      NFI=NFI()
      DB 510 K=1,NPI
      510 AI(K)=0,
      IF(NFI.EQ.0) GO TO 540
C
      DB 530 J=1,NFI
      DB 520 K=1,NPI
      JJ=J1+K
      520 AI(K)=AI(K) + F(JJ)*E(I3,M)
      JI=J1+NPI
      530 I3=I3+1
C
      540 DB 550 K=1,NPI
      KK=K1+K
      550 YSP(KK)=AI(K)/AA
C
      IF(ISL().EQ.0) K1=K1+1
      600 K1=K1+NPI-1
      K1=K1+1
C
      WRITE(6,710) M,(I,B(I),AP(I),ZP(I),YSP(I),YYP(I),I=1,K1)
      710 F$FORMAT(6HMBDE I2,7H *****/1M0,3X,10HCR8SS SECT,3X,5HSHEAK,8X,
      *3HPSI/6M STA.,3X,8HLBCATIBV,7X,10HDEFLECTION,3X,8HR0TATION,5X,5HA
      *NGLE,8X,8HPRIME/(I5,1PE14.4,2X,4E13.4))
C
      IF(MTAPE.EQ.0) GO TO 800
      MREQ=6.2831853
      GMASS=GMV(M)
      WRITE(10) MKBUNT,MREQ,GMASS,K1
      WRITE(10) (AP(I),I=1,K1)
      WRITE(10) (YSP(I),I=1,K1)
      WRITE(10) (YYP(I),I=1,K1)
      WRITE(10) (ZP(I),I=1,K1)
      800 CONTINUE
      810 CALL CLEAN
      IF(MTAPE.EQ.0) GO TO 820
      END FILE 10
      REWIND 10
      820 RETURN
      END

```

LMSC C56L - EFN SOURCE STATEMENT - IFN(S) - 12/15/66
 SUBROUTINE LABMAX(A,B,NXA,NXB,K,AMAX,N,NCHAR,NC,ISIGN)
 DIMENSION A(NXA),B(NXB)
 ISIGN=0
 NCHAR=1
 NC=1
 AMAX=A(1)
 IF(VXA.LT.4) GO TO 15
 DO 10 I=4,VXA-2
 10 AMAX=AMAX1(AMAX,A(I))
 15 IF(K.EQ.1) GO TO 30
 BMAX=B(1)
 DO 20 I=1,NXB-2
 20 BMAX=AMAX1(BMAX,B(I))
 AMAX=AMAX1(AMAX,BMAX)
 30 IF(AMAX.LT.1.E-35) GO TO 120
 IF(AMAX.LE.2.) GO TO 60
 N=0
 A1=1.
 40 IF(AMAX.LE.A1) GO TO 50
 N=N+1
 A1=A1/10.
 GO TO 40
 50 A1=A1/10.
 GO TO 80
 60 ISIGN=1
 N=1
 A1=-1
 70 IF(AMAX.GT.A1) GO TO 80
 N=N+1
 A1=A1/10.
 GO TO 70
 80 AMAX=AMAX/A1
 IF(AMAX.GE.10.) GO TO 90
 IF(AMAX.EQ.2.0) GO TO 100
 AMAX=FL8AT(IFIX(AMAX)+1)
 IF(AMAX.EQ.10.) NC=2
 IF(AMAX.EQ.2.0) GO TO 100
 GO TO 130
 90 NC=2
 IF(AMAX.GT.10.) AMAX=20.
 GO TO 130
 100 NC=2
 AMAX=20.
 IF(ISIGN.EQ.0) GO TO 110
 N=N+1
 GO TO 130
 110 N=N-1
 GO TO 130
 120 AMAX=10.0
 N=0
 NC=2
 GO TO 140
 130 IF(N.GE.10) NCHAR=2
 140 RETURN
 END

LMSC C56B - EFN SOURCE STATEMENT - IFN(S) - 12/15/66
 SUBROUTINE LINE1(NP,X,Y,J)
 DIMENSION X(NP),Y(NP)
 NX0=NXV(X(1))
 NY0=NYV(Y(1))
 DO 10 I=2,NP,J
 NX1=NXV(X(I))
 NY1=NYV(Y(I))
 CALL LINEV(NX0,NY0,NX1,NY1)
 NX0=NX1
 10 NY0=NY1
 RETURN
 END

LMSL
CS6N - EFN SOURCE STATEMENT - IFN(S) -

12/15/66

```
SUBROUTINE PL0T1L(NP,X,Y,J,ISYM)
DIMENSION X(NP),Y(NP)
NX0=XV(X(1))
NY0=YV(Y(1))
CALL PL0TV(NX0,NY0,ISYM)
DO 10 I=2,NP,J
NX1=XV(X(I))
NY1=YV(Y(I))
CALL LINEV(NX0,NY0,NX1,NY1)
CALL PL0TV(NX1,NY1,ISYM)
NX0=NX1
10 NY0=NY1
RETURN
END
```

GRPH3210
GRPH3220
GRPH3230 2
GRPH3240 4
GRPH3250 6
GRPH3260
GRPH3270 12
GRPH3280 15
GRPH3290 17
GRPH3300 19
GRPH3310
GRPH3320
GRPH3330
GRPH3340

LMSL
CS6N - EFN SOURCE STATEMENT - IFN(S) -

12/15/66

```
SUBROUTINE PL0T2L(A,N)
DIMENSION A(N)
NX0=NXV(A(1))
NY0=NYV(A(2))
NY1=NYV(A(1))
IF(N<LT,3) GO TO 20
DO 10 I=3,N-2
NX1=NXV(A(I))
NY1=NYV(A(I+1))
CALL LINEV(NX0,NY0,NX1,NY1)
NX0=NX1
10 NY0=NY1
20 RETURN
END
```

GRPH3080
GRPH3090
GRPH3100 2
GRPH3110 4
GRPH3120
GRPH3130 13
GRPH3140 15
GRPH3150 18
GRPH3160
GRPH3170
GRPH3190

INPUT DATA F2LL2W * * * SA-501 STADOLA COMPARISON WITH ROTARY INERTIA MODIFIED SHAPES/ 11/3

N = 4

OPTIONS 1 -0 1 -J -C 14 -4 -D -O -P -C -O

BEAM BL SL RM BC PAU NI N2 NP NMP NIP NEI NGA

1	0.42750100E C2	-0.000000005-38	-0.00100000E-38	-0.00000000E-38	-C.0C0000CC0E-38	3	3	172	344	344	344	344
2	0.43000J0CE C2	-0.00000000E-38	-0.00100000E-38	-0.00000000E-38	-0.0C0000CC0E-38	3	3	173	346	346	346	346
3	0.12500J00F C2	0.250000005 CC	-0.00100000E-38	-0.00000000E-38	-C.0C0000CC0E-38	3	3	151	102	102	102	102
4	0.12000000E C2	-0.00000000E-38	-0.00100000E-38	-0.00000000E-38	-0.0C0000CC0E-38	3	3	145	98	98	98	98

BEAM (1)

NP(1) = 172

STATION	RP	IP	EI	GA
1	C.29229E50E 03	C.1C15E120E 04	0.5738000E 12	C.2224250E 1C
2	0.44970250E 03	0.16165150E 04	0.5738000E 12	0.2224250E 1C
3	0.54564250E 03	C.15598350E 04	0.5738000E 12	C.2224250E 1C
4	0.6040E00F 03	C.21546C53E 04	0.5738000E 12	C.2224250E 1C
5	0.62724450E 03	0.22492100E 04	0.5738000E 12	C.2224250E 1C
6	0.65931E50E 03	0.23651700E 04	0.5738000E 12	C.2224250E 1C
7	C.70534250E 03	0.27528500E 04	0.5738000E 12	C.2224250E 1C
8	C.75664100E 03	0.27257650F 04	0.5738000E 12	C.2224250E 1C
9	C.42478200E 03	0.25542400E 04	0.5738000E 12	C.2224250E 1C
10	0.68473E00E 03	0.3167E150E 04	0.5738000E 12	0.2224250E 1C
11	0.93229449E 03	0.33511200E 04	0.5738000E 12	C.2224250E 1C
12	G.10305E5E 04	0.3596C500E 04	0.5738000E 12	C.2224250E 1C
13	C.11873450E 04	0.35373450E 04	0.5738000E 12	C.2224250E 1C
14	U.13131250E 04	0.43323C00E 04	0.5738000E 12	C.2224250E 1C
15	U.13727300E 04	0.47633500F 04	0.5738000E 12	C.2224250E 1C
16	0.14551450E 04	0.57006E650F 04	G.5738000E 12	C.2224250E 1C
17	C.17326100E 04	0.73523450E 04	0.5738000E 12	C.2224250E 1C
18	U.20658000E 04	0.9634C349E 04	0.5738000E 12	C.2224250E 1C
19	U.24931200E 04	0.1251C1C50F 05	0.5738000E 12	U.2224250E 1C
20	C.32722250E 04	0.16371350E 05	0.5738000E 12	U.2224250E 1C
21	C.45037150E 04	0.21313260F 05	0.5738000E 12	U.2224250E 1C
22	C.12C52315E 05	0.924423250F 05	0.5738000E 12	U.2224250E 1C
23	U.25499700E 05	0.23004850E 06	0.5738000E 12	U.2224250E 1C
24	U.26665400E 05	0.25261800E 06	0.63863299E 12	C.28864037E 1C
25	C.167271150E 05	0.169C3100E 06	0.60638849E 12	C.35365575E 1C
26	U.12744E00E 05	0.150561030E 06	0.68223400E 12	C.35365575E 1C
27	U.13781400E 05	0.18429300E 06	0.6880795E 12	C.35365575E 1C
28	C.13H26250F 05	0.18059550F 06	0.6397865E 12	U.33141325E 1C
29	C.12964400E 05	0.14421150E 06	0.59303950E 12	C.3C917075E 1C
30	U.12014400E 05	0.12353490E 06	0.54597600E 12	U.30917075E 1C
31	U.11C03E00E 05	0.11742250E 06	0.50958250E 12	U.30917075E 1C
32	U.10222665E 05	0.11355400E 06	0.45452450E 12	C.3C917075E 1C
33	U.96662020E 04	0.11179550E 06	0.46283500E 12	U.28914250E 1C
34	U.93387550E 04	C.1C32C8B5E 04	0.44024450E 12	C.26913425E 1C
35	U.92884E50E 04	0.46881350E 05	0.41765400E 12	C.26913425E 1C
36	C.85900E00E 04	0.72945E00E 05	0.39506350E 12	C.26913425E 1C
37	U.71483100E 04	0.62551100E 05	0.37247250E 12	C.26913425E 1C
38	U.60167C00E 04	0.54C73450E 05	0.34988200E 12	C.25356450E 1C
39	U.52862300E 04	0.67194E00E 05	0.32729150E 12	C.23795475E 1C
40	C.44955150E 04	0.4684C800E 05	0.34C70100E 12	C.23795475E 1C
41	C.49250300E 04	0.54955E50F 05	0.28814250E 12	C.23132200E 1C
42	U.4771500E 04	0.55862E00E 05	0.29005500E 12	C.22464925E 1C
43	U.43261100E 04	0.47347E50F 05	0.2744C750E 12	C.22464925E 1C
44	C.39740C00E 04	0.4C72C750E 05	0.26876000E 12	C.22464925E 1C
45	U.3775A300E 04	0.37223700E 05	0.26311200E 12	C.22464925E 1C
46	U.39291650E 04	0.3P745950E 05	0.22482100E 12	C.22464925E 1C
47	U.453471750E 04	0.46163E50E 05	0.18935400E 12	C.22464925E 1C
48	U.45717500F 04	0.46631450E 05	U.18935400E 12	C.22464925E 1C
49	U.35828300E 04	0.3438C550E 05	0.18935400E 12	C.22464925E 1C
50	U.27195550E 04	0.24013350E 05	0.18935400E 12	U.2131E850E 1C
51	U.246472750E 04	0.2169C150E 05	0.18935400E 12	U.2C111945E 1C
52	U.24298E00E 04	0.220C7450E 05	0.18935400E 12	C.1599C254E 1C

53	0.24391650E 04	0.22592500E 05	0.18935400E 12	0.1986562E 10
54	0.24633850E 04	0.23128850E 05	0.18935400E 12	0.19746872E 10
55	0.24756800E 04	0.23340550E 05	0.18648500E 12	0.19625180E 10
56	0.24835102E 04	0.23402550E 05	0.18361600E 12	0.19503489E 10
57	0.24937400E 04	0.23473500E 05	0.19316000E 12	0.19381758E 10
58	0.25088150E 04	0.23597150E 05	0.18361600E 12	0.1926108E 10
59	0.25316450E 04	0.23828500E 05	0.18361600E 12	0.19138416E 10
60	0.25310250E 04	0.23798500E 05	0.19361600E 12	0.19114725E 10
61	0.24648980E 04	0.23114700E 05	0.18074700E 12	0.18695034E 10
62	0.23845535E 04	0.22249750E 05	0.17787800E 12	0.18773344E 10
63	0.23257550E 04	0.218018C0E 05	0.17787800E 12	0.18651652E 10
64	0.23104500E 04	0.21897150E 05	0.17787800E 12	0.18525961E 10
65	0.23676450E 04	0.22764800E 05	0.17787800E 12	0.18408270E 10
66	0.24485200E 04	0.23863250E 05	0.17787800E 12	0.1828578E 10
67	0.24788350E 04	0.24364C00E 05	0.17509000E 12	0.18164888E 10
68	0.24834100E 04	0.24455935E 05	0.17214000E 12	0.1806233E 10
69	0.250535C50E 04	0.24445050E 05	0.17214000E 12	0.18016425E 10
70	0.25282650E 04	0.24235150E 05	0.17214000E 12	0.18016425E 10
71	0.25355250E 04	0.23621250E 05	0.17214000E 12	0.18016425E 10
72	0.26284550E 04	0.24086C50E 05	0.17214000E 12	0.18016425E 10
73	0.30745500E 04	0.29453600E 05	0.17214000E 12	0.18016425E 10
74	0.37243950E 04	0.37691150E 05	0.17214000E 12	0.18016425E 10
75	0.40143750E 04	0.41228600E 05	0.17142250E 12	0.18016425E 10
76	0.39203250E 04	0.40C021500E 05	0.17070500E 12	0.16014600E 10
77	0.35999750E 04	0.36676C50E 05	0.17070500E 12	0.14012775E 10
78	0.31462700E 04	0.31976300E 05	0.17070500E 12	0.14012775E 10
79	0.28356100E 04	0.27843150E 05	0.17070500E 12	0.14012775E 10
80	0.266595C50E 04	0.24484600E 05	0.17070500E 12	0.14012775E 10
81	0.26048500E 04	0.23114300E 05	0.17070500E 12	0.14012775E 10
82	0.26575250E 04	0.23497900E 05	0.17070500E 12	0.14012775E 10
83	0.28589300E 04	0.24271150E 05	0.17070500E 12	0.14012775E 10
84	0.32935150E 04	0.25287750E 05	0.17070500E 12	0.14012775E 10
85	0.34822200E 04	0.24909C00E 05	0.17070500E 12	0.14012775E 10
86	0.34663700E 04	0.23316800E 05	0.17070500E 12	0.14012775E 10
87	0.32275200E 04	0.22953750E 05	0.17070500E 12	0.14012775E 10
88	0.27897200E 04	0.23692550E 05	0.17070500E 12	0.14012775E 10
89	0.26725250E 04	0.22834C00E 05	0.17070500E 12	0.14012775E 10
90	0.28659550E 04	0.240427600E 05	0.17070500E 12	0.14012775E 10
91	0.28185400E 04	0.187571750E 05	0.17070500E 12	0.14C12775E 10
92	0.25002350E 04	0.18082700E 05	0.17070500E 12	0.14012775E 10
93	0.22560450E 04	0.19056500E 05	0.17070500E 12	0.14C12775E 10
94	0.21160150E 04	0.2142C250E 05	0.17070500E 12	0.14012775E 10
95	0.20446650E 04	0.2299C250E 05	0.17070500E 12	0.14012775E 10
96	0.20444400E 04	0.23738300E 05	0.17070500E 12	0.17126725E 10
97	0.20803400E 04	0.24584700E 05	0.17070500E 12	0.2024C675E 10
98	0.21515450E 04	0.255638C0E 05	0.17070500E 12	0.2024C675E 10
99	0.21033250E 04	0.25182550E 05	0.17070500E 12	0.2024C675E 10
100	0.18957C00E 04	0.23003200E 05	0.17070500E 12	0.2024C675E 10
101	0.21088850E 04	0.26966330E 05	0.17070500E 12	0.22C4C675E 10
102	0.28380300E 04	0.355C7200E 05	0.19867800E 12	0.22C4C675E 10
103	0.30195300E 04	0.381277500E 05	0.22665100E 11	0.2024C675E 10
104	0.24C18400E 04	0.3C802650E 05	0.22665100E 12	0.2024C675E 10
105	0.18021700E 04	0.235776750E 05	0.22665100E 12	0.23665837E 10
106	0.14222600E 04	0.185578700E 05	0.22665100E 12	0.26691000E 10
107	0.12229450E 04	0.16538330E 05	0.22665100E 12	0.26691000E 10
108	0.12604350E 04	0.170892900E 05	0.22665100E 12	0.26663638E 10
109	0.13679200E 04	0.18347750E 05	0.22665100E 12	0.26524078E 10
110	0.14734250E 04	0.19366600E 05	0.22665100E 12	0.26375683E 10
111	0.15467450E 04	0.20C01300E 05	0.22378200E 12	0.26235287E 10
112	0.15716300E 04	0.202194650E 05	0.22091300E 12	0.24090892E 10
113	0.15909C00E 04	0.203222200E 05	0.22091300E 12	0.25944497E 10
114	0.16289750E 04	0.205CC400E 05	0.22091300E 12	0.25802101E 10
115	0.16608450E 04	0.204646700E 05	0.22091300E 12	0.25657708E 10
116	0.16686150E 04	0.20695C00E 05	0.2166095E 12	0.25513310E 10
117	0.16252250E 04	0.202324200E 05	0.2123060E 12	0.25368914E 10
118	0.15144660E 04	0.19003150E 05	0.2123060E 12	0.25224518E 10
119	0.14246C00E 04	0.17995C50E 05	0.2123060E 12	0.2508C123E 10
120	0.142111450E 04	0.17939900E 05	0.2123060E 12	0.24935727E 10
121	0.14643500E 04	0.183711050E 05	0.2123060E 12	0.24791332E 10
122	0.15249150E 04	0.18924500E 05	0.2123060E 12	0.24664936E 10
123	0.15763100E 04	0.19396850E 05	0.2123060E 12	0.24502541E 10
124	0.15951400E 04	0.19565350E 05	0.20C943700E 12	0.24356146E 10
125	0.15948600E 04	0.19577C50E 05	0.20656800E 12	0.24213750E 10
126	0.15910650E 04	0.19593500E 05	0.20656800E 12	0.24069355E 10
127	0.15826900E 04	0.19569700F 05	0.20656800E 12	0.23924959E 10
128	0.15680250E 04	0.19444750E 05	0.20656800E 12	0.2378C564E 10
129	0.14876550E 04	0.18585330E 05	0.20656800E 12	0.23636168E 10
130	0.12600400E 04	0.16112200E 05	0.20369900E 12	0.23491772E 10
131	0.10130825E 04	0.13393650E 05	0.20083000E 12	0.23347377E 10
132	0.91557650E 03	0.12169500E 05	0.20083000E 12	0.23202981E 10
133	0.90865650E 03	0.11838150E 05	0.20083000E 12	0.2305E586E 10
134	0.92368500E 03	0.11664350E 05	0.20083000E 12	0.2291L190E 10
135	0.74944C50E 03	0.11493500E 05	0.20083000E 12	0.22765795E 10
136	0.95908199E 03	0.10925500E 05	0.1972A350E 12	0.22625399E 10
137	0.95665950E 03	0.10165100E 05	0.19365700E 12	0.22481004E 10
138	0.95335350E 03	0.981C1300E 04	0.19365700E 12	0.22336408E 10
139	0.94889100E 03	0.97592250E 04	0.19365700E 12	0.22192212E 10
140	0.94222C50E 03	0.9694CC00E 04	0.19365700E 12	0.22047817E 10
141	0.92402750E 03	0.98459C50E 04	0.19365700E 12	0.21903421E 10
142	0.85661C00E 03	0.11144400E 05	0.19007100E 12	0.21759026E 10
143	0.75688590E 03	0.13067600E 05	0.18648500E 12	0.21614630E 10
144	0.71345590E 03	0.12665800E 05	0.18648500E 12	0.2147C235E 10
145	0.72352150E 03	0.10415450E 05	0.18648500E 12	0.21325840E 10
146	0.77487400E 03	0.98401499E 04	0.18361600E 12	0.21181444E 10
147	0.86039550E 03	0.10718300E 05	0.18074700E 12	0.21037048E 10
148	0.90109350E 03	0.10975700E 05	0.18074700E 12	0.20892653E 10
149	0.89886650E 03	0.10653650E 05	0.18074700E 12	0.2074E257E 10
150	0.90105100E 03	0.10394600E 05	0.18074700E 12	0.20603862E 10
151	0.90456500E 03	0.101C196C50E 05	0.18074700E 12	0.20459466E 10
152	0.91463L99E 03	0.101C191500E 05	0.18074700E 12	0.20315071E 10
153	0.93132500E 03	0.103C381250E 05	0.18074700E 12	0.2017C676E 10
154	0.13146620E 04	0.15294600E 05	0.18074700E 12	0.20026280E 10
155	0.20773500E 04	0.25095C00E 05	0.18074700E 12	0.19881884E 10
156	0.24263950E 04	0.29517550E 05	0.18074700E 12	0.15354256E 10
157	0.22665100E 04	0.273734150E 05	0.17931250E 12	0.10898825E 10
158	0.19937550E 04	0.23764350E 05	0.17787800E 12	0.10898825E 10
159	0.16907C50E 04	0.198747C50E 05	0.17787800E 12	0.10898825E 10
160	0.15557600E 04	0.17683850E 05	0.17787800E 12	0.10898825E 10
161	0.16484800E 04	0.17125150E 05	0.16568A50E 12	0.10898825E 10
162	0.18140900E 04	0.18262450E 05	0.15349100E 12	0.10898825E 10
163	0.19956C00E 04	0.2055200E 05	0.15349100E 12	0.10898825E 10
164	0.21609400E 04	0.21588100E 05	0.15349100E 12	0.10898825E 10
165	0.22942C00E 04	0.21649400E 05	0.16281V5QE 12	0.10898825E 10
166	0.23626250E 04	0.21016650E 05	0.17214000E 12	0.10898825E 10
167	0.23466350E 04	0.20946100E 05	0.17214000E 12	0.10898825E 10
168	0.22942C50E 04	0.20263550E 05	0.17214000E 12	0.10898825E 10
169	0.21243950E 04	0.18446100E 05	0.17787800E 12	0.17905212E 10
170	0.21486650E 04	0.18162C50E 05	0.17787800E 12	0.24911600E 10
171	0.25099450E 04	0.20732250E 05	0.17500900E 12	0.24021900E 10

BEAM (2)

NP(2) = 173

STATION	PP	IP	EI	GA
1	0.28710550E 04	0.23152650E 05	0.17214000E 12	0.23132200E 10
2	0.30543750E 04	0.23822650E 05	0.17214000E 12	0.23132200E 10
3	0.32433950E 04	0.24679800E 05	0.17214000	

5	0.398341C0E 04	0.3C9981C0E 05	0.1721400E 12	C.23132200E 10
6	0.40095750E 04	0.31163C0E 05	0.1721400E 12	0.23132200E 10
7	0.40013400E 04	0.29875C0E 05	0.1721400E 12	0.23132200E 10
8	0.42757450E 04	0.28391R00E 05	0.1721400E 12	0.23132200E 10
9	0.49222250E 04	0.27545200E 05	0.1721400E 12	0.23132200E 10
10	0.60476400E 04	0.28451850E 05	0.1721400E 12	0.23132200E 10
11	0.71748650E 04	0.29893550E 05	0.1721400E 12	0.23132200E 10
12	0.65219C00E 04	0.28281650E 05	0.1721400E 12	0.23132200E 10
13	0.50322400E 04	0.25376100E 05	0.1721400E 12	0.23132200E 10
14	0.44664E50E 04	0.24598650E 05	0.1721400E 12	0.23132200E 10
15	0.46373100E 04	0.25966650E 05	0.1721400E 12	0.23132200E 10
16	0.45241550E 04	0.29783E00E 05	0.1721400E 12	0.23132200E 10
17	0.42023150E 04	0.32291150E 05	0.1721400E 12	0.23132200E 10
18	0.35858100E 04	0.3C0305150E 05	0.1721400E 12	0.23132200E 10
19	0.30024450E 04	0.27704600E 05	0.1721400E 12	0.23132200E 10
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21	0.28642350E 04	0.287E73200E 05	0.15492600E 12	0.21352800E 10
22	C.26931700E 04	0.3C6261300E 05	0.15492600E 12	0.21352800E 10
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26	0.17733E00E 04	0.21247750E 05	0.19796100E 12	0.29137675E 10
27	0.17028200E 04	0.20485900E 05	0.19796100E 12	0.29137675E 10
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31	0.28180C50E 04	0.32767100E 05	0.21087150E 12	0.31361925E 10
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33	0.28114450E 04	0.32624850E 05	0.17644350E 12	0.2624415CE 10
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84	0.10439C00E 04	0.12531550F 05	0.14201500E 12	0.2113C375E 10
85	0.10140780E 04	0.11845700E 05	0.14058100E 12	0.20907950E 10
86	0.94704E00E 03	0.10789C00E 05	0.13049200E 12	0.19414718E 10
87	0.89275450E 03	0.98465099E 04	0.10797820E 12	0.16082540E 10
88	0.85964E00E 03	0.91813700E 04	0.86508200E 11	0.12904847E 10
89	0.87277E50E 03	0.92524100E 04	0.77463000E 11	0.11566100E 10
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91	0.11477780E 04	0.12349450E 05	0.77463000E 11	0.11566100E 10
92	0.14726250E 04	0.15654500E 05	0.77463000E 11	0.11566100E 10
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97	0.15550150E 04	0.12775550E 05	0.73035250E 11	0.11005723E 10
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105	0.10184930E 04	0.55468700E 04	0.47054800E 11	0.87402507E C9
106	0.11572100E 04	0.63002400E 05	0.44946200E 11	0.8587C050E C9
107	0.12C21700E 04	0.61189350E 04	0.42837550E 11	0.84118673E C9
108	0.11776750E 04	0.51004C50E 04	0.40728900E 11	0.82367294E C9
109	0.12221700E 04	0.41275500E 05	0.38620300E 11	0.80615917E C9
110	0.13518600E 04	0.32C72550E 04	0.36511706E 11	0.78864538E C9
111	0.13633250E 04	0.259231350E 04	0.34697599E 11	0.77717390E C9
112	0.12260E00E 04	0.35775590E 04	0.33203600E 11	0.77227007E C9
113	0.11374150E 04	0.38859C50E 04	0.31735200E 11	0.76789162E C9
114	0.11168C00E 04	0.38155300E 04	0.30266800E 11	0.76351318E C9
115	0.12883C50E 04	0.404855350E 04	0.28798400E 11	0.75913473E C9
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117	0.17369500E 04	0.505412550E 04	0.27072500E 11	0.76797930E C9
118	0.13413300E 04	0.49358550E 04	0.26630950E 11	0.77651726E C9
119	0.13583E50E 04	0.69159C50E 04	0.26600154E 11	0.78432546E C9
120	0.17667500E 04	0.10771335E 05	0.30147900E 11	0.79162287E 09
121	0.19954C00E 04	0.13236450E 05	0.33567300E 11	0.79892028E C9
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124	0.18961550E 04	0.13430400E 05	0.26394800E 11	0.82081250E C9
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128	0.13515300E 04	0.93387849E 04	0.33567300E 11	0.85000214E C9
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130	0.94767C00E 03	0.636794200E 04	0.29837600E 11	0.81019500E 10
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156	0.51400599E 03	0.26459590E 04	0.23525800E 11	0.81165125E C9
157	0.51362749E 03	0.265153350E 04	0.17214000E 11	0.60054750E C9
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167	0.12925150E 04	0.557C5800E 04	0.17214000E 11	0.60054750E C9
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3	0.23215450E 03	0.12486525E 04	0.10034306E 11	0.35065484E C9
4	0.17858199E 03	0.94063361E 03	0.83263329E 10	0.29522286E C9
5	0.17858200E 03	0.93592300E 03	0.82413199E 10	0.29369302E C9
6	0.17858200E 03	0.93121233E 03	0.81563066E 10	0.29216316E C9
7	0.17858200E 03	0.92545181E 03	0.80712897E 10	0.29063330E C9
8	0.17858200E 03	0.91864150E 03	0.79862700E 10	0.2891C346E C9
9	0.17858200E 03	0.9118311E 03	0.79012500E 10	0.28757360E C9
10	0.19346382E 03	0.97680492E 03	0.78182378E 10	0.28604372E C9
11	0.223227750E 03	0.11135630E 04	0.77312349E 10	0.28451389E C9
12	0.25299116E 03	0.12503210E 04	0.76462316E 10	0.28298404E C9
13	0.25299113E 03	0.12414C93E 04	0.75612230E 10	0.28145414E C9
14	0.22322750E 03	0.10868285E 04	0.7476215CE 10	0.27992432E C9
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19	0.17858199E 03	0.83533343E 03	0.70511545E 10	0.27227504E C9
20	0.17858200E 03	0.82973349E 03	0.69661450E 10	0.27074520E C9
21	0.17858200E 03	0.82412849E 03	0.68811350E 10	0.26921534E C9
22	0.67691150E 04	0.28835757E 05	0.67961228E 10	0.26768547E C9
23	0.20273580E 05	0.84864651E 05	0.67111100E 10	0.26615563E C9
24	0.33670261E 05	0.14089354E 06	0.66260966E 10	0.26462578E C9
25	0.33670775E 05	0.14085512E 06	0.65410845E 10	0.26300959E C9
26	0.20275C78E 05	0.84749367E 05	0.645647C94E 10	0.26156406E C9
27	0.66793553E 04	0.28643610E 05	0.63710650E 10	0.26003621E C9
28	0.18700795E 03	0.60478249E 03	0.62902368E 10	0.25856429E C9
29	0.19792400E 03	0.63291998E 03	0.62135950E 10	0.25697650E C9
30	0.20884C00E 03	0.66105732E 03	0.61366951E 10	0.25544465E C9
31	0.21429795E 03	0.67481C66E 03	0.60631352E 10	0.25391673E C9
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33	0.21429800E 03	0.67355018E 03	0.59211635E 10	0.25085709E C9
34	0.21429795E 03	0.67215184E 03	0.58501735E 10	0.24932717E C9
35	0.21429800E 03	0.67222599E 03	0.57791850E 10	0.24779737E C9
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37	0.21429795E 03	0.67102966E 03	0.56372053E 10	0.24473760E C9
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54	0.21429800E 03	0.66031599E 03	0.44304233E 10	0.21873013E C9
55	0.21429795E 03	0.65968566E 03	0.43594339E 10	0.2172C022E C9
56	0.21429800E 03	0.65905550E 03	0.42884450E 10	0.21567042E C9
57	0.21429800E 03	0.65842516E 03	0.42174590E 10	0.21414057E C9
58	0.20453562E 03	0.63508320E 03	0.41466465E 10	0.21261066E C9
59	0.19102300E 03	0.58903001E 03	0.40754800E 10	0.21108085E C9
60	0.17550634E 03	0.54297668E 03	0.40044933E 10	0.20955100E C9
61	0.16746462E 03	0.51653103E 03	0.39335057E 10	0.20802109E C9
62	0.16691C00E 03	0.51089350E 03	0.38625200E 10	0.20645129E C9
63	0.16635133E 03	0.50485583E 03	0.37915333E 10	0.20496144E 09
64	0.16579263E 03	0.49881787E 03	0.37205457E 10	0.20343153E C9
65	0.16523400E 03	0.49278C00E 03	0.36495600E 10	0.2019C172E C9
66	0.16467533E 03	0.48674200E 03	0.35785733E 10	0.20037187E C9
67	0.16411679E 03	0.48070404E 03	0.35075842E 10	0.19884197E C9
68	0.16355585E 03	0.47466650E 03	0.34365595E 10	0.19731216E C9
69	0.16300C17E 03	0.46862883E 03	0.33656050E 10	0.19572831E C9
70	0.16244163E 03	0.46259C89E 03	0.32946159E 10	0.19425240E C9
71	0.16188300E 03	0.45855300E 03	0.32236300E 10	0.19272259E C9
72	0.16132433E 03	0.45051500E 03	0.31526434E 10	0.19119274E C9
73	0.16076579E 03	0.44447705E 03	0.30816156E 10	0.18766284E C9
74	0.16020750E 03	0.43843950E 03	0.30106700E 10	0.18813303E C9
75	0.15964917E 03	0.43240183E 03	0.29396834E 10	0.18660310E C9
76	0.15909C63E 03	0.42636389E 03	0.28868944E 10	0.18507328E C9
77	0.15853200E 03	0.42032600E 03	0.27977050E 10	0.18354346E C9
78	0.15797333E 03	0.41428800E 03	0.27267150E 10	0.18021361E C9
79	0.15741633E 03	0.40825050E 03	0.24557261E 10	0.18048371E C9
80	0.15685600E 03	0.40221250E 03	0.250847400E 10	0.17895390E C9
81	0.15629733E 03	0.39617484E 03	0.25137533E 10	0.17742405E C9
82	0.15573879E 03	0.39013691E 03	0.24427661E 10	0.17569415E 09
83	0.15518C50E 03	0.38409900E 03	0.23717800E 10	0.17436434E C9
84	0.15462217E 03	0.37806100E 03	0.23007933E 10	0.17283449E C9
85	0.15406363E 03	0.37202308E 03	0.22798045E 10	0.17130459E C9
86	0.15350500E 03	0.36598550E 03	0.21588150E 10	0.16977478E C9
87	0.15294e33E 03	0.35994783E 03	0.20878250E 10	0.16824493E C9

88	0.152393779E 03	0.35390592E 03	0.20168362E 10	0.116671503E 09
89	0.15182550E 03	0.34787200E 03	0.19458500E 10	0.116518521E 09
90	0.15127117E 03	0.34183400E 03	0.1874634E 10	0.116365536E 09
91	0.15456661E 03	0.35184172E 03	0.18038762E 10	0.116212546E 09
92	0.1737159E 03	0.37789548E 03	0.17328900E 10	0.116059564E 09
93	0.18886532E 03	0.43594515E 03	0.16619034E 10	0.115906579E 09
94	0.18805657E 03	0.39807826E 03	0.15909163E 10	0.115753589E 09
95	0.17127301E 03	0.36028302E 03	0.15199300E 10	0.115606008E 09
96	0.15449501E 03	0.32486796E 03	0.14489434E 10	0.11547623E 09
97	0.14557513E 03	0.3C131159E 03	0.13779547E 10	0.115294633E 09
98	0.14452550E 03	0.29675500E 03	0.13069650E 10	0.115141651E 09
99	0.14347183E 03	0.29219833E 03	0.12359751E 10	0.114988666E 09
100	0.82122507E 03	0.66955844E 03	0.12819696E 10	0.115186923E 09
101	0.21777515E 04	0.14288394E 04	0.14450349E 10	0.115736466E 09
102	0.35343561E 04	0.21881192E 04	0.16088715E 10	0.116285999E 09
103	0.45400594E 04	0.23621216E 04	0.17106233E 10	0.11658C934E 09
104	0.51949145E 04	0.19508503E 04	0.17526956E 10	0.116621320E 09
105	0.58497643E 04	0.15395771E 04	0.17947649E 10	0.116661690E 09
106	0.62490488E 04	0.12873239E 04	0.18287548E 10	0.116681859E 09
107	0.63927869E 04	0.1194C951E 04	0.18566706E 10	0.116681875E 09
108	0.65365148E 04	0.11008651E 04	0.18805833E 10	0.116681875E 09
109	0.65923719E 04	0.1C287G61E 04	0.18935381E 10	0.116681859E 09
110	0.65603746E 04	0.97762103E 03	0.18935400E 10	0.116681875E 09
111	0.65283711E 04	0.92653504E 03	0.18935400E 10	0.116681875E 09
112	0.64874437E 04	0.87407304E 03	0.18935381E 10	0.116681859E 09
113	0.64376700E 04	0.82023753E 03	0.18935400E 10	0.116681875E 09
114	0.63878700E 04	0.7664C121E 03	0.18935400E 10	0.116681875E 09
115	0.63828506E 04	0.7610C221E 03	0.18935381E 10	0.116681859E 09
116	0.64227499E 04	0.4AC41C596E 03	0.18935400E 10	0.116681875E 09
117	0.64626233E 04	0.44718795E 03	0.18935400E 10	0.116681875E 09
118	0.64825237E 04	0.86872836E 03	0.18935381E 10	0.116681859E 09
119	0.64825200E 04	0.86872500E 03	0.18935400E 10	0.116681875E 09
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121	0.64557700E 04	0.83986225E 03	0.18935381E 10	0.116681859E 09
122	0.64022700E 04	0.78196903E 03	0.18935400E 10	0.116681875E 09
123	0.63487634E 04	0.72412505E 03	0.18935400E 10	0.116681875E 09
124	0.63127405E 04	0.68519502E 03	0.18935381E 10	0.116681859E 09
125	0.62942220E 04	0.66516901E 03	0.18935400E 10	0.116681875E 09
126	0.62756533E 04	0.64514234E 03	0.18935400E 10	0.116681875E 09
127	0.63C83521E 04	0.68045656E 03	0.18935381E 10	0.116681859E 09
128	0.63923349E 04	0.77123392E 03	0.18935400E 10	0.116681875E 09
129	0.64762715E 04	0.86197C57E 03	0.18935400E 10	0.116681875E 09
130	0.65182336E 04	0.90733812E 03	0.18935381E 10	0.116681859E 09
131	0.65182400E 04	0.9C733500E 03	0.18935400E 10	0.116681875E 09
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133	0.65431718E 04	0.93429486E 03	0.18935381E 10	0.116681859E 09
134	0.65930549E 04	0.98820542E 03	0.18935400E 10	0.116681875E 09
135	0.64429315E 04	0.1C621231E 04	0.18935400E 10	0.116681875E 09
136	0.67136367E 04	0.11185621E 04	0.18935381E 10	0.116681859E 09
137	0.68051698E 04	0.12175298E 04	0.18935400E 10	0.116681875E 09
138	0.68967365E 04	0.13164565E 04	0.18935400E 10	0.116681875E 09
139	0.69267C16E 04	0.13695753E 04	0.18935381E 10	0.116681859E 09
140	0.68951505E 04	0.13779700E 04	0.18935400E 10	0.116681875E 09
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143	0.411179727E 04	0.13896600E 04	0.188262950E 10	0.116681875E 09
144	0.22981531E 04	0.13896400E 04	0.18754650E 10	0.116681875E 09
145	0.13032552E 04	0.13899587E 04	0.18158234E 10	0.116681859E 09
146	0.11305802E 04	0.13895200E 04	0.170371752E 10	0.116681875E 09
147	0.95880695E 03	0.13896000E 04	0.15917252E 10	0.116681875E 09
148	0.80031889E 03	0.15C59399E 04	0.13562559E 10	0.114457616E 09
149	0.65511E71E 03	0.17379407E 04	0.99737050E 09	0.1C009131E 09
150	0.18841829E 04	0.19698681E 04	0.63848367E 09	0.5560E2292E 08

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3	0.27520866E 04	0.29752583E 04	0.14451154E 10	1.1035C164E 09
4	0.31568781E 04	0.31568608E 04	0.16140916E 10	1.1199E168E 09
5	0.34129750E 04	0.32819250E 04	0.15576150E 10	0.12482663E 09
6	0.36669716E 04	0.33678716E 04	0.15011383E 10	0.12965157E 09
7	0.36570232E 04	0.32229596E 04	0.14466461E 10	0.13455650E 09
8	0.33768300E 04	0.28475700E 04	0.13881856E 10	0.13942144E 09
9	0.30966336E 04	0.24721433E 04	0.13317103E 10	0.14426638E 09
10	0.28637215E 04	0.21840408E 04	0.12757882E 10	0.14915131E 09
11	0.26780E050E 04	0.19832850E 04	0.12204253E 10	0.15401626E 09
12	0.24926483E 04	0.17825217E 04	0.11650617E 10	0.15888120E 09
13	0.22897580E 04	0.15831531E 04	0.11160898E 10	0.16374611E 09
14	0.20700150E 04	0.13853C00E 04	0.10735100E 10	0.16661107E 09
15	0.18502717E 04	0.11874067E 04	0.10309300E 10	0.17347601E 09
16	0.17081765E 04	0.10607188E 04	0.98834844E 09	0.17834093E 09
17	0.16437300E 04	0.10052363E 04	0.94576555E 09	0.1832C589E 09
18	0.15792E233E 04	0.94975417E 03	0.90318256E 09	0.18807083E 09
19	0.15148349E 04	0.89427128E 03	0.88606028E 09	0.19293575E 09
20	0.145038350E 04	0.83878801E 03	0.81801900E 09	0.1978C070E 09
21	0.13859350E 04	0.7833C467E 03	0.77543767E 09	C.2026E564E 09
22	0.13214649E 04	0.72782146E 03	0.73286294E 09	0.20753056E 09
23	0.12573050E 04	0.67233850E 03	0.69027500E 09	0.21239551E 09
24	0.119256552E 04	0.61685550E 03	0.64769367E 09	0.21726045E 09
25	0.11237494E 04	0.56336214E 03	0.54401966E 09	0.19716435E 09
26	0.10505285E 04	0.51185851E 03	0.37925303E 09	0.1521C722E 09
27	0.97730751E 03	0.46033548E 03	0.214468367E 09	0.10705008E 09
28	0.89613547E 03	0.41245657E 03	0.131513537E 09	0.84521479E 09
29	0.80701301E 03	0.36816401E 03	0.13039600E 09	0.84521500E 09
30	0.71789C35E 03	0.32387134E 03	0.12925800E 09	0.84521500E 09
31	0.62876771E 03	0.27957877E 03	0.12811997E 09	0.84521479E 09
32	0.53964552E 03	0.23528650E 03	0.12698200E 09	0.84521500E 09
33	0.45052319E 03	0.19095418E 03	0.12584000E 09	0.84521500E 09
34	0.36140C60E 03	0.1467C176E 03	0.124703597E 09	C.84521479E 09
35	0.27227203E 03	0.10240937E 03	0.12356800E 09	0.84521500E 09
36	0.18315533E 03	0.58116937E 02	0.12243000E 09	0.84521500E 09
37	0.12740C44E 03	0.3C407690E 02	0.12129197E 09	0.84521479E 09
38	0.10501341E 03	0.19281689E 02	0.12015400E 09	0.84521500E 09
39	0.82426234E 02	0.81556802E 01	0.11901600E 09	0.84521500E 09
40	0.71432782E 02	0.25926693E 01	0.11787757E 09	0.84521479E 09
41	0.71432800E 02	0.259267C0E 01	0.11674000E 09	0.84521500E 09
42	0.71432800E 02	0.25926700E 01	0.11560200E 09	0.84521500E 09
43	0.71432782E 02	0.25926693E 01	0.11427764E 09	0.84521479E 09
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46	0.71432782E 02	0.25926693E 01	0.10972947E 09	0.84521479E 09
47	0.71432800E 02	0.25926700E 01	0.10818650E 09	0.84521500E 09
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52	0.71432783E 02	0.25926693E 01	0.10047054E 09	0.84521479E 09
53	0.71432800E 02	0.25926700E 01	0.98927700E 08	0.84521500E 08
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55	0.90556625E 02	0.30553387E 01	0.95841834E 08	0.84521500E 08
56	0.1288043RF 03	0.33986796E 01	0.94298800E 08	0.84521500E 08
57	0.16705211E 03	0.49C6C196E 01	0.92755734E 08	0.84521500E 08
58	0.21547092E 03	0.6C774296E 01	0.91212644E 08	0.84521479E 08
59	0.27490C97E 03	0.74994145E 01	0.89666000E 08	0.84521500E 08

61	0.369461690E 04	0.379746206E 01	0.11492428E 09	0.134461552E C9
62	0.38435699E 03	0.10141620E 02	0.1700298E 09	0.2342C376E C9
63	0.39330C99E 03	0.1C486406E 02	0.22520163E 09	0.33395194E C9
64	0.40091307E 03	0.1C508466E 02	0.22464417E 09	0.35267700E C9
65	0.38419554E 03	0.1C21C105E 02	0.16939062E 09	0.29025902E C9
66	0.37747784E 03	0.98949418E 01	0.11213703E 09	0.22784097E C9
67	0.40492401E 03	0.1C361C05E 02	0.9C330466E 08	0.23651862E C9
68	0.47154C45E 03	0.116C2404E 02	0.10297109E 09	0.31625239E C9
69	0.53815479E 03	0.12843C01E 02	0.11561169E 09	0.39606610E C9
70	0.57146185E 03	0.13463296E 02	0.12193197E 09	0.43595289E C9
71	0.57146200E 03	0.134643C0E 02	0.12193206E 09	0.43595300E C9
72	0.57146200E 03	0.134643300E 02	0.12193206E 09	0.43595300E C9
73	0.57146185E 03	0.13463296E 02	0.12193197E 09	0.43595289E 09
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76	0.57146185E 03	0.13463296E 02	0.12193197E 09	0.43595289E C9
77	0.57146200E 03	0.13463300E 02	0.12193200E 09	0.43595300E C9
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79	0.57146185E 03	0.13463296E 02	0.12193197E 09	0.43595289E C9
80	0.57146200E 03	0.13463300E 02	0.12193206E 09	0.43595300E C9
81	0.57146200E 03	0.13463300E 02	0.12193206E 09	0.43595300E C9
82	0.57146185E 03	0.13463296E 02	0.12193197E 09	0.43595289E C9
83	0.57146200E 03	0.13463300E 02	0.12193206E 09	0.43595300E C9
84	0.57146200E 03	0.13463300E 02	0.12193206E 05	0.43595300E C9
85	0.57146185E 03	0.13463296E 02	0.12193197E 09	0.43595289E C9
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90	0.57146200E 03	0.13463300E 02	0.12193206E 09	0.43595300E C9
91	0.57146185E 03	0.13463296E 02	0.12193197E 09	0.43595289E C9
92	0.57146200E 03	0.13463300E 02	0.12193206E 09	0.43595300E C9
93	0.57146200E 03	0.13463300E 07	0.12193206E 09	0.43595300E C9
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99	0.57146200E 03	0.13463300E 02	0.12193206E 09	0.43595300E C9
100	0.57146144E 03	0.13463287E 02	0.12193188E 09	0.43595258E C9
101	0.57146200E 03	0.13463300E 02	0.12193206E 09	0.43595300E C9
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103	0.57146144E 03	0.13463287E 02	0.12193188E 09	0.43595258E C9
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106	C.55852C81E 03	0.13162C204E 02	0.12193188E 09	0.43595258E C9
107	0.53264C01E 03	0.125554540E 02	0.12193204E 09	0.43595300E C9
108	0.50675869E 03	0.11956884E 01	0.12193206E 09	0.43595300E C9
109	0.45983564E 03	0.10864386E 02	0.10809426E 09	C.39072631E C9
110	C.39197205E 03	0.92819860E 01	0.81049019E 08	0.3C027381E C9
111	0.32390806E 03	0.76995765E 01	0.53793692E 08	0.20982100E C9
112	C.25594371E 03	0.61171609E 01	0.4C165941E 08	0.14455434E C9
113	0.18797570E 03	0.45347561E 01	0.40166C0CE 08	0.16455450E C9
114	0.12C0154RF 03	0.25523465E 01	0.4016600GE 08	0.16455450E C9
115	0.11266400E 03	0.28744439E 01	0.40165941E 08	0.16455434E C9
116	0.16586411E 03	0.43011239E 01	0.40166000E 08	0.16455450E C9
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121	0.28573C72E 03	0.74903627E 01	0.88939194E 08	0.31584320E C9
122	0.28573100E 03	0.74903700E 01	0.88939000E 08	0.31584350E C9
123	0.28573100E 03	0.74903700E 01	0.88939000E 08	0.31584350E C9
124	0.28573C72E 03	0.74903627E 01	0.81766438E 08	C.29062351E C9
125	0.28573100E 03	0.74903700E 01	0.6742151UE 08	0.24021904E C9
126	0.28573100E 03	0.74903700E 01	0.53076514E 08	0.18982727E C9
127	0.28573C72E 03	0.74903627E 01	0.45903956E 08	0.16455434E C9
128	0.28573100E 03	0.74903700E 01	0.45904000E 08	0.16455450E C9
129	0.28573100E 03	0.74903700E 01	0.45904000E 08	0.16455450E C9
130	0.28573C72E 03	0.74903627E 01	0.45903956E 08	0.16455434E C9
131	0.28573100E 03	0.74903700E 01	0.45904000E 08	0.16455450E C9
132	0.28573100E 03	0.74903700E 01	0.45904000E 08	0.16455450E C9
133	0.41664345E 03	0.92404951E 01	0.45075625E 08	0.16162426E C9
134	0.67847C12E 03	0.12740783E 02	0.43419002E 08	0.15568424E C9
135	0.94029633E 03	0.16241C55E 02	0.41762335E 08	0.14974407E C9
136	0.11447771E 04	0.18825C46F 02	0.39051416E 08	0.14002375E C9
137	0.12919148E 04	0.2C504797E 02	0.35286355F 08	0.12652368E C9
138	0.14393514E 04	0.22180530E 02	0.31521256E 08	0.11302347E C9
139	0.12825268E 04	0.1941C767E 02	0.27756128E 08	0.99523165E C9
140	0.82234316E 03	0.12213C5340E 02	0.23991055E 08	C.86023057E C9
141	0.36215828E 03	0.501C2556E 01	0.20225956E 08	0.72522853E 08
142	0.12327657E 03	0.12856279E 01	0.16460850E 08	0.59022582E C9
143	0.10573C02E 03	0.10395668E 01	0.12695790E 08	0.45522434E C9
144	0.88123350E 02	0.7935C440E 00	0.89307119E 07	0.32022221E C9

COMPUTED TERMS FOLLOW * * *

BEAM	RW	BJ	R1	R2
1	C.13429962E 06	0.20799750E 07	0.49659474E 08	C.49659474E 08
2	C.63644605E 05	0.96462209E 06	0.25955327E 08	C.25955327E 08
3	C.34593462E 05	0.26161592E 06	0.25628602E 07	C.25628602E 07
4	C.89404071E 04	0.35268672E 05	0.27559190E 06	C.27559190E 06

TOTAL VEHICLE MASS AND LOCATION OF CG

TVM = 0.24147809E 06 LB-SEC=2/IN
 = 0.93307135F 0E LBM

XMC = 0.35536069E 02 IN

CONVERSION FACTORS FOR INPUT DATA

FMP = -0.0C000000E-38
 FIP = -0.0C00C000E-38
 FEI = -0.0C00C000E-38
 FGA = -0.0C000000E-38

LATERAL SUPPORT SPRING CONSTANTS

BEAM	SSL1	SSL2	SSR1	SSR2
1	C.0C000000E-38	0.0C000000E-38	0.0CCC0000E-38	C.0C000000E-38
2	C.00010000E-38	0.0C000000E-38	0.0C000000E-38	C.0C000000E-38
3	C.00001000E-38	0.00000000E-38	0.00000000E-38	C.00000000E-38
4	C.00000100E-38	0.00000000E-38	0.00000000E-38	C.00000000E-38

ROTATIONAL SUPPORT SPRING CONSTANTS

BEAM	RSL1	RSL2	RSR1	RSR2
1	C.0C000000E-38	0.0C000000E-38	0.0CCC0000E-38	C.0C000000E-38
2	C.00001000E-38	0.00000000E-38	0.0C000000E-38	C.00000000E-38
3	C.00000100E-38	0.00000000E-38	0.00000000E-38	C.00000000E-38
4	C.00000010E-38	0.00000000E-38	0.0C000000E-38	C.00000000E-38

BRANCH BEAM SPRING CONSTANTS

SKB(I,J,K)	I = INTERSTAGE NUMBER
I	(I,1,1) (I,1,2) (I,2,1) (I,2,2)
1	C.0C0000000E-38 0.00000000E-38 0.0C0000000E-38 C.0C0000000E-38
2	C.000000000E-38 0.00000000E-38 0.0CCC00000E-38 C.000000000E-38
3	C.000000000E-38 0.00000000E-38 0.00000000E-38 C.000000000E-38
4	C.0C0000000E-38 0.00000000E-38 0.0C0000000E-38 C.0C0000000E-38

INTERSTAGE SPRING CONSTANTS

SK(I,J,K)	I = INTERSTAGE NUMBER
I J K = 1 2 3 4	
1 1 0.1C000000E 14 C.0CCC0000E-38 0.00000000E-38 C.000C0000E-38	
2 1 0.0C000000E-38 0.11C00000E 14 0.00000000E-38 C.000C0000E-38	
3 1 0.1C000000E-38 C.000C00000E-38 0.00000000E-38 C.000C0000E-38	
4 1 0.0C000000E-38 C.0CC00000E-38 0.00000000E-38 C.000C0000E-38	
2 1 0.1C000000E-13 C.0CCC00000E-38 0.00000000E-38 C.000C0000E-38	
2 2 0.0C000000E-38 C.011C00000E-13 0.00000000E-38 C.000C0000E-38	
3 1 0.0C000000E-38 C.0CCC00000E-38 0.00000000E-38 C.000C0000E-38	
4 1 0.1C000000E-38 C.0CCC00000E-38 0.00000000E-38 C.000C0000E-38	
3 1 0.18404000E 10 0.18362325E 10 0.00000000E-38 C.000C0000E-38	
2 1 0.18404000E-38 C.0184C4000E-10 0.00000000E-38 C.000C0000E-38	
3 1 0.1C000000E-38 C.0CCC00000E-38 0.18404000E 10 C.18362325E 10	
4 1 0.0C000000E-38 C.0CCC00000E-38 0.00000000E-38 C.000C0000E-38	

BEAM	SHP FCN	Y1	Y2	Y21	Y22
1	1	-C.5795054E 05	-C.5795054E 05	-0.11474881E C7	-C.11474881E C7
	2	-C.74414619E 05	-C.74414619E 05	-0.13084633E C7	-C.13084633E C7
	3	-C.86638563E 05	-C.86638563E 05	-0.13936237E C7	-C.13936237E C7
	4	-C.0CC00000E-19	-C.0CC00000E-19	-0.00000000E-19	-C.00000000E-19
2	1	C.31820540E 05	C.31820540E 05	0.65802879E C6	C.658C2879E 06
	2	-C.29023572E 05	-C.29023572E 05	-0.65179473E C6	-C.65179473E 06
	3	-C.33274451E 05	-C.33274451E 05	-0.65988696E C6	-C.65988696E C6
	4	-C.0CC00000E-19	-C.0CC00000E-19	-0.00000000E-19	-C.00000000E-19
3	1	C.21836667E 05	C.21836667E 05	0.18435450E C6	C.18425450E C6
	2	-C.19839012E 05	-C.19839012E 05	-0.170C4398E C6	-C.170C4398E C6
	3	-C.18193060E 05	-C.18193060E 05	-0.14681895E C6	-C.14681895E 06
	4	-C.0CC00000E-19	-C.0CC00000E-19	-0.00000000E-19	-C.00000000E-19
4	1	-C.38874516E 04	-C.38874516E 04	-0.20009396E C5	-C.200C9396E C5
	2	-C.35203453E 04	-C.35203453E 04	-0.24665668E C5	-C.24665668E C5
	3	-C.4C340005E 04	-C.4C340005E 04	-0.21722366E C5	-C.21722366E C5
	4	-C.0CC00000E-19	-C.0CC00000E-19	-0.00000000E-19	-C.00000000E-19
BEAM	SHP FCN	Y1PL	Y2PL	Y1PR	Y2PR
BEAM	SHP FCN	Y1PL	Y2PL	Y1PR	Y2PR
1	1	-0.25289939E-01	-C.25289939E-01	0.21735917E C0	0.21735917E 00
	2	-0.37162976E-01	-C.37162976E-01	0.14599744E 00	C.14599744E 00
	3	-C.1C485152E 00	-C.1C485152E 00	0.39014370E-C1	C.39014370E-C1
	4	-C.0CC00000E-19	-C.0CC00000E-19	-0.00000000E-19	-C.00000000E-19
2	1	0.48960096E-01	0.48960098E-01	-0.71741068E-C1	-C.71741068E-C1
	2	-0.35144027E-01	-C.35144027E-01	0.20295327E CC	C.20295327E CC
	3	-0.86091162E-01	-C.86091162E-01	0.65758556E-C1	0.65758556E-C1
	4	-C.0CC00000E-19	-C.0CC00000E-19	-0.00000000E-19	-C.00000000E-19
3	1	0.12360351E 00	C.12360351E 00	-0.15875683E 00	-C.15875683E 00
	2	-C.86662955E-01	-C.86662955E-01	0.62426668E C0	C.62426668E C0
	3	-C.36018053E 00	-C.36018053E 00	0.13207106E C0	C.13207106E C0
	4	-C.0CC00000E-19	-C.0CC00000E-19	-0.00000000E-19	-C.00000000E-19
4	1	0.48960096E 00	0.48960098E 00	0.19591540E C0	C.19591540E 00
	2	-C.18929621E 00	-C.18929621E 00	0.79334632E CC	C.79334632E CC
	3	-0.25864947E 00	-0.25864947E 00	0.25836378E C0	C.25836378E C0
	4	-C.0CC00000E-19	-C.0CC00000E-19	-0.00000000E-19	-C.00000000E-19

G1(I,J,K)	I = BEAM NUMBER	J,K = SHAPE FUNCTION NUMBERS
1	I J K = 1	2
	1	0.57863017E 09
	2	0.36086964E 09
	3	0.44080864E 09
2	4	-0.0CC00000E-19
	1	0.25442211E 08
	2	-0.26922318E 08
	3	-0.3C794295E 08
3	4	-0.0CC00000E-19
	1	0.4331725E 08
	2	-0.36769463E 08
	3	-0.35570333E 08
4	4	-0.0CC00000E-19
	1	0.65840589E 07
	2	0.19352083E 07
	3	0.51258183E 07
5	4	-0.0CC00000E-19
	I J K = 2	3
	1	C.36C86964E 09
	2	C.24243176E 09
	3	C.65581643E 08
	4	-C.0CC00000E-19
6	1	C.26522318E 08
	2	C.76437541E 08
	3	C.24694575E 08
	4	-C.0CC00000E-19
7	1	-C.36769463E 08
	2	0.1531071RE 09
	3	0.23873370E 08
	4	-C.0CC00000E-19
8	1	0.4331725E 08
	2	-0.36769463E 08
	3	-0.35570333E 08
	4	-0.0CC00000E-19
9	1	0.65840589E 07
	2	0.19352083E 07
	3	0.51258183E 07
	4	-0.0CC00000E-19
G2(I,J,K)	I = BEAM NUMBER	J,K = SHAPE FUNCTION NUMBERS
1	I J K = 1	2
	1	0.57863017E 09
	2	0.36086964E 09
	3	0.44080864E 09
2	4	-0.0CC00000E-19
	1	0.25442211E 08
	2	-0.26922318E 08
	3	-0.3C794295E 08
3	4	-0.0CC00000E-19
	1	0.4331725E 08
	2	-0.36769463E 08
	3	-0.35570333E 08
4	4	-0.0CC00000E-19
	I J K = 2	3
	1	C.19352083F 07
	2	C.84892875E 07
	3	C.25595624E 07
	4	-0.0CC00000E-19
5	1	0.51258183E 07
	2	0.25595624E 07
	3	C.42230257E 07
	4	-0.0CC00000E-19
6	1	0.65840589E 07
	2	0.19352083E 07
	3	0.51258183E 07
	4	-0.0CC00000E-19

BYZ1(I,J,K)		I = BEAM NUMBER J,K = SHAPE FUNCTION NUMBERS				
1		1	0.42356304E 05	C.4E43471E 05	0.47090285E 05	-C.000C0000E-19
2		2	0.4E43471E 05	C.54068772E 05	0.58792282E C5	-C.000C0000E-19
3		3	0.47090285E 05	C.58792282E 05	0.69862051E C5	-C.000C0000E-19
4		4	-0.0C000000E-19	-0.0CC00000E-19	-0.0000000E-19	-C.000C0000E-19
2		1	0.24038240E 05	-C.22761673E 05	-0.24804631E C5	-C.000C0000E-19
2		2	-0.22761673E 05	C.22210844E 05	0.23173659E C5	-C.000C0000E-19
3		3	-0.24804031E 05	C.23173659E 05	0.25916231E 05	-C.000C0000E-19
4		4	-0.0C000000E-19	-0.0000000E-19	-0.0000000E-19	-C.000C0000E-19
3		1	0.16583064E 05	-0.15504325E 05	-0.14394384E 05	-0.000C0000E-19
2		2	-0.15504325E 05	0.15C10293E 05	0.13004556E C5	-C.000C0000E-19
3		3	-0.14394384E 05	C.13C04556E 05	0.14863855E 05	-C.000C0000E-19
4		4	-0.0C000000E-19	-0.0CC00000E-19	-0.0000000E-19	-C.000C0000E-19
4		1	0.3C095205E 04	C.2775070RE 04	0.30244214E C4	-C.000C0000E-19
2		2	0.27750708F 04	C.29768123E 04	0.29117187E C4	-C.000C0000E-19
3		3	0.3C244214F 04	C.29117187F 04	0.30781721E 04	-C.000C0000E-19
4		4	-0.0C000000E-19	-0.0CC00000E-19	-0.0000000E-19	-C.000C0000E-19

BYZ2(I,J,K)		I = BEAM NUMBER J,K = SHAPE FUNCTION NUMBERS					
1	J	K =	1	2	3	4	
1			1	2	3	4	
1			1	0.42356304E 05	C.4E43471E 05	0.47090285E 05	-C.000C0000E-19
2			2	0.4E43471E 05	C.54068772E 05	0.58792282E C5	-C.000C0000E-19
3			3	0.47090285E 05	C.58792282E 05	0.69862051E C5	-C.000C0000E-19
4			4	-0.0C000000E-19	-0.0CC00000E-19	-0.0000000E-19	-C.000C0000E-19
2			1	0.24038240E 05	-C.22761673E 05	-0.24804031E 05	-C.000C0000E-19
2			2	-0.22761673E 05	C.22210844E 05	0.23173659E 05	-C.000C0000E-19
3			3	-0.24804031E 05	C.23173659E 05	0.25916231E 05	-C.000C0000E-19
4			4	-0.0C000000E-19	-0.0CC00000E-19	-0.0000000E-19	-C.000C0000E-19
3			1	0.16583064E 05	-0.15504325E 05	-0.14394384E 05	-0.000C0000E-19
2			2	-0.15504325E 05	0.15C10293E 05	0.13004556E C5	-C.000C0000E-19
3			3	-0.14394384E 05	C.13C04556E 05	0.14863855E 05	-C.000C0000E-19
4			4	-0.0C000000E-19	-0.0CC00000E-19	-0.0000000E-19	-C.000C0000E-19
4			1	0.3C095205E 04	C.27750708F 04	0.30244214E C4	-C.000C0000E-19
2			2	0.27750708F 04	C.29768123E 04	0.29117187E C4	-C.000C0000E-19
3			3	0.3C244214E 04	C.29117187F 04	0.30781721E 04	-C.000C0000E-19
4			4	-0.0C000000E-19	-0.0CC00000E-19	-0.0000000E-19	-C.000C0000E-19

PNU1(I)	0.0C000000F-38	0.00CC0000E-38	0.00000000E-38	-0.0C000000E-19	-0.00000000E-19	-0.00CC0000E-19
	-0.0C000000E-19	-0.0CC00000E-19	-0.00000000E-19	-0.0C000000E-19	-0.00000000E-19	-0.00CC0000E-19

CNU1(I)	0.1C000000E 01	0.10000000E 01	0.10000000E 01	-0.CCC0000E-19	-0.0C000000E-19	-0.000C0000E-19
	-0.0C000000E-19	-0.0CC00000E-19	-0.00000000E-19	-0.0C000000E-19	-0.00000000E-19	-0.00CC0000E-19

SNU1(I)	0.0C000000E-38	0.00000000E-38	0.00000000E-38	-0.0C000000E-19	-0.0C000000E-19	-0.00000000E-19
	-0.0C000000E-19	-0.0CC00000E-19	-0.00000000E-19	-0.0C000000E-19	-0.00000000E-19	-0.00CC0000E-19

THE ANGULAR DISPLACEMENT COEFFICIENT MATRIX, C FOLLOWS

	COLUMN(1)	COLUMN(2)	COLUMN(3)	COLUMN(4)	COLUMN(5)	COLUMN(6)	COLUMN(7)	COLUMN(8)	COLUMN(9)	COLUMN(10)
RW(1)	2.3392E-02	-4.6648E-02	2.3256E-02	0.0000E-39						
RW(2)	0.0000E-39	0.0000E-39	-0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	2.3392E-02	-4.6648E-02	2.3256E-02
RW(3)	0.0000E-39	2.3256E-02	-1.0326E-01	8.0000E-02	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(4)	0.0000E-39	0.0000E-39	0.0000E-39	-0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	2.3256E-02	-1.0326E-01
RW(5)	0.0000E-39	0.0300E-39	8.0000E-02	-4.0800E-00	4.0000E-00	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(6)	0.0000E-39	0.0000E-39	0.0000E-39	4.0000E-00	-4.0800E-00	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(7)	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	-0.0000E-39	0.0000E-39	0.0000E-39	8.0000E-02	-4.0800E-00	0.0000E-39
RW(8)	0.0000E-39	4.0000E-00								
	COLUMN(11)	COLUMN(12)	COLUMN(13)	COLUMN(14)	COLUMN(15)	COLUMN(16)	COLUMN(17)	COLUMN(18)	COLUMN(19)	COLUMN(20)
RW(1)	0.0000E-39	0.0000E-39	-2.1736E-01	-1.4600E-01	-3.9014E-02	4.8900E-02	-3.9144E-02	-8.6051E-02	0.0000E-39	0.0000E-39
RW(2)	0.0000E-39									
RW(3)	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	7.1741E-02	-2.0295E-01	-6.5759E-02	1.2366E-01	-8.6663E-02
RW(4)	0.0000E-39									
RW(5)	0.0000E-39									
RW(6)	-0.0000E-39	0.0000E-39	1.5876E-01	-6.2427E-01						
RW(7)	4.0000E-00	0.0000E-39								
RW(8)	-4.0833E-00	8.3333E-02	0.0000E-39							
	COLUMN(21)	COLUMN(22)	COLUMN(23)	COLUMN(24)	COLUMN(25)	COLUMN(26)	COLUMN(27)	COLUMN(28)	COLUMN(29)	COLUMN(30)
RW(1)	0.0000E-39									
RW(2)	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	-2.1736E-01	-1.4600E-01	-3.9014E-02	4.8900E-02	-3.9144E-02
RW(3)	-3.6018E-01	0.0000E-39								
RW(4)	0.0000E-39	7.1741E-02	-2.0295E-01							
RW(5)	-1.0207E-01	0.0000E-39								
RW(6)	0.0000E-39	-3.6237E-01	-1.0207E-01	-2.9865E-01	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(7)	0.0000E-39									
RW(8)	0.0000E-39									
	COLUMN(31)	COLUMN(32)	COLUMN(33)	COLUMN(34)	COLUMN(35)	COLUMN(36)	COLUMN(37)			
RW(1)	0.0000E-39									
RW(2)	0.0000E-39									
RW(3)	0.0000E-39	-0.0000E-39	-0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39			
RW(4)	1.2360E-01	-8.6663E-02	-3.6018E-01	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39			
RW(5)	0.0000E-39									
RW(6)	0.0000E-39									
RW(7)	1.5876E-01	-6.2427E-01	-1.0207E-01	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39			
RW(8)	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	-3.6237E-01	-1.0207E-01	-2.9865E-01			

THE STIFFNESS MATRIX, S FOLLOWS

	COLUMN(1)	COLUMN(2)	COLUMN(3)	COLUMN(4)	COLUMN(5)	COLUMN(6)	COLUMN(7)	COLUMN(8)	COLUMN(9)	COLUMN(10)
RW(1)	1.0000E-13	0.0000E-39								
RW(2)	0.0000E-39	1.1000E-13	0.0000E-39							
RW(3)	0.0000E-39	0.0000E-39	1.0000E-13	0.0000E-39						
RW(4)	0.0000E-39	0.0000E-39	0.0000E-39	1.0000E-13	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(5)	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	1.0000E-13	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(6)	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	1.0000E-13	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(7)	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	1.0000E-13	0.0000E-39	0.0000E-39	0.0000E-39
RW(8)	0.0000E-39	1.0000E-13	0.0000E-39	0.0000E-39						

THE K-E. MATRIX, A FBLLBWS

COLUMN(1)	COLUMN(2)	COLUMN(3)	COLUMN(4)	COLUMN(5)	COLUMN(6)	COLUMN(7)	COLUMN(8)	COLUMN(9)	COLUMN(10)
RW(1)	6.4163E 04	2.1482E 04	0.00CCE-39	0.00CCE-39	0.00UOE-39	0.0CCE-39	C.CCCCE-39	0.0CCDE-39	0.00CCE-39
RW(2)	2.1492E 04	5.9498E 04	4.3956E 03	0.0CCE-39	0.0UOE-39	0.00EDE-39	0.CCCE-39	0.0CCDE-39	0.00CCE-39
RW(3)	0.0C00E-39	8.3956E 03	2.3174E 04	4.5273E 03	0.00OEE-39	0.00OEE-39	0.CCCE-39	0.0CCDE-39	0.00OEE-39
RW(4)	0.0300E-39	0.0000E-39	4.5273E 03	1.6402E 04	0.0L00E-39	0.CCCE-39	0.CCCCE-39	0.0CCDE-39	0.0000E-39
RW(5)	0.0300E-39	0.0000E-39	0.00CCE-39	0.00CCE-39	4.9761E C3	1.0252E C3	C.CD0E-39	0.00CCE-39	0.00CCE-39
RW(6)	0.0UOE-39	0.0000E-39	0.00CCE-39	0.0000E-39	1.0252E C3	0.9138E C3	0.00OEE-39	0.0CCDE-39	0.00CCE-39
RW(7)	0.0C00E-39	0.0000E-39	0.00CCE-39	0.0000E-39	0.00OEE-39	0.0CCE-39	6.4163E 04	2.1482E 04	0.00CCE-39
RW(8)	0.0300E-39	0.0000E-39	0.00CCE-39	0.0000E-39	0.0UOE-39	0.0CCE-39	2.1492E 04	5.9498E 04	8.3956E 03
RW(9)	0.0C00E-39	0.0000E-39	0.00CCE-39	0.0000E-39	0.0UOE-39	0.00OEE-39	0.CCCE-39	0.0CCDE-39	0.00OEE-39
RW(10)	0.C300E-39	0.0000E-39	0.00CCE-39	0.0000E-39	0.0CCE-39	0.00OEE-39	0.CCCE-36	0.0CCDE-39	4.5273E 03
RW(11)	0.C300E-39	0.0000E-39	0.00CCE-39	0.0000E-39	0.0CCE-39	0.00OEE-39	0.CCCE-39	0.0CCDE-39	0.00OEE-39
RW(12)	0.0000E-39	0.0000E-39	0.00CCE-39	0.0000E-39	0.0CCE-39	0.00OEE-39	0.CCCE-39	0.0CCDE-39	0.0000E-39
RW(13)	-3.1109E 04	-2.6842E 04	0.00CCE-39	0.00UOE-39	0.00OEE-39	0.00CCE-39	0.CCCE-39	0.0CCDE-39	0.0000E-39
RW(14)	-4.3907E 04	-3.0607E 04	0.00CCE-39	0.0000E-39	0.00OEE-39	0.00CCE-39	0.CCCE-39	0.0CCDE-39	0.0000E-39
RW(15)	-5.4393E 04	-3.2399E 04	0.00CCE-39	0.0000E-39	0.0UOE-39	0.00OEE-39	0.CCCE-39	0.0CCDE-39	0.0000E-39
RW(16)	0.0000E-39	-1.6518E 04	1.5303E 04	0.00CCE-39	0.0000E-39	0.00OEE-39	0.CCCE-39	0.0CCDE-39	0.0000E-39
RW(17)	0.0300E-39	-1.3866E 04	-1.5158E 04	0.00CCE-39	0.0000E-39	0.00OEE-39	0.CCCE-39	0.0CCDE-39	0.0000E-39
RW(18)	0.0100E-39	-1.7928E 04	-1.5344E 04	0.00CCE-39	0.0000E-39	0.00OEE-39	0.CCCE-39	0.0CCDE-39	0.0000E-39
RW(19)	0.0000E-39	7.0883E 03	1.4748E 04	0.00CCE-39	0.0000E-39	0.00OEE-39	0.CCCE-35	0.0CCDE-39	0.0000E-39
RW(20)	0.0000E-39	5.0000E-39	-6.1875E 03	-1.3652E 04	0.00CCE-39	0.CCCE-39	0.CCCE-39	0.0CCDE-39	0.0000E-39
RW(21)	0.0000E-39	5.0000E-39	-6.4475E 03	-1.1746E 04	0.00CCE-39	0.00OEE-39	0.CCCE-39	0.0CCDE-39	0.0000E-39
RW(22)	0.0000E-39	5.0000E-39	0.00CCE-39	0.0000E-39	-2.2200E 03	-1.6674E C3	0.00CCE-39	0.0CCDE-39	0.0000E-39
RW(23)	0.0000E-39	5.0000E-39	0.00CCE-39	0.0000E-39	-1.8649E 03	-2.0555E C3	C.CCCE-39	0.0CCDE-39	0.0000E-39
RW(24)	0.0000E-39	5.0000E-39	0.00CCE-39	0.0000E-39	-2.2238E 03	-1.8102E C3	C.CCCE-39	0.0CCDE-39	0.0000E-39
RW(25)	0.0000E-39	5.0000E-39	0.00CCE-39	0.0000E-39	0.00OEE-39	-3.1109E 04	-2.6842E 04	0.00CCE-39	0.0000E-39
RW(26)	0.0000E-39	5.0000E-39	0.00CCE-39	0.0000E-39	0.00OEE-39	-4.3807E 04	-3.0607E 04	0.00CCE-39	0.0000E-39
RW(27)	0.0000E-39	5.0000E-39	0.00CCE-39	0.0000E-39	0.00OEE-39	0.C00E-39	-5.4039E C4	-2.5599E 04	0.00CCE-39
RW(28)	0.0000E-39	5.0000E-39	0.00CCE-39	0.0000E-39	0.00OEE-39	0.CCCE-39	0.CCCE-39	-1.6518E 04	1.5303E 04
RW(29)	0.0000E-39	5.0000E-39	0.00CCE-39	0.0000E-39	0.00OEE-39	0.CCCE-39	0.CCCE-39	-1.3866E 04	1.4748E 04
RW(30)	0.0000E-39	5.0000E-39	0.00CCE-39	0.0000E-39	0.00OEE-39	0.CCCE-39	0.CCCE-39	-1.7928E 04	1.5344E 04
RW(31)	0.0000E-39	5.0000E-39	0.00CCE-39	0.0000E-39	0.00OEE-39	0.CCCE-39	0.CCCE-39	7.0883E 03	1.4748E 04
RW(32)	0.0000E-39	5.0000E-39	0.00CCE-39	0.0000E-39	0.00OEE-39	0.CCCE-35	0.0CCDE-39	-6.1875E 03	-1.3652E 04
RW(33)	0.0000E-39	5.0000E-39	0.00CCE-39	0.0000E-39	0.00OEE-39	0.CCCE-35	0.0CCDE-39	-6.4475E 03	-1.1746E 04
RW(34)	0.0000E-39	5.0000E-39	0.00CCE-39	0.0000E-39	0.00OEE-39	0.CCCE-39	0.0CCDE-39	0.0000E-39	0.0000E-39
RW(35)	0.0000E-39	5.0000E-39	0.00CCE-39	0.0000E-39	0.00OEE-39	0.CCCE-39	0.0CCDE-39	0.0000E-39	0.0000E-39
RW(36)	0.0000E-39	5.0000E-39	0.00CCE-39	0.0000E-39	0.00OEE-39	0.CCCE-39	0.0CCDE-39	0.0000E-39	0.0000E-39

COLUMN(11)	COLUMN(12)	COLUMN(13)	COLUMN(14)	COLUMN(15)	COLUMN(16)	COLUMN(17)	COLUMN(18)	COLUMN(19)	COLUMN(20)
RW(1)	0.0000E-39	0.0000E-39	-3.1109E 04	-4.3807E 04	-5.4039E C4	0.0000E-39	0.00CCE-39	0.0CCDE-39	0.00CCE-39
RW(2)	0.0000E-39	0.0000E-39	-2.6842E 04	-3.0607E 04	-4.2599E C4	1.6518E C4	-1.3866E 04	-1.7928E 04	0.00CCE-39
RW(3)	0.0000E-39	0.0000E-39	0.00CCE-39	0.0000E-39	0.00OEE-39	1.5303E C4	-1.5158E C4	-1.5344E 04	7.0883E 03
RW(4)	0.0000E-39	0.0000E-39	0.00CCE-39	0.0000E-39	0.00OEE-39	0.00CCE-39	C.CCCCE-35	0.0CCDE-39	1.4744E 04
RW(5)	0.0000E-39	0.0000E-39	0.00CCE-39	0.0000E-39	0.00OEE-39	0.00CCE-39	0.00CCE-39	0.00CCE-39	1.3652E 04
RW(6)	0.0000E-39	0.0000E-39	0.00CCE-39	0.0000E-39	0.00OEE-39	0.00CCE-39	0.00CCE-39	0.00CCE-39	0.0000E-39
RW(7)	0.0000E-39	0.0000E-39	0.00CCE-39	0.0000E-39	0.00OEE-39	0.00CCE-39	0.00CCE-39	0.00CCE-39	0.0000E-39
RW(8)	0.0000E-39	0.0000E-39	0.00CCE-39	0.0000E-39	0.00OEE-39	0.00CCE-39	0.00CCE-39	0.00CCE-39	0.0000E-39
RW(9)	0.0000E-39	0.0000E-39	0.00CCE-39	0.0000E-39	0.00OEE-39	0.00CCE-39	0.00CCE-39	0.00CCE-39	0.0000E-39
RW(10)	0.0000E-39	0.0000E-39	0.00CCE-39	0.0000E-39	0.00OEE-39	0.00CCE-39	0.00CCE-39	0.00CCE-39	0.0000E-39
RW(11)	4.9761E 02	1.0252E 03	0.00CCE-39	0.0000E-39	0.00OEE-39	0.00CCE-39	C.CCCE-39	0.0CCDE-39	0.0000E-39
RW(12)	1.0252E 02	0.9138E 03	0.00CCE-39	0.0000E-39	0.00OEE-39	0.00CCE-39	0.00CCE-39	0.00CCE-39	0.0000E-39
RW(13)	0.0000E-39	4.2356E 04	4.6435E 04	4.6435E 04	4.5792E C4	5.8792E 04	5.9682E C4	6.0962E 04	0.00CCE-39
RW(14)	0.0000E-39	4.705CE 04	4.705CE 04	4.705CE 04	4.705CE 04	4.705CE 04	4.705CE 04	4.705CE 04	0.00CCE-39
RW(15)	0.0000E-39	5.0000E-39	0.00CCE-39	0.0000E-39	0.00OEE-39	2.4038E C4	-2.2762E 04	-2.4840E 04	0.00CCE-39
RW(16)	0.0000E-39	5.0000E-39	0.00CCE-39	0.0000E-39	0.00OEE-39	0.00CCE-39	-2.2762E 04	-2.4840E 04	0.00CCE-39
RW(17)	0.0000E-39	5.0000E-39	0.00CCE-39	0.0000E-39	0.00OEE-39	0.00CCE-39	0.00CCE-39	0.00CCE-39	0.0000E-39
RW(18)	0.0000E-39	5.0000E-39	0.00CCE-39	0.0000E-39	0.00OEE-39	0.00CCE-39	0.00CCE-39	0.00CCE-39	0.0000E-39
RW(19)	0.0000E-39	5.0000E-39	0.00CCE-39	0.0000E-39	0.00OEE-39	0.00CCE-39	0.00CCE-39	0.00CCE-39	0.0000E-39
RW(20)	0.0000E-39	5.0000E-39	0.00CCE-39	0.0000E-39	0.00OEE-39	0.00CCE-39	0.00CCE-39	0.00CCE-39	0.0000E-39
RW(21)	0.0000E-39	5.0000E-39	0.00CCE-39	0.0000E-39	0.00OEE-39	0.00CCE-39	0.00CCE-39	0.00CCE-39	0.0000E-39
RW(22)	0.0000E-39	5.0000E-39	0.00CCE-39	0.0000E-39	0.00OEE-39	0.00CCE-39	0.00CCE-39	0.00CCE-39	0.0000E-39
RW(23)	0.0000E-39	5.0000E-39	0.00CCE-39	0.0000E-39	0.00OEE-39	0.00CCE-39	0.00CCE-39	0.00CCE-39	0.0000E-39
RW(24)	0.0000E-39	5.0000E-39	0.00CCE-39	0.0000E-39	0.00OEE-39	0.00CCE-39	0.00CCE-39	0.00CCE-39	0.0000E-39
RW(25)	0.0000E-39	5.0000E-39	0.00CCE-39	0.0000E-39	0.00OEE-39	0.00CCE-39	0.00CCE-39	0.00CCE-39	0.0000E-39
RW(26)	0.0000E-39	5.0000E-39	0.00CCE-39	0.0000E-39	0.00OEE-39	0.00CCE-39	0.00CCE-39	0.00CCE-39	0.0000E-39
RW(27)	0.0000E-39	5.0000E-39	0.00CCE-39	0.0000E-39	0.00OEE-39	0.00CCE-39	0.00CCE-39	0.00CCE-39	0.0000E-39
RW(28)	0.0000E-39	5.0000E-39	0.00CCE-39	0.0000E-39	0.00OEE-39	0.00CCE-39	0.00CCE-39	0.00CCE-39	0.0000E-39
RW(29)	0.0000E-39	5.0000E-39	0.00CCE-39	0.0000E-39	0.00OEE-39	0.00CCE-39	0.00CCE-39	0.00CCE-39	0.0000E-39
RW(30)	0.0000E-39	5.0000E-39	0.00CCE-39	0.0000E-39	0.00OEE-39	0.00CCE-39	0.00CCE-39	0.00CCE-39	0.0000E-39
RW(31)	0.0000E-39	5.0000E-39	0.00CCE-39	0.0000E-39	0.00OEE-39	0.00CCE-39	0.00CCE-39	0.00CCE-39	0.0000E-39
RW(32)	0.0000E-39	5.0000E-39	0.00CCE-39	0.0000E-39	0.00OEE-39	0.00CCE-39	0.00CCE-39	0.00CCE-39	0.0000E-39
RW(33)	0.0000E-39	5.0000E-39	0.00CCE-39	0.0000E-39	0.00OEE-39	0.00CCE-39	0.00CCE-39	0.00CCE-39	0.0000E-39
RW(34)	0.0000E-39	5.0000E-39	0.00CCE-39	0.0000E-39	0.00OEE-39	0.00CCE-39	0.00CCE-39	0.00CCE-39	0.0000E-39
RW(35)	0.0000E-39	5.0000E-39	0.00CCE-39	0.0000E-39	0.00OEE-39	0.00CCE-39	0.00CCE-39	0.00CCE-39	0.0000E-39
RW(36)	0.0000E-39	5.0000E-39	0.00CCE-39	0.0000E-39	0.00OEE-39	0.00CCE-39	0.00CCE-39	0.00CCE-39	0.0000E-39

COLUMN(21)	COLUMN(22)	COLUMN(23)	COLUMN(24)	COLUMN(25)	COLUMN(26)	COLUMN(27)	COLUMN(28)	COLUMN(29)	COLUMN(30)

<tbl_r cells="

RW(1)	0.0000E-39	0.3000E-39	0.000CE-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(2)	0.0000E-39	0.0000E-39	0.000CE-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(3)	0.0000E-39	0.0000E-39	0.000CE-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(4)	0.0000E-39	0.0000E-39	0.000CE-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(5)	0.0000E-39	0.0000E-39	0.000CE-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(6)	0.0000E-39	0.0000E-39	0.000CE-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(7)	0.0000E-39	0.0000E-39	0.000CE-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(8)	0.0000E-39	0.0000E-39	0.000CE-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(9)	0.0000E-39	0.0000E-39	0.000CE-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(10)	1.4748E-04	-1.3652E-04	-1.1746E-04	0.000CE-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(11)	0.0000E-39	0.0000E-39	0.000CE-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(12)	0.0000E-39	0.0000E-39	0.000CE-39	-1.6674E-03	-2.0555E-03	-1.8102E-03	-2.2233E-03	-2.2233E-03	-2.2233E-03
RW(13)	0.0000E-39	0.0000E-39	0.000CE-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(14)	0.0000E-39	0.0000E-39	0.000CE-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(15)	0.0000E-39	0.0000E-39	0.000CE-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(16)	0.0000E-39	0.0000E-39	0.000CE-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(17)	0.0000E-39	0.0000E-39	0.000CE-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(18)	0.0000E-39	0.0000E-39	0.000CE-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(19)	0.0000E-39	0.0000E-39	0.000CE-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(20)	0.0000E-39	0.0000E-39	0.000CE-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(21)	0.0000E-39	0.0000E-39	0.000CE-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(22)	0.0000E-39	0.0000E-39	0.000CE-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(23)	0.0000E-39	0.0000E-39	0.000CE-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(24)	0.0000E-39	0.0000E-39	0.000CE-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(25)	0.0000E-39	0.0000E-39	0.000CE-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(26)	0.0000E-39	0.0000E-39	0.000CE-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(27)	0.0000E-39	0.0000E-39	0.000CE-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(28)	0.0000E-39	0.0000E-39	0.000CE-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(29)	0.0000E-39	0.0000E-39	0.000CE-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(30)	0.0000E-39	0.0000E-39	0.000CE-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(31)	1.6583E-04	-1.5504E-04	-1.4344E-04	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(32)	1.5504E-04	1.5010E-04	1.3035E-04	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(33)	-1.4394E-04	1.3005E-04	1.4864E-04	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(34)	0.0000E-39	0.0000E-39	0.000CE-39	3.0095E-03	2.7751E-03	3.0244E-03	3.0244E-03	3.0244E-03	3.0244E-03
RW(35)	0.0000E-39	0.0000E-39	0.000CE-39	2.7751E-03	2.9768E-03	2.9117E-03	2.9117E-03	2.9117E-03	2.9117E-03
RW(36)	0.0000E-39	0.0000E-39	0.000CE-39	3.0244E-03	2.9117E-03	3.0782E-03	3.0782E-03	3.0782E-03	3.0782E-03

THE P.E. MATRIX, R FOLLOWS

	COLUMN(1)	COLUMN(2)	COLUMN(3)	COLUMN(4)	COLUMN(5)	COLUMN(6)	COLUMN(7)	COLUMN(8)	COLUMN(9)	COLUMN(10)
RW(1)	5.4718E-05	-1.0412E-10	5.4440E-09	0.000CE-39	0.0000E-39	-0.0000E-39	0.0000E-39	0.000CE-39	-0.000CE-39	0.0000E-39
RW(2)	-1.0912E-10	2.2301E-10	-1.3254E-10	1.8605E-09	0.0000E-39	-0.000CE-39	0.0000E-39	0.000CE-39	-0.000CE-39	0.0000E-39
RW(3)	5.4440E-09	-1.3254E-10	1.6082E-10	-8.2736E-09	-1.0408E-07	1.2226E-07	C.000CE-35	0.000CE-39	0.000CE-39	-0.000CE-39
RW(4)	0.0000E-39	1.8605E-09	-8.2736E-09	6.5478E-08	-1.2384E-08	-1.0852E-07	1.4492E-08	-1.4170E-07	1.2781E-07	C.000CE-39
RW(5)	0.0000E-39	0.0000E-39	-1.0408E-07	-1.2384E-08	1.4492E-08	-1.4170E-07	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(6)	-0.0000E-39	-0.0000E-39	-1.2242E-07	-1.0852E-07	-1.4170E-07	1.2781E-07	C.000CE-35	0.000CE-39	0.000CE-39	-0.000CE-39
RW(7)	0.0000E-39	0.0000E-39	0.000CE-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(8)	0.0000E-39	0.0000E-39	0.000CE-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(9)	0.0000E-39	0.0000E-39	0.000CE-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(10)	0.0000E-39	0.0000E-39	0.000CE-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(11)	0.0000E-39	0.0000E-39	0.000CE-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(12)	0.0000E-39	0.0000E-39	0.000CE-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(13)	-0.0000E-39	1.2139E-11	-5.0545E-10	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(14)	-3.4151E-10	6.8170E-10	-13.3953E-10	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(15)	-9.1262E-09	1.4119E-09	-9.0731E-09	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(16)	1.1453E-09	-2.1170E-09	3.9784E-09	5.7393E-09	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(17)	-9.1565E-09	1.3540E-09	1.1851E-09	-1.6236E-09	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(18)	7.0131E-09	3.8630E-09	-11.3231E-09	5.2670E-09	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(19)	3.0000E-09	2.8745E-09	-11.2735E-09	9.8623E-09	-16.1464E-07	2.4293E-07	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(20)	0.0000E-39	-2.0154E-09	8.8565E-09	-6.8307E-09	3.85110E-09	-9.5525E-09	C.000CE-39	0.000CE-39	0.000CE-39	0.0000E-39
RW(21)	1.0000E-09	-3.0763E-09	3.7177E-09	-10.2875E-09	1.39171E-09	-7.15619E-09	C.000CE-35	0.000CE-39	0.000CE-39	0.0000E-39
RW(22)	0.0000E-39	0.0000E-39	5.3232E-07	4.7191E-07	6.16171E-07	-5.55756E-07	C.000CE-35	0.000CE-39	0.000CE-39	0.0000E-39
RW(23)	0.0000E-39	0.0000E-39	-2.6575E-07	2.3562E-07	3.0764E-07	-2.7748E-07	C.000CE-35	0.000CE-39	0.000CE-39	0.0000E-39
RW(24)	0.0000E-39	0.0000E-39	-3.4871E-07	3.8893E-07	5.07871E-07	-4.5803E-07	C.000CE-35	0.000CE-39	0.000CE-39	0.0000E-39
RW(25)	0.0000E-39	0.0000E-39	0.000CE-39	0.0000E-39	0.0000E-39	-3.5929E-07	1.0539E-09	-5.5929E-07	1.1153E-11	-5.5604E-10
RW(26)	0.0000E-39	0.0000E-39	0.000CE-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(27)	0.0000E-39	0.0000E-39	0.000CE-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(28)	0.0000E-39	0.0000E-39	0.000CE-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(29)	0.0000E-39	0.0000E-39	0.000CE-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(30)	0.0000E-39	0.0000E-39	0.000CE-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(31)	0.0000E-39	0.0000E-39	0.000CE-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(32)	0.0000E-39	0.0000E-39	0.000CE-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(33)	0.0000E-39	0.0000E-39	0.000CE-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(34)	-0.0000E-39	0.0000E-39	-0.000CE-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	-5.3232E-07	4.7191E-07
RW(35)	-0.0000E-39	-0.000CE-39	-0.000CE-39	-0.0000E-39	-0.0000E-39					

RW(16)	-1.1973E-08	-0.0039E-39	-5.5394E-09	0.0000E-39	0.0000E-39	1.0000E-00	-0.0000E-39	-3.1243E-08	-0.0000E-39	1.2694E-09
RW(17)	-0.0000E-39	-1.0217E-09	-0.0000E-39	3.0759E-09	1.7300E-08	-0.0000E-39	1.0000E-00	-3.3481E-09	-0.0000E-39	-6.2155E-09
RW(18)	-5.5722E-09	-0.0000E-39	-6.4257E-09	0.0000E-39	0.0000E-39	-3.1243E-08	-0.0000E-39	1.0000E-00	-0.0000E-39	-6.2155E-09
RW(19)	-0.0000E-39	6.1634E-09	-0.0000E-39	1.5250E-08	7.4907E-10	-0.0000E-39	-3.3481E-09	-0.0000E-39	1.0000E-00	-0.0000E-39
RW(20)	-1.0H15E-08	-0.0000E-39	8.0081E-10	0.0000E-39	0.0000E-39	1.2694E-09	-0.0000E-39	1.2694E-09	-0.0000E-39	1.0000E-00
RW(21)	3.6166E-05	-0.0000E-39	8.1485E-09	0.0000E-39	0.0000E-39	-1.1742E-08	-0.0000E-39	1.71C0E-09	-0.0000E-39	1.0318E-09
RW(22)	0.0000E-19	8.5007E-09	0.0000E-39	6.6826E-09	-6.0753E-09	0.0000E-39	-7.8112E-10	-0.0000E-39	1.4329E-08	-0.0000E-39
RW(23)	-3.4316E-08	-0.0000E-39	9.7645E-09	0.0000E-39	0.0000E-39	-7.8112E-10	-0.0000E-39	1.4329E-08	-0.0000E-39	5.8989E-09
RW(24)	-0.0000E-39	4.4164E-09	-0.0000E-39	-7.0182E-09	1.3127E-08	-0.0000E-39	1.8835E-09	-0.0000E-39	-1.3221E-08	-0.0000E-39
RW(25)	6.4165E-08	-0.0000E-39	1.4629E-08	0.0000E-39	0.0000E-39	6.4591E-09	-0.0000E-39	1.0111E-08	-0.0000E-39	1.6384E-08
RW(26)	0.0000E-39	-2.1878E-08	0.0000E-39	1.2969E-08	2.4174E-09	0.0000E-39	1.0000E-09	0.0000E-39	2.6411E-08	0.0000E-39
RW(27)	-0.0000E-39	3.3674E-08	-0.0000E-39	-5.7573E-10	-1.1340E-08	-0.0000E-39	-8.5504E-09	-0.0000E-39	-1.2193E-08	-0.0000E-39
RW(28)	-1.7678E-07	-0.0000E-39	1.7543E-09	0.0000E-39	0.0000E-39	1.7140E-09	-0.0000E-39	-1.0146E-08	-0.0000E-39	-8.6728E-09
RW(29)	-0.0000E-39	2.4438E-07	-0.0000E-39	2.3626E-08	-7.7108E-08	-0.0000E-39	1.1043E-09	-0.0000E-39	-5.4703E-09	-0.0000E-39
RW(30)	1.2441E-06	-0.0000E-39	-1.6677E-08	0.0000E-39	0.0000E-39	4.3447E-08	-0.0000E-39	3.0393E-09	-0.0000E-39	-2.1331E-09
RW(31)	-1.6615E-06	-0.0300E-39	2.8192E-08	0.0000E-39	0.0000E-39	-5.3753E-08	-0.0000E-39	3.4731E-10	-0.0000E-39	9.9188E-10
RW(32)	0.0000E-39	-3.3400E-07	0.0000E-39	-3.0087E-09	1.0516E-09	-0.0000E-39	4.4636E-09	0.0000E-39	2.6921E-09	0.0000E-39
RW(33)	0.0000E-39	1.7309E-08	0.0000E-39	-3.1963E-10	-5.6139E-09	0.0000E-39	5.6183E-10	0.0000E-39	-2.3359E-09	0.0000E-39
RW(34)	2.5641E-07	-0.0J00E-39	-5.0819E-09	0.0000E-39	0.0000E-39	8.0519E-09	-0.0000E-39	3.6335E-09	-0.0000E-39	2.5461E-09
RW(35)	3.0000E-39	-5.0J01E-08	0.0000E-39	-4.4498E-09	1.7618E-08	0.0000E-39	1.2020E-09	0.0000E-39	1.6754E-09	0.0000E-39
RW(36)	1.5326E-08	-0.0u00E-39	-1.8533E-09	0.0000E-39	0.0000E-39	5.8262E-10	-0.0000E-39	4.6450E-10	-0.0000E-39	-1.7675E-09

COLUMN(21)	COLUMN(22)	COLUMN(23)	COLUMN(24)	COLUMN(25)	COLUMN(26)	COLUMN(27)	COLUMN(28)	COLUMN(29)	COLUMN(30)	
RW(1)	0.0000E-39	5.7847E-08	-0.0000E-39	8.9144E-09	0.0000E-39	-1.6102E-08	-2.1229E-08	0.0000E-39	7.4568E-09	0.0000E-39
RW(2)	-1.0574E-08	0.0000E-34	3.5458E-09	-0.0000E-39	-1.6522E-10	0.0000E-39	3.0000E-39	-0.0000E-39	1.2375E-09	
RW(3)	-1.0-0000E-35	5.0715E-04	-0.0000E-39	6.0815E-05	-0.0000E-39	-1.6238E-04	-2.2243E-04	-0.0000E-39	7.3611E-05	-0.0000E-39
RW(4)	4.6512E-04	0.0000E-39	-5.5742E-05	-0.0000E-39	-1.6730E-04	0.0000E-39	-2.0420E-04	-0.0000E-39	-6.7521E-05	
RW(5)	0.0000E-39	-3.2668E-05	0.0000E-39	-6.1894E-06	0.0000E-39	4.0044E-06	-2.5462E-05	0.0000E-39	1.4982E-05	0.0000E-39
RW(6)	2.9236E-05	0.0000E-39	-5.5359E-06	-0.0000E-39	-3.5887E-05	0.0000E-39	-2.2752E-05	-0.0000E-39	1.3415E-05	
RW(7)	1.5631E-07	0.0000E-39	2.5514E-07	-0.0000E-39	6.5545E-07	0.0000E-39	-1.7441E-07	-0.0000E-39	-3.1602E-07	
RW(8)	-0.0000E-35	-1.6167E-07	0.0000E-39	2.5791E-07	0.0000E-39	-6.6343E-07	1.7941E-07	0.0000E-39	-3.1909E-07	0.0000E-39
RW(9)	1.2766E-07	0.0000E-39	1.2103E-05	-0.0000E-39	-1.5357E-05	0.0000E-39	1.2000E-05	0.0000E-39	4.7436E-05	-0.0000E-39
RW(10)	-0.0000E-39	1.1999E-07	-0.0000E-39	-1.0110E-07	-0.0000E-39	-1.3610E-05	4.1995E-05	0.0000E-39	2.9225E-04	-0.0000E-39
RW(11)	3.6366E-05	0.0000E-39	-3.4313E-08	-0.0000E-39	6.4365E-08	0.0000E-39	3.0000E-39	-0.0000E-39	1.2441E-06	
RW(12)	-0.0300E-39	-8.5837E-09	4.4164E-09	-0.0000E-39	-2.1876E-08	3.3674E-08	-0.0000E-39	2.4438E-07	-0.0000E-39	
RW(13)	8.1485E-05	0.0000E-39	9.7645E-09	-0.0000E-39	1.4629E-08	0.0000E-39	-0.0000E-39	1.5743E-09	-0.0000E-39	1.6877E-08
RW(14)	0.0000E-39	6.6826E-09	0.0000E-39	-7.0182E-09	0.0000E-39	-1.2596E-08	5.5757E-10	0.0000E-39	2.3626E-08	0.0000E-39
RW(15)	0.0000E-39	-6.0753E-09	0.0000E-39	1.3127E-08	0.0000E-39	2.4174E-09	1.1340E-08	0.0000E-39	-7.7108E-08	0.0000E-39
RW(16)	-1.1742E-08	0.0000E-39	-7.8112E-10	-0.0000E-39	6.4991E-09	0.0000E-39	0.0000E-39	1.7140E-09	-0.0000E-39	4.3447E-08
RW(17)	-0.0000E-35	2.8681E-09	-0.0000E-39	1.8835E-09	-0.0000E-39	4.9108E-09	8.5504E-09	-0.0000E-39	1.1043E-08	-0.0000E-39
RW(18)	1.7100E-05	0.0000E-39	-1.4325E-08	-0.0000E-39	-1.0111E-08	0.0000E-39	-1.0166E-08	-0.0000E-39	-3.9533E-09	
RW(19)	-0.0000E-39	-7.8724E-09	-0.0000E-39	-1.3221E-08	-0.0000E-39	2.6411E-08	-1.2193E-08	-0.0000E-39	-5.4703E-09	-0.0000E-39
RW(20)	1.0318E-05	0.0000E-39	5.8958E-09	-0.0000E-39	1.6384E-18	0.0000E-39	-0.0000E-39	-8.6728E-09	-0.0000E-39	-2.1331E-09
RW(21)	1.0300E-0C	0.0000E-39	-1.4447E-08	-0.0000E-39	2.2651E-08	0.0000E-39	-0.0000E-39	1.4540E-08	-0.0000E-39	-8.8375E-10
RW(22)	0.0000E-35	1.0000E-00	0.0000E-39	-2.3859E-09	0.0000E-39	-1.6183E-08	0.0000E-39	-0.0000E-39	1.0332E-08	-0.0000E-39
RW(23)	-1.4407E-08	0.0000E-39	1.0000E-00	-0.0000E-39	-1.6183E-08	0.0000E-39	-0.0000E-39	-3.5335E-10	5.1040E-05	-0.0000E-39
RW(24)	-0.0000E-35	-2.3859E-09	-0.0000E-39	1.0000E-00	0.0000E-39	-2.0572E-08	0.0000E-39	-0.0000E-39	-1.5235E-08	-0.0000E-39
RW(25)	2.2651E-08	0.0000E-39	-1.6183E-08	-0.0000E-39	1.0000E-00	0.0000E-39	-0.0000E-39	-1.5235E-08	-0.0000E-39	-1.900CE-08
RW(26)	0.0000E-35	-2.5792E-08	0.0000E-39	-3.5335E-10	0.0000E-39	1.0000E-00	-0.0000E-39	-1.5235E-08	-0.0000E-39	-7.8357E-09
RW(27)	-0.0000E-35	1.0474E-08	-0.0000E-39	5.0104E-09	-0.0000E-39	-1.5234E-08	0.0000E-39	-1.5234E-08	0.0000E-39	2.0057E-09
RW(28)	1.45560E-08	0.0000E-39	1.0332E-08	-0.0000E-39	-1.5234E-08	0.0000E-39	-0.0000E-39	1.4977E-08	-0.0000E-39	-1.9795E-08
RW(29)	-7.0700E-05	-5.6292E-09	0.0000E-39	-1.900CE-08	-1.5234E-08	0.0000E-39	-0.0000E-39	2.0572E-09	1.4970E-08	-0.0000E-39
RW(30)	-8.8375E-10	0.0000E-39	-2.3724E-08	-0.0000E-39	-7.8357E-09	0.0000E-39	-0.0000E-39	1.0000E-00	0.0000E-39	-1.000CE-00
RW(31)	-2.5536E-05	0.0000E-39	-4.0332E-09	-0.0000E-39	-1.7635E-08	0.0000E-39	-0.0000E-39	-2.4256E-08	-0.0000E-39	-3.0044E-08
RW(32)	0.0000E-39	-2.0510E-09	0.0000E-39	-1.7536E-09	0.0000E-39	-3.7846E-09	8.0000E-39	-0.0000E-39	2.160EE-08	0.0000E-39
RW(33)	0.0000E-39	-2.4718E-09	0.0000E-39	-1.3132E-08	0.0000E-39	-1.3132E-08	0.0000E-39	-0.0000E-39	3.6431E-08	-0.0000E-39
RW(34)	8.3556E-05	0.0000E-39	1.1C36E-09	-0.0000E-39	-6.1322E-09	0.0000E-39	-0.0000E-39	-3.1918E-08	0.0000E-39	-5.117EE-08
RW(35)	0.0000E-39	4.3578E-09	0.0000E-39	-6.6509E-09	0.0000E-39	-1.2699E-08	0.0000E-39	-0.0000E-39	4.836CE-08	0.0000E-39
RW(36)	-8.7956E-1C	0.0000E-39	3.8206E-09	-0.0000E-39	-8.9920E-08	0.0000E-39	-0.0000E-39	1.0954E-07	-0.0000E-39	-1.312EE-09

COLUMN(31)	COLUMN(32)	COLUMN(33)	COLUMN(34)	COLUMN(35)	COLUMN(36)	COLUMN(37)
RW(1)	0.0000E-39	2.320CE-09	-3.9682E-09	0.0000E-39	1.0337E-08	0.0000E-39
RW(2)	1.6489E-09	0.0000E-39	0.0CCCCE-39	-4.4391E-09	0.0000E-39	-3.1564E-11
RW(3)	-0.0000E-35	2.3614E-05	-0.5598E-05	-0.0000E-39	7.740CE-05	-0.0000E-39
RW(4)	-2.1663E-05	0.0000E-39	0.0CCCCE-39	7.4622E-05	0.0000E-39	4.7521E-06
RW(5)	0.0000E-39	7.3611E-06	-2.4424E-06	-0.0000E-39	7.2651E-06	0.0000E-39
RW(6)	6.5903E-06	0.0000E-39	0.0CCCCE-39	-6.8365E-06	-0.0000E-39	4.3555E-07
RW(7)	-1.8431E-07	0.0000E-39	1.0000E-09	1.5300E-07	0.0000E-39	7.1701E-09
RW(8)	0.0000E-39	-1.8715E-07	3.701CE-08	0.0000E-39	-1.1176E-07	0.0000E-39
RW(9)	4.3843E-04	0.0000E-39	0.0000E-39	-6.7422E-05	0.0000E-39	-4.2967E-06
RW(10)	-0.0000E-39	-3.8818E-04	1.8767E-05	-0.0000E-39	-5.6793E-05	-0.0000E-39
RW(11)	-1.6615E-06	0.0000E-39	0.0000E-39	2.5641E-07	0.0000E-39	1.5324E-08
RW(12)	-0.0000E-35	-3.3490E-07	1.73C9E-08	-0.0000E-39	-5.0001E-08	-0.0000E-39
RW(13)	2.8192E-08	0.0000E-39	0.0000E-39	-5.0810E-09	0.0000E-39	1.8533E-09
RW(14)	0.0000E-39	-3.0807E-08	-1.9193E-10	0.0000E-39	-4.4498E-09	0.0000E-39
RW(15)	0.0000E-39	1.0516E-07	-5.6135E-07	0.0000E-39	1.7618E-08	0.0000E-39
RW(16)	-5.3753E-08	0.0000E-39	0.0000E-39	8.0519E-09	0.0000E-39	5.8262E-10
RW(17)	-0.0000E-39	-4.4636E-09	-5.6135E-10	-0.0000E-39	-1.202CE-09	-0.0000E-39
RW(18)	-3.4731E-1C	0.0000E-39	0.0000E-39	3.6335E-09	0.0000E-39	4.6450E-

P(-1) B P(-1) = F (PP=0)

	COLUMN(1)	COLUMN(2)	COLUMN(3)	COLUMN(4)	COLUMN(5)	COLUMN(6)	COLUMN(7)	COLUMN(8)	COLUMN(9)	COLUMN(10)
RW(1)	8.5279E 04	-2.1895E 05	1.994E 05	-4.9138E 04	0.0000E-39	-0.0C00E-39	C.CCCCE-35	0.0C00E-39	0.00CCE-39	0.0000E-39
RW(2)	-2.1895E 05	5.7240E 05	-5.8536E 05	2.0932E 05	0.0000E-39	-0.0C00E-39	C.CCCCE-39	0.0C00E-39	0.00CCE-39	0.0000E-39
RW(3)	1.994E 05	-5.8536E 05	9.9085E 05	-7.1041E 05	-1.0464E 05	C.3761E C3	0.CCCCE-39	0.0C00E-39	0.0000E-39	0.0000E-39
RW(4)	-4.9138E 04	2.0932E 05	-7.1041E 05	7.1332E 05	-1.3860E 04	2.2722E C3	C.CCCCE-39	0.0C00E-39	0.0000E-39	0.0000E-39
RW(5)	0.0000E-39	0.0000E-39	-1.0464E 03	-1.3860E 04	2.9927E 04	-1.5409E C4	0.C000E-39	0.0C00E-39	0.0000E-39	0.0000E-39
RW(6)	-0.0C00E-39	-0.0000E-39	2.3761E 03	2.2722E 03	-1.5409E 04	1.4648E C4	-C.CCCCE-35	-0.0C00E-39	-C.00CCE-39	-0.0000E-39
RW(7)	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	-0.0C00E-39	9.3807E 04	-2.4085E 05	2.194CE 05	-5.4052E 04
RW(8)	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	-0.0C00E-39	2.4085E 05	6.2946E 05	-6.4385E 05	2.3025E 05
RW(9)	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	-0.0C00E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(10)	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	-0.0C00E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(11)	-0.0C00E-39	-0.0000E-39	-0.0000E-39	-0.0000E-39	-0.0000E-39	-0.0C00E-39	-0.0000E-39	-0.0000E-39	-0.0000E-39	-0.0000E-39
RW(12)	0.0000E-39									
RW(13)	-1.4189E 06	3.6591E 06	-3.4343E 06	9.4921E 05	-2.8379E 02	-2.1729E C2	C.CCCCE-35	0.0C00E-39	0.00CCE-39	-0.0000E-39
RW(14)	1.7751E 05	-4.5528E 06	4.1182E 06	-9.8439E 06	-8.2608E 01	-6.3415E C1	C.00CCE-39	0.00CCE-39	0.0000E-39	0.0000E-39
RW(15)	-1.3078E 06	3.3555E 06	-3.0425E 06	7.3509E 05	3.9718E C1	3.0463E C1	C.00CCE-39	0.00CCE-39	0.0000E-39	0.0000E-39
RW(16)	5.8686E 05	-3.1688E 06	3.8223E 06	7.8806E 05	-1.9153E C3	-1.4690E C3	C.00CCE-39	0.00CCE-39	0.0000E-39	0.0000E-39
RW(17)	5.8656E 05	-2.1257E 06	5.8113E 06	-5.3795E 06	6.4883E C2	4.9765E C2	C.CCCCE-35	0.0C00E-39	0.00CCE-39	-0.0000E-39
RW(18)	-2.2141E 06	5.4545E 06	-2.4547E 06	-1.9562E 06	-2.7605E 02	-2.1173E C2	C.00CCE-39	0.00CCE-39	0.0000E-39	0.0000E-39
RW(19)	-1.0224E 05	5.1609E 05	-1.9831E 06	2.0194E 06	2.3577E 04	6.1782E C3	C.00CCE-39	0.00CCE-39	0.0000E-39	0.0000E-39
RW(20)	-5.2661E 04	3.5499E 05	-1.7511E 06	1.8839E 06	4.7129E 04	-9.4750E C4	C.CCCCE-35	0.0C00E-39	0.00CCE-39	-0.0000E-39
RW(21)	-4.8465E 05	-3.5414E 05	3.2987E 05	-8.3850E 03	4.0232E 04	-5.1732E C4	C.00CCE-39	0.00CCE-39	0.0000E-39	0.0000E-39
RW(22)	0.0000E-39	0.0000E-39	-9.5000E 03	2.8987E 03	4.0047E 04	-5.0224E C4	C.00CCE-35	0.0C00E-39	0.00CCE-39	-0.0000E-39
RW(23)	0.0000E-39	0.0000E-39	6.2563E 03	-8.7040E 03	-2.3671E 04	3.9336E C4	C.00CCE-35	0.00CCE-39	0.0000E-39	0.0000E-39
RW(24)	0.0000E-39	0.0000E-39	1.0533E 04	-2.9136E 04	2.2388E 03	3.7636E C4	C.00CCE-39	0.00CCE-39	0.0000E-39	-0.0000E-39
RW(25)	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	-0.0C00E-39	3.5607E 06	4.0250E 06	-3.7777E 06	1.0441E 06
RW(26)	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	1.9526E 06	-6.5008E 06	4.5259E 06	-1.0828E 06
RW(27)	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	-1.4386E 06	3.6910E 06	-3.3466E 06	8.086CE 05	0.0000E-39
RW(28)	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	4.5505E 06	-5.1502E 06	4.2061E 05	8.6660E 05
RW(29)	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	5.2332E 06	6.3924E 06	-5.9174E 06	0.0000E-39
RW(30)	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	6.5096E 06	-6.000CE 06	-2.7001E 06	-2.1519E 06
RW(31)	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	1.2476E 05	5.5769E 05	-2.1815E 06	2.2237E 06
RW(32)	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	1.1247E 05	-2.1782E 03	9.4750E 04	0.0000E-39
RW(33)	0.0990E-35	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	-0.0C00E-39	3.5331E 04	-3.8952E 05	3.6295E 06	-4.2387E 06
RW(34)	-0.0000E-35	0.0000E-39	-0.0000E-39	-0.0000E-39	-0.0000E-39	0.0000E-39	-0.0C00E-39	-9.5000E 03	2.8987E 03	0.0000E-39
RW(35)	-0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	8.2563E 03	-8.7040E 03	0.0000E-39
RW(36)	-0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	-0.0C00E-39	1.0536E 04	-2.9136E 04	0.0000E-39

	COLUMN(11)	COLUMN(12)	COLUMN(13)	COLUMN(14)	COLUMN(15)	COLUMN(16)	COLUMN(17)	COLUMN(18)	COLUMN(19)	COLUMN(20)
RW(1)	-0.0300E-35	0.0000E-39	-1.4185E 06	1.7751E 06	-1.3078E 06	5.8686E C5	5.8606E 05	-2.2814E 06	-1.0224E 05	-5.2661E 04
RW(2)	-0.0000E-39	0.0000E-39	3.6591E 06	-4.5528E 06	3.3554E 06	-1.3684E 06	-2.1257E 06	5.4545E 06	5.0699E 05	3.5993E 05
RW(3)	-0.0000E-39	0.0000E-39	-3.4343E 06	4.1180E 06	5.04245E 06	5.8232E C5	5.8113E 05	-2.4547E 06	-1.9831E 06	-1.7511E 06
RW(4)	-0.0000E-39	0.0000E-39	9.4921E 05	-9.8439E 05	7.3509E 05	7.8806E 05	-1.9526E 06	-1.9522E 06	2.0194E 06	1.8839E 06
RW(5)	-0.0000E-35	0.0000E-39	0.0000E-39	-2.8325E 02	-8.2608E 01	3.9718E C1	-1.9153E C3	6.4883E 02	-2.7652E 02	2.3577E 04
RW(6)	0.0100E-35	-0.0000E-39	-2.1725E 02	-6.3415E 01	3.0463E C1	-1.4690E 03	4.9765E 02	-2.1173E 02	6.1782E 03	-9.4750E 04
RW(7)	-0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	-0.0C00E-39	3.05607E 06	4.0250E 06	-3.7777E 06	1.0441E 06
RW(8)	-0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	1.9526E 06	-6.5008E 06	4.5259E 06	-1.0828E 06
RW(9)	-1.0464E 03	2.3761E 03	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	1.4386E 06	-1.4386E 06	2.0194E 06	1.8839E 06
RW(10)	-1.3860E 04	2.4722E 03	-0.0000E-39	-0.0000E-39	-0.0000E-39	-0.0000E-39	1.7195E 07	-1.7195E 07	2.1783E 07	-9.4750E 04
RW(11)	2.9927E 04	-1.5409E 04	0.0000E-39	-0.0000E-39	-0.0000E-39	-0.0000E-39	-1.5409E 04	-1.5409E 04	-1.5409E 04	-0.0000E-39
RW(12)	-1.5409E 04	1.4648E 04	0.0000E-39	-0.0000E-39	-0.0000E-39	-0.0000E-39	3.2356E 07	-2.9565E 07	2.1783E 07	-9.5482E 06
RW(13)	-0.0000E-39	0.0000E-39	2.3659E 07	-2.9565E 07	-2.1783E 07	-9.5482E 06	-1.7132E C6	-1.7132E C6	-1.7132E C6	-1.7132E C6
RW(14)	-0.0000E-35	0.0000E-39	-2.9565E 07	3.7027E 07	1.2281E 07	1.2281E 07	1.9153E 07	-4.7272E 07	-2.0155E 06	-9.9162E 05
RW(15)	0.0000E-35	0.0000E-39	2.1783E 07	-2.7281E 07	2.0241E 07	2.0241E 07	-1.0269E 06	8.4740E 06	3.5375E 07	1.5141E 06
RW(16)	-0.0000E-35	0.0000E-39	-9.5482E 06	1.2281E 07	-9.0269E 06	5.9130E 06	-4.3561E 06	2.1144E 06	2.5922E 06	2.6971E 06
RW(17)	-0.0000E-35	0.0000E-39	-1.0733E 07	1.9153E 07	-8.8470E 06	6.43561E 06	4.1768E 07	8.8159E 06	-1.5528E 07	-1.3996E 07
RW(18)	0.0000E-35	0.0000E-39	3.7322E 07	-6.7674E 07	3.5075E 07	-2.1144E 07	8.8158E 06	7.68823E 06	7.68823E 06	6.0443E 06
RW(19)	-0.0000E-35	0.0000E-39	-9.1732E 04	2.0858E 06	-2.0159E 06	1.5141E 06	2.5293E 06	-6.15528E 06	6.0443E 06	5.2789E 06
RW(20)	-2.7605E 04	-2.1173E 02	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	9.9162E 05	-2.7289E 05	6.0346E 06	0.0000E-39
RW(21)	-0.0000E-35	0.0000E-39	-2.2222E 03	-1.2442E 03	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(22)	-0.0000E-35	0.0000E-39	-2.1222E 03	-1.2442E 03	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(23)	-4.2322E 04	-4.0427E 04	2.3671E 04	-2.2388E 03	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39	0.0000E-39
RW(24)	-6.5132E 04	-5.4224E 04	3.9336E 04	-3.7636E 04	0.0000E-39	-0.0000E-39	-0.0000E-39	-0.0000E-39	-0.0000E-39	-0.0000E-39
RW(25)	0.0000E-39	-0.0000E-39	3.7636E 04	-3.7636E 04	0.0000E-39	-0.0000E-39	-0.0000E-39	-0.0000E-39	-0.0000E-39	-0.0000E-39
RW(26)	0.0000E-39	-0.0000E-39	3.7636E 04	-3.7636E 04	0.0000E-39	-0.0000E-39	-0.0000E-39	-0.0000E-39	-0.0000E-39	-0.0000E-39
RW(27)	0.0000E-39	-0.0000E-39	3.7636E 04	-3.7636E 04	0.0000E-39	-0.0000E-39	-0.0000E-39	-0.0000E-39	-0.0000E-39	-0.0000E-39
RW(28)	0.0000E-39	-0.0000E-39	3.7636E 04	-3.7636E 04	0.0000E-39	-0.0000E-39	-0.0000E-39	-0.0000E-39	-0.0000E-39	-0.0000E-39
RW(29)	0.0000E-39	-0.0000E-39	3.7636E 04	-3.7636E 04	0.0000E-39	-0.0000E-39	-0.0000E-39	-0.00		

```

RW( 1) = 0.0300E-39 0.0000E-39 0.0000E-39 -0.0000E-39 -0.0000E-39
RW( 2) = 0.0300E-39 0.0000E-39 0.0000E-39 -0.0000E-39 -0.0000E-39
RW( 3) = 0.0000E-39 0.0000E-39 0.0000E-39 -0.0000E-39 -0.0000E-39
RW( 4) = 0.0000E-39 0.0000E-39 0.0000E-39 -0.0000E-39 -0.0000E-39
RW( 5) = 0.0000E-39 0.0000E-39 0.0000E-39 -0.0000E-39 -0.0000E-39
RW( 6) = -0.0000E-39 -0.0000E-39 -0.0000E-39 0.0000E-39 0.0000E-39
RW( 7) = -1.1247E 05 -5.7927E 04 -5.3311E 04 -0.0000E-39 -0.0000E-39
RW( 8) = 5.5768E 05 3.9592E 05 -3.8952E 05 -0.0000E-39 -0.0000E-39
RW( 9) = -2.1819E 06 -1.9241E 06 3.6255E 06 -9.5008E 03 8.2563E C3
RW(10) = 2.2237E 06 2.0693E 06 -4.2387E 06 2.8987E 03 -8.7040E C3 -2.9136E C4
RW(11) = 2.3577E 04 4.7129E 04 4.0232E 04 4.0047E 04 -2.3671E C4 2.2386E C3
RW(12) = 6.1782E 03 -9.4750E 04 -5.1732E 04 -5.0224E 04 3.9336E 04 3.7633E C4
RW(13) = 0.6000E-35 0.0000E-39 0.0000E-39 -0.0000E-39 -0.0000E-39 -0.0000E-39
RW(14) = 0.0000E-39 0.0000E-39 0.0000E-39 -0.0000E-39 -0.0000E-39 -0.0000E-39
RW(15) = 0.0000E-39 0.0000E-39 0.0000E-39 -0.0000E-39 -0.0000E-39 -0.0000E-39
RW(16) = 0.0000E-35 0.0000E-39 0.0000E-39 -0.0000E-39 -0.0000E-39 -0.0000E-39
RW(17) = 0.0000E-35 0.0000E-39 0.0000E-39 -0.0000E-39 -0.0000E-39 -0.0000E-39
RW(18) = 0.0000E-39 0.0000E-39 0.0000E-39 -0.0000E-39 -0.0000E-39 -0.0000E-39
RW(19) = 0.0000E-35 0.0000E-39 0.0000E-39 -0.0000E-39 -0.0000E-39 -0.0000E-39
RW(20) = 0.0000E-35 0.0000E-39 0.0000E-39 -0.0000E-39 -0.0000E-39 -0.0000E-39
RW(21) = 0.0000E-39 0.0000E-39 0.0000E-39 -0.0000E-39 -0.0000E-39 -0.0000E-39
RW(22) = 0.0000E-35 0.0000E-39 0.0000E-39 -0.0000E-39 -0.0000E-39 -0.0000E-39
RW(23) = 0.0000E-35 0.0000E-39 0.0000E-39 -0.0000E-39 -0.0000E-39 -0.0000E-39
RW(24) = 0.0000E-35 0.0000E-39 0.0000E-39 -0.0000E-39 -0.0000E-39 -0.0000E-39
RW(25) = 2.2945E 06 1.3573E 06 5.7328E 04 1.2220E 03 -1.2442E C3 -2.1190E C3
RW(26) = -2.2175E 06 -1.0909E 06 -1.3518E 06 3.5664E 02 -3.6313E 02 -6.1844E C2
RW(27) = 1.6655E 06 8.3319E 05 9.3356E 05 -1.7132E 02 1.7444E C2 2.5709E C2
RW(28) = 2.8522E 06 2.9645E 06 -7.4658E 06 8.2617E 03 -8.4119E 03 -1.4326E C4
RW(29) = -1.7080E 07 -1.5395E 07 3.1536E 07 -2.7988E 03 2.8496E 03 4.8532E C3
RW(30) = -7.5704E 07 -8.1706E 06 2.2135E 07 1.1908E 03 -1.2124E 03 -2.6648E C3
RW(31) = 6.6400E 06 5.8216E 06 -1.2539E 07 -4.9211E 04 5.5414E 04 1.0758E C5
RW(32) = 5.8216E 06 6.5309E 06 -1.0972E 07 3.7382E 05 -3.2226E 05 -4.0364E C5
RW(33) = -1.2539E 07 -1.0972E 07 2.4964E 07 1.9059E 05 -1.5723E 05 -1.7617E 05
RW(34) = -4.9211E 04 3.7382E 05 1.9059E 05 1.9014E 05 -1.5774E 05 -1.7890E 05
RW(35) = 5.5414E 04 -3.2226E 05 -1.5723E 05 -1.5774E 05 1.8999E .5 2.2134E C4
RW(36) = 1.0758E 05 -4.0364E 05 -1.7617E 05 -1.7890E 05 2.2134E 04 9.1511E C5

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TIME CHECK FOR EIGENVALUE SOLUTION

TIME IN 200057

TIME BUT 200114

ELAPSED TIME 17 SECONDS

EIGENVALUES OF F MATRIX

```

DW( 1) = 0.17202952750346940 09
DW( 2) = 0.15713255246862680 09
DW( 3) = 0.92264465865231730 08
DW( 4) = 0.83885843192756710 08
DW( 5) = 0.186972271504253490 07
DW( 6) = 0.18697201850651240 07
DW( 7) = 0.70273728809723640 06
DW( 8) = 0.702737223635976580 06
DW( 9) = 0.1760857388995040 06
DW(10) = 0.17606236877854890 06
DW(11) = 0.12721341561251880 06
DW(12) = 0.12721222317601070 06
DW(13) = 0.104076227510396910 06
DW(14) = 0.10407622228916480 06
DW(15) = 0.8610241235294180 05
DW(16) = 0.86106924749166780 05
DW(17) = 0.50188505888927740 05
DW(18) = 0.50187706739790460 05
DW(19) = 0.17410816728278580 05
DW(20) = 0.17410727560966900 05
DW(21) = 0.90583658178659360 05
DW(22) = 0.9058353429135140 04
DW(23) = 0.516652709877466820 04
DW(24) = 0.51664565785909400 04
DW(25) = 0.28578977067586220 04
DW(26) = 0.28578842696045800 04
DW(27) = 0.10913935183835750 04
DW(28) = 0.10913653193891040 04
DW(29) = 0.27800327711282940 03
DW(30) = 0.2779990811543410 03
DW(31) = 0.989146131515282610 02
DW(32) = 0.98914002462014940 02
DW(33) = 0.9828517128738710-03
DW(34) = -0.56408735690633520-03
DW(35) = -0.71279783912692240-03
DW(36) = -0.1842107504077970D-02

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EIGENVECTORS OF F MATRIX

	COLUMN(1)	COLUMN(2)	COLUMN(3)	COLUMN(4)	COLUMN(5)	COLUMN(6)	COLUMN(7)	COLUMN(8)	COLUMN(9)	COLUMN(10)
RW(1) 11	2.0020E-35	-2.2319E-02	0.0000E-39	-9.0869E-01	0.0000E-39	1.7380E-04	-5.8471E-05	0.00CCE-39	7.2285E-03	0.000CE-39
RW(1) 21	9.0020E-39	5.5003E-02	0.0000E-39	3.3705E-02	0.0000E-39	-9.8935E-05	-6.247CE-05	0.00CCE-39	-2.1834E-02	0.000CE-39
RW(1) 31	9.0000E-35	-3.5740E-02	0.0000E-39	-9.6713E-02	0.0000E-39	-1.7239E-02	5.5C95E-03	0.00CCE-39	4.2953E-02	0.000CE-39
RW(1) 41	9.0000E-39	-5.8074E-03	0.0000E-39	9.1113E-02	0.0000E-39	2.4261E-02	1.9276E-02	0.00CCE-39	4.1754E-02	0.000CE-39
RW(1) 51	0.0000E-35	1.7163E-05	0.0000E-39	-1.0801E-04	0.0000E-39	3.3760E-02	-5.5254E-02	0.00CCE-39	1.0362E-02	0.000CE-39
RW(1) 61	0.0000E-39	-1.8879E-05	0.0000E-39	7.8813E-05	0.0000E-39	-6.8509E-02	3.4832E-02	0.00CCE-39	1.2345E-03	0.000CE-39
RW(1) 71	2.2321E-02	0.0000E-39	-9.0869E-01	0.0000E-39	-1.7380E-04	0.0000E-39	C. C000E-39	5.8517E-05	0.00CCE-39	7.2272E-03
RW(1) 81	-5.5096E-02	0.0000E-39	3.3687E-02	0.0000E-39	9.7576E-05	0.0000E-39	C. C000E-39	6.2236E-05	0.00CCE-39	-2.1841E-02
RW(1) 91	3.5765E-02	0.0000E-39	-9.6713E-02	0.0000E-39	1.7239E-02	0.0000E-39	C. C000E-39	5.0589E-03	0.00CCE-39	4.2884E-02
RW(1) 101	5.8085E-13	0.0000E-39	9.1113E-02	0.0000E-39	-2.4261E-02	0.0000E-39	C. C000E-39	-1.9277E-02	0.00CCE-39	4.1761E-02
RW(1) 111	-1.5503E-05	0.0000E-39	-1.0801E-04	0.0000E-39	-3.3761E-02	0.0000E-39	5.5254E-02	0.00CCE-39	1.0362E-02	0.000CE-39
RW(1) 121	1.7147E-05	0.0000E-39	7.7123E-05	0.0000E-39	6.8910E-02	0.0000E-39	3.4832E-02	0.00CCE-39	1.2345E-03	0.000CE-39
RW(1) 131	0.0000E-35	3.6795E-01	0.0000E-39	1.6813E-01	0.0000E-39	-8.1075E-05	9.7038E-04	0.00CCE-39	3.7433E-02	0.000CE-39
RW(1) 141	0.0000E-35	-4.6667E-01	0.0000E-39	-1.8511E-01	0.0000E-39	4.7864E-03	-1.5915E-03	0.00CCE-39	-1.8472E-01	0.000CE-39
RW(1) 151	0.0000E-35	3.4341E-01	0.0000E-39	1.3778E-01	0.0000E-39	-3.5784E-03	1.5304E-03	0.00CCE-39	7.5454E-01	0.000CE-39
RW(1) 161	0.0000E-35	-1.8467E-01	0.0000E-39	8.0734E-02	0.0000E-39	2.2577E-02	-2.4596E-03	0.00CCE-39	1.35CE-02	0.000CE-39
RW(1) 171	3.0100E-05	-1.3694E-02	0.0000E-39	-7.0533E-01	0.0000E-39	-2.8403E-02	1.9769E-02	0.00CCE-39	4.2128E-01	0.000CE-39
RW(1) 181	0.0000E-35	6.8829E-01	0.0000E-39	-1.7452E-01	0.0000E-39	-1.7676E-02	1.5478E-02	0.00CCE-39	-5.5803E-01	0.000CE-39
RW(1) 191	0.0000E-35	-2.8134E-02	0.0000E-39	3.0000E-01	0.0000E-39	-9.0179E-01	-3.979CE-02	0.00CCE-39	-6.4158E-02	0.000CE-39
RW(1) 201	0.0000E-35	3.6478E-02	0.0000E-39	2.3704E-01	0.0000E-39	7.3100E-01	-3.2404E-01	0.00CCE-39	-1.0203E-01	0.000CE-39
RW(1) 211	0.0000E-39	1.2026E-02	0.0000E-39	-4.8953E-01	0.0000E-39	3.5518E-01	-2.9C9CE-01	0.00CCE-39	2.1857E-01	0.000CE-39
RW(1) 221	0.0000E-35	6.7343E-05	0.0000E-39	-2.3663E-04	0.0000E-39	2.7655E-01	-5.164CE-02	0.00CCE-39	-1.9255E-02	0.000CE-39
RW(1) 231	0.0000E-35	-5.4282E-05	0.0000E-39	-2.3865E-04	0.0000E-39	-2.1109E-01	2.5887E-01	0.00CCE-39	3.8325E-02	0.000CE-39
RW(1) 241	0.0000E-39	-5.7238E-05	0.0000E-39	-2.6971E-05	0.0000E-39	-2.4410E-01	2.8403E-01	0.00CCE-39	-4.4887E-01	0.000CE-39
RW(1) 251	-3.6796E-01	0.0000E-39	1.6811E-01	0.0000E-39	8.4778E-05	0.0000E-39	-9.7156E-04	0.00CCE-39	3.7494E-02	0.000CE-39
RW(1) 261	4.6609E-01	0.0000E-39	-1.8512E-01	0.0000E-39	-4.7860E-03	0.0000E-39	C. C000E-39	1.5928E-03	0.00CCE-39	-1.8476E-01
RW(1) 271	-3.4339E-01	-0.0000E-39	1.3733E-01	-0.0000E-39	3.5802E-03	-0.0000E-39	-1.5316E-03	-0.0000E-39	7.5482E-01	0.000CE-39
RW(1) 281	1.8466E-01	0.0000E-39	8.0734E-02	0.0000E-39	-2.2570E-01	0.0000E-39	3.4582E-03	0.00CCE-39	1.3469E-02	0.000CE-39
RW(1) 291	1.3731E-02	0.0000E-39	-7.0533E-01	0.0000E-39	2.8363E-02	0.0000E-39	-1.9758E-02	0.00CCE-39	1.2115E-01	0.000CE-39
RW(1) 301	-6.8829E-01	-0.0000E-39	-1.7452E-01	-0.0000E-39	1.7651E-01	-0.0000E-39	-3.5CCE-05	-1.5472E-02	-0.0000E-39	-5.5807E-01
RW(1) 311	2.8132E-02	0.0000E-39	2.6350E-01	0.0000E-39	1.0181E-01	0.0000E-39	C. C000E-39	3.9787E-02	0.0000E-39	-6.4135E-02
RW(1) 321	3.6495E-02	0.0000E-39	2.3707E-01	0.0000E-39	-7.3C99E-01	0.0000E-39	C. C000E-39	3.2404E-01	C. C000E-39	-1.0203E-01
RW(1) 331	-1.2025E-01	-0.0000E-39	-4.8952E-01	-0.0000E-39	3.5521E-01	-0.0000E-39	C. C000E-39	2.051CE-01	C. C000E-39	2.186GE-01
RW(1) 341	-6.1159E-05	0.0000E-39	-2.2747E-04	0.0000E-39	-2.7655E-01	0.0000E-39	C. C000E-39	9.1641E-02	0.0000E-39	-1.9254E-02
RW(1) 351	4.9305E-05	0.0000E-39	2.3586E-04	0.0000E-39	2.1108E-01	0.0000E-39	C. C000E-39	-2.5887E-01	0.0000E-39	3.8348E-02
RW(1) 361	5.1933E-05	0.0000E-39	-3.1683E-04	0.0000E-39	4.4682E-01	0.0000E-39	8.7693E-01	0.0000E-39	4.8879E-03	0.000CE-39

	COLUMN(11)	COLUMN(12)	COLUMN(13)	COLUMN(14)	COLUMN(15)	COLUMN(16)	COLUMN(17)	COLUMN(18)	COLUMN(19)	COLUMN(20)
RW(1) 21	3.8680E-03	0.0000E-39	7.6213E-04	0.00CCE-39	1.0111E-02	0.00CCE-35	5.6424E-03	0.00CCE-39	9.6217E-03	
RW(1) 22	-9.0529E-03	0.0000E-39	-1.4712E-03	0.0000E-39	1.0111E-02	0.00CCE-35	-9.4331E-03	0.00CCE-39	-1.8391E-02	
RW(1) 23	-1.6499E-02	0.0000E-39	8.7052E-03	0.0000E-39	3.0000E-03	0.0000E-39	-1.4912E-02	0.00CCE-39	-1.573CE-02	0.000CE-39
RW(1) 24	1.4992E-01	0.0000E-37	1.5677E-01	0.0000E-39	9.0000E-03	0.0000E-39	-6.3379E-02	0.00CCE-39	-5.4619E-02	0.000CE-39
RW(1) 25	-1.6739E-01	0.0000E-39	-3.9732E-01	0.0000E-39	9.0000E-03	0.0000E-39	1.2974E-01	0.00CCE-39	-4.0161E-01	0.000CE-39
RW(1) 26	5.5981E-03	-1.5981E-03	1.9100E-01	0.0000E-39	-2.7004E-02	0.0000E-39	-2.7004E-02	0.0000E-39	4.0124E-02	0.000CE-39
RW(1) 27	7.0000E-39	-3.8686E-03	0.0000E-39	7.6240E-04	-1.0112E-02	0.0000E-39	-5.4326E-03	0.00CCE-39	9.6223E-03	0.000CE-39
RW(1) 28	0.0000E-35	9.05041E-03	0.00CCE-39	-1.4710E-03	-1.9716E-02	0.0000E-39	5.4335E-03	0.00CCE-39	-1.8353E-02	0.000CE-39
RW(1) 29	0.0000E-35	1.6495E-02	0.00CCE-39	8.0705E-03	-1.4906E-02	0.0000E-39	1.5705E-02	0.00CCE-39	-4.9575E-03	0.000CE-39
RW(1) 30	0.0000E-35	-1.4491E-01	0.00GCE-01	1.9026E-01	-4.3386E-02	0.0000E-39	5.4614E-02	0.00CCE-39	1.8811E-01	0.000CE-39
RW(1) 31	0.0000E-39	1.6740E-01	0.0000E-39	-3.9732E-01	1.2974E-01	0.0000E-39	-1.4C15E-01	0.00CCE-39	-3.4057E-01	0.000CE-39
RW(1) 32	0.0000E-39	-4.4379E-02	0.0000E-39	-3.0742E-02	0.0000E-39	3.9103E-02	0.00CCE-39	1.9643E-01	0.000CE-39	3.1656E-01
RW(1) 33	4.6698E-02	0.0000E-39	1.9556E-02	0.0000E-39	-4.00CCE-02	0.0000E-39	4.4370E-01	0.00CCE-39	-4.4545E-01	0.000CE-39
RW(1) 34	1.8107E-01	0.0000E-39	3.0783E-02	0.0000E-39	0.0000E-39	0.0000E-39	4.5522E-01	0.00CCE-39	-2.2121E-01	0.000CE-39
RW(1) 35	0.7774E-02	0.0000E-39	4.3437E-02	0.0000E-39	0.0000E-39	0.0000E-39	4.5222E-01	0.00CCE-39	-2.4758E-02	0.000CE-39
RW(1) 36	2.1234E-01	0.0000E-39	2.7773E-02	0.0000E-39	0.0000E-39	0.0000E-39	5.9653E-01	0.00CCE-39	1.1342E-01	0.000CE-39
RW(1) 37	6.5896E-02	0.0000E-39	2.844CE-02	0.0000E-39	0.0000E-39	0.0000E-39	4.241CE-01	0.00CCE-39	4.532CE-01	0.000CE-39
RW(1) 38	-6.0909E-01	0.0000E-39	-3.4297E-01	0.0000E-39	0.0000E-39	0.0000E-39	2.6230E-01	0.00CCE-39	2.6595E-01	0.000CE-39
RW(1) 39	1.6202E-02	0.0000E-39	3.7808E-01	0.0000E-39	0.0000E-39	0.0000E-39	-2.7313E-01	0.00CCE-39	3.4635E-01	0.000CE-39
RW(1) 40	-5.4747E-01	0.0000E-39	-3.2436E-01	0.0000E-39	0.0000E-39	0.0000E-39	-2.1517E-01	0.0000E-39	-4.5222E-01	0.000CE-39
RW(1) 41	-5.0037E-01	0.0000E-39	4.0832E-01	0.0000E-39	0.0000E-39	0.0000E-39	1.7179E-01	0.0000E-39	1.7179E-01	0.000CE-39
RW(1) 42	8.8636E-03	0.0000E-39	1.0081E-01	0.0000E-39	0.0000E-39	0.0000E-39	4.1688E-03	0.00CCE-39	3.0000E-03	0.000CE-39
RW(1) 43	0.0000E-35	4.4388E-02	0.0000E-39	-3.0745E-02	0.0000E-39	3.0745E-02	0.0000E-39	2.1020E-01	-3.0745E-02	0.000CE-39
RW(1) 44	0.0000E-35	-4.3680E-02	0.0000E-39	1.9599E-02	0.0000E-39	4.4965E-01	0.0000E-39	-1.7323E-01	0.0000E-39	-1.9765E-01
RW(1) 45	0.0000E-35	-1.0647E-01	0.0000E-39	-3.4853E-02	0.0000E-39	9.7868E-02	0.0000E-39	-2.1697E-01	0.0000E-39	-2.6155E-02
RW(1) 46	0.0000E-35	-1.0647E-01	0.0000E-39	3.0747E-02	0.0000E-39	3.0747E-02	0.0000E-39	-2.2102E-01	0.0000E-39	-2.7582E-02
RW(1) 47	0.0000E-35	-1.8113E-01	0.0000E-39	3.0797E-02	0.0000E-39	3.0797E-02	0.0000E-39	-2.2102E-01	0.0000E-39	-2.7592E-01
RW(1) 48	0.0000E-35	-3.7779E-01	0.0000E-39	4.3477E-02	0.0000E-39	4.3477E-02	0.0000E-39	-3.5204E-02	0.0000E-39	-4.3204E-02
RW(1)										

RW1(1)	-2.6740E-01	0.0000E-39	-0.4450E-01	-0.3134E-01	-0.4040E-01	-5.9355E-02
RW1(2)	5.4028E-01	0.0000E-39	-0.6000E-01	-2.8539E-01	-0.5000E-01	-4.7752E-01
RW1(3)	2.3142E-01	0.0000E-39	-0.3000E-01	-1.2027E-01	-0.3000E-01	-6.1856E-01
RW1(4)	-3.1325E-01	0.0000E-39	-0.6000E-01	1.4117E-01	-0.6000E-01	-4.8523E-01
RW1(5)	-3.7553E-01	0.0000E-39	-0.6000E-01	0.10516E-01	-0.3000E-01	-3.4486E-01
RW1(6)	-6.7480E-01	0.0000E-39	-0.2000E-01	6.9264E-02	-0.4000E-01	-1.8283E-01
RW1(7)	-0.3000E-03	2.6779E-01	2.9322E-01	7.0032E-01	-8.8660E-01	0.3000E-01
RW1(8)	0.0000E-35	-5.4000E-01	-3.3641E-01	0.0000E-39	-4.4238E-01	0.0000E-01
RW1(9)	-0.4000E-35	-2.3141E-01	-6.1689E-01	0.0000E-39	-1.1962E-01	0.0000E-01
RW1(10)	0.0000E-35	3.1324E-01	-5.3351E-01	0.0000E-39	-5.0e00E-02	0.0000E-01
RW1(11)	-0.4000E-35	3.7554E-01	-3.5546E-01	0.0000E-39	-2.9e00E-02	0.0000E-01
RW1(12)	0.0000E-39	5.7194E-01	-1.9544E-01	0.0000E-39	-6.0725E-03	0.0000E-01
RW1(13)	4.0545E-03	0.0000E-39	-0.0000E-01	1.8102E-04	-0.0000E-39	7.6852E-07
RW1(14)	4.2563E-03	0.0000E-39	-0.0000E-01	1.0272E-06	-0.0000E-39	4.5391E-07
RW1(15)	-3.4054E-13	0.0000E-39	-0.0000E-01	-4.1275E-07	-0.0000E-39	-2.2494E-07
RW1(16)	1.0296E-01	0.0000E-39	-0.0000E-01	4.1309E-07	-0.0000E-39	1.1139E-06
RW1(17)	-2.8428E-04	0.0000E-39	-0.0000E-01	-9.5625E-08	-0.0000E-39	4.6445E-07
RW1(18)	-7.591R-02	0.0000E-39	-0.0000E-01	3.7114E-07	-0.0000E-39	-1.2154E-07
RW1(19)	3.5634E-03	0.0000E-39	-0.0000E-01	9.4690E-05	-0.0000E-39	-8.2159E-07
RW1(20)	8.9243E-03	0.0000E-39	-0.0000E-01	6.1428E-04	-0.0000E-39	-4.4499E-07
RW1(21)	-1.9618E-02	0.0000E-39	-0.0000E-01	-8.7643E-08	-0.0000E-39	7.4242E-07
RW1(22)	-5.1223E-02	0.0000E-39	-0.0000E-01	-3.6922E-08	-0.0000E-39	3.4C39E-07
RW1(23)	-1.9946E-03	0.0000E-39	-0.0000E-01	-1.8453E-09	-0.0000E-39	6.7194E-09
RW1(24)	-6.5177E-04	0.0000E-39	-0.0000E-01	-6.4727E-10	-0.0000E-39	2.3363E-09
RW1(25)	0.0000E-39	-4.0e00E-03	-1.811e-06	0.0000E-39	-1.3724E-01	0.0000E-39
RW1(26)	0.0000E-35	-4.2512E-03	-1.0843E-06	0.0000E-39	-8.2758E-07	0.0000E-39
RW1(27)	-0.0000E-39	3.4058E-03	6.1073E-07	-0.0000E-39	5.2806E-07	-0.0000E-39
RW1(28)	0.0000E-35	-1.0096E-01	-2.16CC-06	0.0000E-39	-1.0388E-06	0.0000E-39
RW1(29)	0.0000E-35	2.8394E-04	-5.681CE-08	0.0000E-39	4.5870E-08	0.0000E-39
RW1(30)	-0.0000E-39	7.5919E-03	5.2876E-07	-0.0000E-39	6.0370E-08	0.0000E-39
RW1(31)	0.0000E-39	-3.5436E-02	-1.4465E-06	0.0000E-39	-4.1739E-07	0.0000E-39
RW1(32)	0.0000E-39	-8.9253E-03	-8.3434E-07	0.0000E-39	-2.2858E-07	0.0000E-39
RW1(33)	-0.0000E-39	1.9d19E-02	1.2676E-06	-0.0000E-39	3.7590E-07	-0.0000E-39
RW1(34)	0.0000E-35	5.1223E-02	-1.8827E-07	0.0000E-39	5.1645E-09	0.0000E-39
RW1(35)	0.0000E-39	1.9446L-03	7.1331E-09	0.0000E-39	8.0944E-10	0.0000E-39
RW1(36)	0.0000E-39	5.5177E-04	2.7054E-09	0.0000E-39	3.1545E-10	0.0000E-39

BRTH0 CHECK

COLUMN(1)	COLUMN(2)	COLUMN(3)	COLUMN(4)	COLUMN(5)	COLUMN(6)	COLUMN(7)	COLUMN(8)	COLUMN(9)	COLUMN(10)	
RW1(1)	1.0000E 0C	0.0000E-39	4.0311E-09	0.0000E-39	-1.8740E-08	0.0000E-39	-1.7113E-08	0.0000E-39	-7.0258E-08	
RW1(2)	0.0000E-39	1.0000E 00	-0.0000E-39	-1.7322E-09	0.0000E-39	-3.5132E-C9	-2.2411E-09	0.0CC0E-39	1.6775E-C8	-0.0000E-39
RW1(3)	4.0311E-09	-0.0000E-39	1.0000E 00	0.0000E-39	-2.4722E-06	-0.0000E-39	-9.0.0000E-39	-0.0000E-39	-4.7451E-08	-0.0000E-39
RW1(4)	0.0000E-05	-0.0000E-39	1.0000E 00	0.0000E-39	0.0000F-39	2.2824E-C6	4.3677E-04	0.0CC0E-39	3.0354E-04	-0.0000E-39
RW1(5)	-1.8740E-06	0.0000E-39	-2.4722E-06	0.0000E-39	1.0000E 00	0.0000F-39	3.0.0000E-39	4.3000E-39	-4.7451E-08	-0.0000E-39
RW1(6)	-0.0000E-39	-3.5132E-09	-0.0000E-39	2.2824E-06	0.0LC0E-39	1.0000E 00	-1.6779E-08	0.0CC0E-39	2.2461E-08	-0.0000E-39
RW1(7)	0.0000E-39	-3.5132E-09	-0.0000E-39	2.2824E-06	0.0LC0E-39	1.0000E 00	-1.7679E-08	1.0000E 00	5.7615E-09	-0.0000E-39
RW1(8)	-1.7113E-06	0.0000E-39	-4.7451E-04	0.0000E-39	-8.3211E-09	0.0000E-39	3.0.0000E-39	4.3000E-39	1.0CC0E 00	0.0000E-39
RW1(9)	0.0000E-39	1.6775E-08	-0.0000E-39	3.0354E-04	-0.0000E-39	-3.1964E-08	-0.0000E-39	-1.0000E 00	-0.0000E-39	1.0000E 00
RW1(10)	-7.0258E-08	-0.0000E-39	3.3105E-04	-0.0000E-39	-3.1964E-08	-0.0000E-39	-2.9040E-C9	-0.0000E-39	-1.0000E 00	-0.0000E-39
RW1(11)	-0.0000E-35	-5.5308E-10	-0.0000E-39	-2.5837E-04	0.0000E-39	-2.3381E-C6	5.6246E-C5	0.0CC0E-39	-9.5262E-09	-0.0000E-39
RW1(12)	-1.4987E-05	-0.0000E-39	2.8164E-04	-0.0000E-39	-2.6103E-06	-0.0000E-39	-0.0000E-39	3.51718E-09	-0.0000E-39	2.7619E-09
RW1(13)	0.0000E-39	-1.0583E-09	-0.0000E-39	-5.2544E-05	0.0000E-39	5.7943E-C5	1.5365E-08	0.0CC0E-39	-5.0459E-09	-0.0000E-39
RW1(14)	2.4589E-05	0.0000E-39	-5.7257E-05	0.0000E-39	-6.4711E-05	0.0CC0E-39	3.0.0000E-39	3.17225E-08	0.0000E-39	-1.9985E-09
RW1(15)	4.7898E-08	0.0000E-39	-6.3642E-04	0.0000E-39	7.1364E-U6	0.0CC0E-39	3.0.0000E-39	6.85C7E-09	0.0000E-39	-1.1417E-08
RW1(16)	0.0000E-39	-1.4119E-08	-0.0000E-39	-5.5623E-04	0.0000E-39	-6.3803E-06	8.7558E-09	0.0CC0E-39	-2.7589E-08	-0.0000E-39
RW1(17)	0.0000E-35	5.6717E-09	-0.0000E-39	-4.8276E-05	0.0000E-39	1.7797E-05	-0.0000E-39	0.0CC0E-39	8.9942E-09	-0.0000E-39
RW1(18)	0.0000E-35	5.6717E-09	-0.0000E-39	-4.8276E-05	0.0000E-39	1.5542E-C5	5.3871E-05	0.0CC0E-39	-6.6238E-09	-0.0000E-39
RW1(19)	2.5298E-08	-0.0000E-39	1.5088E-03	-0.0000E-39	6.9769E-05	-0.0000E-39	-2.3381E-C6	5.6246E-C5	0.0CC0E-39	-9.5262E-09
RW1(20)	0.0000E-35	-2.5298E-09	-0.0000E-39	1.3837E-04	0.0000E-39	-2.6103E-06	-0.0000E-39	-0.0000E-39	3.51718E-09	-0.0000E-39
RW1(21)	0.0000E-39	-1.0074E-08	-0.0000E-39	4.6512E-04	0.0000E-39	2.9236E-C5	1.5631E-07	0.0CC0E-39	1.2766E-07	-0.0000E-39
RW1(22)	5.7847E-08	0.0000E-39	5.7151F-05	0.0000E-39	-3.2644E-05	0.0000E-39	29.CCC0E-35	-1.61617E-07	0.0000E-39	1.1995E-07
RW1(23)	0.0000E-35	5.5698E-09	-0.0000E-39	-5.5724E-05	0.0000E-39	-5.5358E-C6	2.5514E-07	0.0CC0E-39	1.2103E-05	-0.0000E-39
RW1(24)	8.9144E-09	0.0000E-39	6.0815E-05	-0.0000E-39	-6.1946E-06	0.0000E-39	-0.0000E-39	3.2497E-07	-0.0000E-33	-1.0710E-05
RW1(25)	0.0000E-35	-1.6522E-10	-0.0000E-39	-1.6730E-04	0.0000E-39	-3.5882E-C6	6.5545E-07	0.0CC0E-39	-1.5357E-05	-0.0000E-39
RW1(26)	-1.6132E-08	0.0000E-39	-1.8238E-04	0.0000E-39	-4.0444E-06	0.0000E-39	-0.0000E-39	6.5634E-07	-0.0000E-39	-1.3601E-05
RW1(27)	-2.1229E-08	-0.0000E-39	-2.2236E-04	-0.0000E-39	-2.5462E-05	-0.0000E-39	-0.0000E-39	1.3C28E-07	-0.0000E-39	-1.5522E-08
RW1(28)	0.0.000E-05	3.0393E-09	-0.0000E-39	-2.0424E-04	0.0000E-39	-2.2792E-C5	-1.7441E-07	0.0000E-39	4.7436E-05	-0.0000E-39
RW1(29)	7.4565E-05	-0.0000E-39	7.3611F-05	0.0000E-39	1.4982E-05	-0.0000E-39	-0.0000E-39	3.0.0000E-07	0.0000E-39	2.9205E-04
RW1(30)	0.0.000E-35	1.2375E-09	-0.0000E-39	-6.7521E-05	0.0000E-39	-1.3614E-06	-1.6102E-07	0.0000E-39	3.1492E-07	-0.0000E-39
RW1(31)	0.0.000E-39	1.6480E-09	-0.0000E-39	-2.1663E-05	0.0000E-39	7.3611E-06	-1.6102E-07	0.0000E-39	3.1603E-07	-0.0000E-39
RW1(32)	2.3200E-05	0.0000E-39	-2.5595E-09	0.0000E-39	-2.4024E-06	0.0000E-39	0.0CC0E-39	4.3843E-04	-0.0000E-39	-3.8818E-04
RW1(33)	-3.9625E-09	0.0000E-39	-2.5595E-09	0.0000E-39	-2.4024E-06	0.0000E-39	0.0CC0E-39	3.7C10E-08	0.0000E-39	1.8767E-05
RW1(34)	0.0000E-35	-4.4391E-09	-0.0000E-39	7.4622E-05	0.0000E-39	-6.8363E-C6	1.1539E-07	0.0CC0E-39	-6.7422E-05	-0.0000E-39
RW1(35)	1.0337E-08	0.0000E-39	7.7405E-05	0.0000E-39	7.2651E-06	0.0000E-39	0.0000E-39	-1.1176E-07	0.0000E-39	-5.6793E-05
RW1(36)	0.0000E-39	-3.1564E-11	-0.0000E-39	4.7521E-06	0.0000E-39	-4.3559E-C7	7.1710E-C9	0.0CC0E-39	-4.2967E-06	-0.0000E-39

COLUMN(11)	COLUMN(12)	COLUMN(13)	COLUMN(14)	COLUMN(15)	COLUMN(16)	COLUMN(17)	COLUMN(18)	COLUMN(19)	COLUMN(20)	
RW1(1)	0.0000E-39	-1.4987E-09	0.0000E-39	2.4589E-09	4.7858E-C8	0.0000E-39	-2.419E-08	0.0CC0E-39	2.2508E-08	0.0000E-39
RW1(2)	-5.5318E-1C	-0.0000E-39	-1.0583E-09	0.0000E-39	-0.0000E-39	-1.4119E-C8	-0.0CC0E-39	5.6717E-09	-0.0000E-39	-2.5259E-09
RW1(3)	-0.0000E-35	2.8164E-04	-0.0000E-39	-5.7297E-05	-6.0624E-04	-0.0000E-39	5.2597E-05	-0.0000E-39	1.5086E-04	-0.0000E-39
RW1(4)	-2.5837E-04	-0.0000E-39	-5.2544E-05	0.0000E-39	0.0000E-39	-5.5623E-C4	-0.0CC0E-39	-4.8270E-05	-0.0000E-39	1.3337E-04
RW1(5)	0.0000E-39	-2.6103E-06	0.0CC0E-39	-6.4711E-05	7.1363E-06	-0.0000E-39	3.7797E-05	0.0000E-39	6.9749E-05	0.0000E-39
RW1(6)	-2.3381E-06	-0.0000E-39	5.7943E-05	0.0000E-39	0.0000E-39	-3.5803E-C6	-0.0CC0E-39	5.5942E-05	-0.0000E-39	-6.2464E-05
RW1(7)	5.6246E-05	-0.0000E-39	1.5365E-08	0.0000E-39	0.0000E-39	-8.7758E-C9	-0.0CC0E-39	5.3871E-09	-0.0000E-39	-1.32C9E-07
RW1(8)	0.0000E-39	5.7177E-09	0.0000E-39	-2.1225E-04	8.6507E-08	0.0000E-39	8.5942E-09	0.0000E-39	1.3028E-07	0.0000E-39
RW1(9)	-9.5262E-05	-0.0000E-39	-5.0455E-09	0.0000E-39	0.0000E-39	-3.5789E-C8	-0.0000E-39	6.6286E-C9	-0.0000E-39	-1.8645E-08

ROW(16)	-0.000E-39	0.000E-39	-1.642F 11	-7.148E 10	-1.910E 10	2.914E 10	-3.375E 10	-4.6859E 10	8.8674E 09	-6.2173E 09
ROW(17)	-0.000E-39	0.000E-39	8.5CP3E 10	5.7149E 10	1.5272E 10	-3.3752E 10	5.6589E 10	4.7070E 10	-2.5086E 10	1.7585E 10
ROW(18)	0.000E-39	5.000E-39	1.6713E 11	1.2569E 11	3.3588E 10	-4.6899E 10	4.7C7CE 10	7.8455E 10	-5.6988E 09	5.6988E 09
ROW(19)	-3.000E-39	0.000E-39	0.000CE-39	0.000CE-39	0.000E-39	8.8674E 09	-2.5086E 10	1.5368E 10	-1.0931E 10	6.3808E 09
ROW(20)	-0.000E-39	0.000E-39	0.000CE-39	0.000CE-39	0.000E-39	-6.2173E 09	1.7585E 10	5.6988E 09	-1.0931E 10	6.3808E 09
ROW(21)	-0.000E-39	0.000E-39	0.000CE-39	0.000CE-39	0.000E-39	-2.5840E 10	7.3100E 10	2.3685E 10	-4.4585E 10	3.1355E 10
ROW(22)	-0.000E-39	0.000E-39	0.000CE-39	0.000CE-39	0.000E-39	0.000CE-39	0.000CE-39	0.000CE-39	-1.0564E 08	4.1535E 08
ROW(23)	-0.000E-39	0.000E-39	0.000CE-39	0.000CE-39	0.000E-39	0.000CE-39	0.000CE-39	0.000CE-39	-5.2743E 07	2.074CE 08
ROW(24)	-0.000E-39	0.000E-39	0.000CE-39	0.000CE-39	0.000E-39	0.000CE-39	0.000CE-39	0.000CE-39	-8.7061E 07	3.4234E 08
ROW(25)	-0.000E-39	0.000E-39	0.000CE-39	0.000CE-39	0.000E-39	0.000CE-39	0.000CE-39	0.000CE-39	0.000E-39	0.000E-39
ROW(26)	-0.000E-39	0.000E-39	0.000CE-39	0.000CE-39	0.000E-39	0.000CE-39	0.000CE-39	0.000CE-39	0.000E-39	0.000E-39
ROW(27)	-0.000E-39	0.000E-39	0.000CE-39	0.000CE-39	0.000E-39	0.000CE-39	0.000CE-39	0.000CE-39	0.000E-39	0.000E-39
ROW(28)	-0.000E-39	0.000E-39	0.000CE-39	0.000CE-39	0.000E-39	0.000CE-39	0.000CE-39	0.000CE-39	0.000E-39	0.000E-39
ROW(29)	-0.000E-39	0.000E-39	0.000CE-39	0.000CE-39	0.000E-39	0.000CE-39	0.000CE-39	0.000CE-39	0.000E-39	0.000E-39
ROW(30)	-0.000E-39	0.000E-39	0.000CE-39	0.000CE-39	0.000E-39	0.000CE-39	0.000CE-39	0.000CE-39	0.000E-39	0.000E-39
ROW(31)	-2.1646E 07	2.4293E 07	0.000CE-39	0.000CE-39	0.000E-39	0.000CE-39	0.000CE-39	0.000CE-39	0.000E-39	0.000E-39
ROW(32)	8.5118E 07	-9.5525E 07	0.000CE-39	0.000CE-39	0.000E-39	0.000CE-39	0.000CE-39	0.000CE-39	0.000E-39	0.000E-39
ROW(33)	1.3917E 07	-1.5619E 07	0.000CE-39	0.000CE-39	0.000E-39	0.000CE-39	0.000CE-39	0.000CE-39	0.000E-39	0.000E-39
ROW(34)	6.1617E 07	-5.5576E 07	-0.000CE-39	-0.000CE-39	-0.000E-39	-0.000CE-39	-0.000CE-39	-0.000CE-39	-0.000E-39	-0.000E-39
ROW(35)	3.0764E 07	-2.7747E 07	-0.000CE-39	-0.000CE-39	-0.000E-39	-0.000CE-39	-0.000CE-39	-0.000CE-39	-0.000E-39	-0.000E-39
ROW(36)	5.0781E 07	-4.5853E 07	-0.000CE-39	-0.000CE-39	-0.000E-39	-0.000CE-39	-0.000CE-39	-0.000CE-39	-0.000E-39	-0.000E-39

COLUMN(21)	COLUMN(22)	COLUMN(23)	COLUMN(24)	COLUMN(25)	COLUMN(26)	COLUMN(27)	COLUMN(28)	COLUMN(29)	COLUMN(30)	
ROW(1)	0.000E-39	0.000E-39	0.000CE-39	0.000CE-39	0.000E-39	0.000CE-39	0.000CE-39	0.000CE-39	0.000CE-39	
ROW(2)	-4.3763E 09	0.000E-39	0.000CE-39	0.000CE-39	0.000E-39	0.000CE-39	0.000CE-39	0.000CE-39	0.000CE-39	
ROW(3)	3.7176E 10	-5.3232E 07	-2.6576E 07	-4.3871E 07	0.000E-39	0.000CE-39	0.000CE-39	0.000CE-39	0.000CE-39	
ROW(4)	-2.8798E 10	4.7191E 07	2.3562E 07	3.8893E 07	0.000E-39	0.000CE-39	0.000CE-39	0.000CE-39	0.000CE-39	
ROW(5)	1.3917E 07	6.1617E 07	3.0764E 07	5.0781E 07	0.000E-39	0.000CE-39	0.000CE-39	0.000CE-39	0.000CE-39	
ROW(6)	-1.5161E 07	-5.5576E 07	-2.7747E 07	-4.5853E 07	-0.000E-39	-0.000CE-39	-0.000CE-39	-0.000CE-39	-0.000CE-39	
ROW(7)	0.000E-39	0.000E-39	0.000CE-39	0.000CE-39	0.000E-39	0.000CE-39	0.000CE-39	0.000CE-39	0.000CE-39	
ROW(8)	0.000E-39	0.000E-39	0.000CE-39	0.000CE-39	0.000E-39	1.1153E 11	7.4915E 10	2.2C19E 10	1.2322E 10	1.4894E 10
ROW(9)	0.000E-39	0.000E-39	0.000CE-39	0.000CE-39	0.000E-39	5.5604E 10	-3.7348E 10	-9.5804E 05	4.3762E 09	1.303EE 10
ROW(10)	0.000E-39	0.000E-39	0.000CE-39	0.000CE-39	0.000E-39	0.000CE-39	0.000CE-39	0.000CE-39	6.3132E 09	-1.786CE 10
ROW(11)	-0.000E-39	-0.000E-39	-0.000CE-39	-0.000CE-39	-0.000E-39	-0.000CE-39	-0.000CE-39	-0.000CE-39	-0.000E-39	-0.000E-39
ROW(12)	0.000E-39	0.000E-39	0.000CE-39	0.000CE-39	0.000E-39	0.000CE-39	0.000CE-39	0.000CE-39	0.000E-39	0.000E-39
ROW(13)	0.000E-39	0.000E-39	0.000CE-39	0.000CE-39	0.000E-39	0.000CE-39	0.000CE-39	0.000CE-39	0.000E-39	0.000E-39
ROW(14)	0.000E-39	0.000E-39	0.000CE-39	0.000CE-39	0.000E-39	0.000CE-39	0.000CE-39	0.000CE-39	0.000E-39	0.000E-39
ROW(15)	0.000E-39	0.000E-39	0.000CE-39	0.000CE-39	0.000E-39	0.000CE-39	0.000CE-39	0.000CE-39	0.000E-39	0.000E-39
ROW(16)	-2.5840E 10	0.000E-39	0.000CE-39	0.000CE-39	0.000E-39	0.000CE-39	0.000CE-39	0.000CE-39	0.000E-39	0.000E-39
ROW(17)	7.3101E 10	0.000E-39	0.000CE-39	0.000CE-39	0.000E-39	0.000CE-39	0.000CE-39	0.000CE-39	0.000E-39	0.000E-39
ROW(18)	2.3685E 10	0.000E-39	0.000CE-39	0.000CE-39	0.000E-39	0.000CE-39	0.000CE-39	0.000CE-39	0.000E-39	0.000E-39
ROW(19)	-6.4585E 10	-1.0564E 08	-5.2743E 07	-8.7041E 07	0.000E-39	0.000CE-39	0.000CE-39	0.000CE-39	0.000E-39	0.000E-39
ROW(20)	3.1355E 10	4.1539E 08	2.074CE 08	3.4234E 08	0.000E-39	0.000CE-39	0.000CE-39	0.000CE-39	0.000E-39	0.000E-39
ROW(21)	1.2985E 11	6.7918E 07	3.391CE 07	5.5975E 07	0.000E-39	0.000CE-39	0.000CE-39	0.000CE-39	0.000E-39	0.000E-39
ROW(22)	6.7919E 07	2.4865E 08	1.226CE 08	2.0430E 08	0.000E-39	0.000CE-39	0.000CE-39	0.000CE-39	0.000E-39	0.000E-39
ROW(23)	3.3910E 07	1.2240E 08	6.6733E 07	1.0202E 08	0.000E-39	0.000CE-39	0.000CE-39	0.000CE-39	0.000E-39	0.000E-39
ROW(24)	5.5775E 07	2.0430E 08	1.0202E 08	1.6837E 08	0.000E-39	0.000CE-39	0.000CE-39	0.000CE-39	0.000E-39	0.000E-39
ROW(25)	0.000E-39	0.000CE-39	0.000CE-39	0.000CE-39	0.000E-39	5.2627E 11	3.4943E 11	5.3326E 10	-1.176CE 11	9.3591E 10
ROW(26)	0.000E-39	0.000CE-39	0.000CE-39	0.000CE-39	0.000E-39	3.4943E 11	2.3471E 11	6.2721E 10	-7.8629E 10	6.2864E 10
ROW(27)	0.000E-39	0.000CE-39	0.000CE-39	0.000CE-39	0.000E-39	0.000CE-39	0.000CE-39	0.000CE-39	0.000E-39	0.000E-39
ROW(28)	0.000E-39	0.000CE-39	0.000CE-39	0.000CE-39	0.000E-39	0.000CE-39	0.000CE-39	0.000CE-39	0.000E-39	0.000E-39
ROW(29)	0.000E-39	0.000CE-39	0.000CE-39	0.000CE-39	0.000E-39	0.000CE-39	0.000CE-39	0.000CE-39	0.000E-39	0.000E-39
ROW(30)	0.000E-39	0.000CE-39	0.000CE-39	0.000CE-39	0.000E-39	0.000CE-39	0.000CE-39	0.000CE-39	0.000E-39	0.000E-39
ROW(31)	0.000E-39	0.000CE-39	0.000CE-39	0.000CE-39	0.000E-39	0.000CE-39	0.000CE-39	0.000CE-39	0.000E-39	0.000E-39
ROW(32)	-0.000E-39	-0.000CE-39	-0.000CE-39	-0.000CE-39	-0.000E-39	-0.000CE-39	-0.000CE-39	-0.000CE-39	-0.000E-39	-0.000E-39
ROW(33)	-0.000E-39	-0.000CE-39	-0.000CE-39	-0.000CE-39	-0.000E-39	-0.000CE-39	-0.000CE-39	-0.000CE-39	-0.000E-39	-0.000E-39
ROW(34)	-0.000E-39	-0.000CE-39	-0.000CE-39	-0.000CE-39	-0.000E-39	-0.000CE-39	-0.000CE-39	-0.000CE-39	-0.000E-39	-0.000E-39
ROW(35)	-0.000E-39	-0.000CE-39	-0.000CE-39	-0.000CE-39	-0.000E-39	-0.000CE-39	-0.000CE-39	-0.000CE-39	-0.000E-39	-0.000E-39
ROW(36)	-0.000E-39	-0.000CE-39	-0.000CE-39	-0.000CE-39	-0.000E-39	-0.000CE-39	-0.000CE-39	-0.000CE-39	-0.000E-39	-0.000E-39

COLUMN(31)	COLUMN(32)	COLUMN(33)	COLUMN(34)	COLUMN(35)	COLUMN(36)	COLUMN(37)
ROW(1)	0.000E-39	-0.000E-39	-0.000CE-39	-0.000CE-39	-0.000E-39	-0.000CE-39
ROW(2)	1.0320E-35	-0.000E-39	-0.000CE-39	-0.000CE-39	-0.000E-39	-0.000CE-39
ROW(3)	0.000E-39	-0.000E-39	-0.000CE-39	-0.000CE-39	-0.000E-39	-0.000CE-39
ROW(4)	0.000E-39	-0.000E-39	-0.000CE-39	-0.000CE-39	-0.000E-39	-0.000CE-39
ROW(5)	-0.000E-39	-0.000E-39	-0.000CE-39	-0.000CE-39	-0.000E-39	-0.000CE-39
ROW(6)	0.000E-39	-0.000E-39	-0.000CE-39	-0.000CE-39	-0.000E-39	-0.000CE-39
ROW(7)	0.000E-39	-0.000E-39	-0.000CE-39	-0.000CE-39	-0.000E-39	-0.000CE-39
ROW(8)	3.1620E 05	-2.2170E 09	-9.2135E 09	-0.000CE-39	-0.000CE-39	-0.000CE-39
ROW(9)	-1.4316E 10	9.7514E 09	4.0855E 09	-0.000CE-39	-0.000CE-39	-0.000CE-39
ROW(10)	1.0851E 10	-7.5240E 09	-3.1679E 09	4.7191E 09	2.3562E 07	3.8893E 07
ROW(11)	-2.1646E 07	8.5118E 07	1.3917E 07	6.1617E 07	3.0764E 07	5.C781E 07
ROW(12)	2.4293E 07	-9.5525E 07	-1.5615E 07	-5.5576E 07	-2.7747E 07	-4.5803E 07
ROW(13)	0.000E-35	-0.000E-39	-0.000CE-39	-0.000CE-39	-0.000E-39	-0.000CE-39
ROW(14)	0.000E-35	-0.000E-39	-0.000CE-39	-0.000CE-39	-0.000E-39	-0.000CE-39
ROW(15)	0.000E-35	-0.000E-39	-0.000CE-39	-0.000CE-39	-0.000E-39	-0.000CE-39
ROW(16)	0.000E-39	-0.000E-39	-0.000CE-39	-0.000CE-39	-0.000E-39	-0.000CE-39
ROW(17)	0.000E-39	-0.000E-39	-0.000CE-39	-0.000CE-39	-0.000E-39	-0.000CE-39
ROW(18)	0.000E-39	-0.000E-39	-0.000CE-39	-0.000CE-39	-0.000E-39	-0.000CE-39
ROW(19)	0.000E-39	-0.000E-39	-0.000CE-39	-0.000CE-39	-0.000E-39	-0.000CE-39
ROW(20)	0.000E-39	-0.000E-39	-0.000CE-39	-0.000CE-39	-0.000E-39	-0.000CE-39
ROW(21)	0.000E-39	-0.000E-39	-0.000CE-39	-0.000CE-39	-0.000E-39	-0.000CE-39
ROW(22)	0.000E-39	-0.000E-39	-0.000CE-39	-0.000CE-39	-0.000E-39	-0.000CE-39
ROW(23)	0.000E-39	-0.000E-39	-0.000CE-39	-0.000CE-39	-0.000E-39	-0.000CE-39
ROW(24)	0.000E-39	-0.000E-39	-0.000CE-39	-0.000CE-39	-0	

SYSTEM EIGENVALUES AND EIGENVECTORS

MODE	1	2	3	4	5	6	7	8	9
FREQ. GEN. MASS	0.034831 5.0938E 04	0.004249 1.1945E 05	C.003780 9.5679E 04	C.004875 4.4566E 04	1.582884 4.425CE 03	1.5E2889 4.4251E 03	2.653639 2.3300E 03	2.653659 2.3300E 03	5.036356 8.5756E 03
UL1(1)	0.063593	0.000000	-1.000000	0.000000	0.000000	-0.115219	-0.071922	-0.000000	-C.189573
UR1(1)	-0.347903	0.000000	-C.412241	0.000000	0.000000	0.116978	C.082523	-0.000000	0.189525
UL1(2)	-0.347903	0.000000	-C.412241	0.000000	0.000000	0.116978	C.082523	-0.000000	C.189525
UR1(2)	-0.761816	0.000000	C.178969	0.000000	0.000000	0.000000	-0.09250	-0.063669	-0.000000
UL1(3)	-0.761816	0.000000	C.178969	0.000000	0.000000	0.000000	-0.09250	-0.063669	-0.000000
UR1(3)	-0.882117	0.000000	0.350832	0.000000	0.000000	-0.183206	-0.122040	-0.000000	C.333666
UL1(4)	-0.884523	0.000000	C.356269	0.000000	0.000000	-0.153818	-C.116592	-0.000000	C.361660
UR1(4)	-1.090000	0.000000	C.519256	0.000000	0.000000	-1.000000	1.000000	0.000000	-1.000000
UL2(1)	-0.000000	-1.000000	-C.000000	C.310232	0.115214	-0.000000	-C.000000	0.071921	-C.000000
UR2(1)	-0.000000	-0.626339	-C.000000	C.196712	-0.116972	-0.000000	-0.000000	-0.082521	-C.000000
UL2(2)	-0.000000	-0.626339	-C.000000	-C.706596	-0.09244	-0.000000	-0.000000	0.063668	-C.000000
UR2(2)	-0.000000	-0.250484	-C.000000	-C.706596	-0.09244	-0.000000	-0.000000	0.063668	-C.000000
UL2(3)	-0.000000	-C.250484	-C.000000	-0.706596	-C.089244	-0.000000	-C.000000	0.63668	-C.000000
UR2(3)	-0.000000	-0.141206	-0.000000	-0.854778	0.1H3210	-0.000000	-0.000000	0.122045	-C.000000
UL2(4)	0.000000	-0.139020	C.000000	-C.857742	0.193822	0.000000	0.000000	0.116598	C.000000
UR2(4)	-0.000000	-0.034111	-C.000000	-1.000000	1.000000	-C.000000	-C.000000	-1.000000	-C.000000
BLMD1(1,1)	-0.03C005	-0.000000	-0.000015	-0.000000	-0.000000	-0.03688	-C.03338	0.000000	C.015087
BLMD1(1,2)	0.03C007	0.000000	C.000024	0.000000	0.000000	-C.05552	C.011090	-0.000000	C.11750
BLMD1(1,3)	-0.03C002	-0.000000	-C.000035	-0.000000	-0.000000	-0.00177	0.000357	0.000000	-C.004165
BLMD1(2,1)	0.09C003	-0.000000	C.000013	-0.000000	-0.000000	C.016607	0.016948	0.000000	-C.135184
BLMD1(2,2)	0.09C004	0.000000	C.000003	0.000000	0.000000	-C.025441	-0.001169	-0.000000	C.129078
BLMD1(2,3)	-0.09C003	-0.000000	0.000009	-0.000000	-0.000000	-C.030739	-C.042857	0.000000	-C.242319
BLMD1(3,1)	0.03C001	-0.000000	-C.000000	-0.000000	-0.000000	-C.03860	-0.015085	0.000000	C.016923
BLMD1(3,2)	-0.03C000	0.000000	C.000000	-0.000000	-0.000000	-C.09829	0.019101	0.000000	-C.019568
BLMD1(3,3)	0.03C004	-0.000000	-C.000011	-0.000000	-0.000000	-C.034403	-C.026228	0.000000	C.164257
BLMD1(4,1)	0.00C002	-C.000003	-C.000000	-0.000000	-0.000000	-C.068036	0.049500	0.000000	0.177864
BLMD1(4,2)	-0.00C000	-0.000000	0.000000	-C.000000	-0.000000	-C.022115	-C.011257	0.000000	C.049118
BLMD1(4,3)	0.00C001	0.000000	-C.000000	0.000000	0.000000	-C.036232	0.161199	-0.000000	-C.826843
BLMD2(1,1)	0.00C000	0.000000	C.000018	C.000000	0.000013	0.003691	0.000000	0.000000	0.003338
BLMD2(1,2)	-0.02C000	-C.000028	-C.000000	-C.000019	0.0:5547	-0.000000	-0.000000	0.11090	-C.000000
BLMD2(1,3)	0.00C000	0.000006	C.000000	0.000004	0.000178	0.000000	C.000000	0.00357	C.000000
BLMD2(2,1)	0.00C000	-0.000004	C.000000	0.000006	-0.016608	C.000000	0.000000	-0.016952	C.000000
BLMD2(2,2)	-0.00C000	-0.000000	-C.000000	0.000004	-C.025441	-0.000000	-0.000000	0.011169	-C.000000
BLMD2(2,3)	0.00C000	-0.000002	C.000000	0.000007	C.030739	0.000000	C.000000	0.43856	C.000000
BLMD2(3,1)	0.00C000	0.000001	C.000000	0.000002	0.003862	0.000000	C.000000	0.019086	C.000000
BLMD2(3,2)	0.00C000	0.000000	0.000000	-0.000001	0.009829	0.000000	C.000000	-0.19101	C.000000
BLMD2(3,3)	0.00C000	C.000003	C.000000	0.000007	0.034405	0.000000	C.000000	0.02629	C.000000
BLMD2(4,1)	-0.00C000	-C.000000	-C.000000	-0.000002	0.068036	-0.000000	-0.000000	-0.094499	-C.000000
BLMD2(4,2)	-0.00C000	-0.000000	-C.000000	-0.000000	-C.022125	-0.000000	-0.000000	0.010257	-C.000000
BLMD2(4,3)	0.00C000	C.000000	0.000000	0.000001	0.036232	0.000000	C.000000	-0.161202	C.000000

MODE	10	11	12	13	14	15	16	17	18
FREQ. GEN. MASS	5.036428 8.5757E 03	R.508293 1.0998E 03	8.508313 1.0998E 03	11.439750 3.0326E 02	11.439828 3.0325E 02	15.147632 5.4905E 02	15.147643 5.4909E 02	21.000449 7.1550E 01	21.000503 7.1551E 01
UL1(1)	-0.000000	0.000000	-C.086099	-0.000000	0.051800	0.000000	-0.104397	-0.008130	-C.000000
UR1(1)	-0.03C000	0.000000	C.029622	-0.000000	0.011374	0.000000	-C.076411	-C.030917	-C.000000
UL1(2)	-0.000000	0.000000	C.029622	-0.000000	0.011374	0.000000	-C.076411	-0.009017	-C.000000
UR1(2)	-0.00C000	0.000000	C.060883	-0.000000	-0.079171	0.000000	-C.063675	-0.033836	-C.000000
UL1(3)	-0.000000	0.000000	C.060883	-0.000000	-C.079171	0.000000	-C.063675	-0.033836	-C.000000
UR1(3)	-0.09C000	0.000000	C.072893	-0.000000	0.014407	0.000000	0.055248	-C.059651	-C.000000
UL1(4)	-0.000000	0.000000	-C.105516	-0.000000	-C.093137	0.000000	0.046749	-C.085333	-C.000000
UR1(4)	0.03C000	-0.000000	C.412152	-0.000000	0.266633	-0.000000	C.204731	-C.184153	C.000000
UL2(1)	-0.185583	-0.086111	-C.000000	-0.051803	-0.000000	-C.1C4392	-C.000000	-0.000000	-C.008130
UR2(1)	0.185522	0.029620	-C.000000	-0.011377	-0.000000	-C.076409	-C.000000	-0.000000	-C.009017
UL2(2)	0.185522	0.029620	-C.000000	-0.011377	-0.000000	-C.076409	-C.000000	-0.000000	-C.033835
UR2(2)	-0.428812	0.060884	-C.000000	0.079169	-0.000000	-C.063674	-0.000000	-0.000000	-C.033835
UL2(3)	0.333667	-0.072894	-C.000000	-0.014405	-0.000000	-C.055248	-C.000000	-0.000000	-C.059651
UR2(3)	0.361162	-0.105517	C.000000	0.093918	0.000000	C.046749	0.000000	0.000000	C.085333
UL2(4)	-1.00C000	C.412153	-C.000000	-C.266635	-0.000000	C.24C731	-C.000000	-0.000000	C.184153
BLMD1(1,1)	0.30C000	-0.000000	C.059999	0.000000	-C.068857	-0.000000	0.205674	0.020528	C.000000
BLMD1(1,2)	-0.00C000	0.000000	C.138532	-0.000000	0.121676	C.000000	-C.305730	-C.24932	C.000000
BLMD1(1,3)	0.00C000	-0.000000	C.064654	0.000000	C.07676	-0.000000	-C.025662	-C.05225	C.000000
BLMD1(2,1)	0.09C030	-0.000000	-C.245662	0.000000	0.075917	-0.000000	C.346413	C.080612	C.000000
BLMD1(2,2)	-0.00C000	0.000000	C.007515	-0.000000	0.04257	0.000000	-C.04906	C.29083	-C.000000
BLMD1(2,3)	0.00C000	-0.000000	-C.072870	0.000000	-C.025595	-0.000000	C.207594	C.18940	C.000000
BLMD1(3,1)	0.09C000	-0.000000	C.093561	0.000000	0.090196	-C.000000	0.022288	0.126232	C.000000
BLMD1(3,2)	0.00C000	-0.000000	C.017513	0.000000	-C.028571	-0.000000	-C.028908	C.10905	C.000000
BLMD1(3,3)	0.00C000	-0.000000	-C.026789	0.000000	0.056833	-0.000000	C.067168	C.32746	C.000000
BLMD1(4,1)	0.00C000	-0.000000	-C.567100	0.000000	-C.6H4957	-0.000000	-C.762760	0.840816	C.000000
BLMD1(4,2)	0.09C000	-0.000000	C.050142	0.000000	-C.038960	-0.000000	C.019249	-C.284200	C.000000
BLMD1(4,3)	0.00C000	0.000000	1.000000	-0.000000	1.000000	C.000000	1.000000	-1.000000	-C.000000
BLMD2(1,1)	0.015105	0.060025	C.000000	0.068875	0.000000	C.2C5697	C.000000	0.000000	C.020532
BLMD2(1,2)	-0.117573	-C.138575	-C.000000	-C.121702	-0.000000	-C.3L5758	-C.000000	-0.000000	-C.024937
BLMD2(1,3)	-0.004160	-C.006449	C.000000	-C.007671	0.000000	-C.029665	0.000000	0.000000	-C.005223
BLMD2(2,1)	-0.135168	-C.245666	C.000000	-C.075911	0.000000	C.346392	C.000000	0.000000	C.080612
BLMD2(2,2)	0.125084	-C.007516	-C.000000	-C.042509	-0.000000	-C.04906	-0.000000	-C.029082	C.018960
BLMD2(2,3)	-0.242321	-C.072873	C.000000	0.025596	0.000000	C.027576	0.000000	0.000000	C.018960
BLMD2(3,1)	0.016926	0.093560	C.000000	-C.08C199	0.000000	C.0C2291	C.000000	0.000000	C.126235

BLMD2(3,2)	-0.015567	-0.017513	C.000000	0.028570	0.000000	-0.028908	0.000000	0.000000	C.010905
BLMD2(3,3)	0.164270	-0.026791	C.000000	-0.056835	0.000000	0.067171	C.000000	0.000000	C.032750
BLMD2(4,1)	0.177880	-0.567099	-0.000000	0.684955	-0.000000	-0.762760	-0.000000	-0.000000	C.840817
BLMD2(4,2)	0.046419	-0.050142	C.000000	0.038560	-0.000000	-0.019249	C.000000	-0.000000	-C.028431
BLMD2(4,3)	-0.826870	1.000000	C.000000	-1.000000	0.000000	1.000000	C.000000	0.000000	-1.000000

MODE	19	20	21	22	23	24	25	26	27
FREQ. GEN. MASS	35.654866 1.9735E 03	35.655149 1.9738E 03	46.702397 3.7335E 02	46.703296 3.7336E 02	51.344742 8.8461E 01	51.344745 8.8462E 01	56.765506 5.0210E 02	56.765777 5.0208E 02	66.781074 1.2120E 02
UL1(1)	-0.069497	-0.000000	-C.027021	0.000000	0.000000	-0.01698	-0.000000	-U.032291	-C.000000
UR1(1)	-0.066758	-0.000000	-U.031702	0.000000	0.000000	-0.01430	-0.000000	-0.017841	-0.000000
UL1(2)	-0.066758	-0.000000	-C.031702	0.000000	0.000000	-0.01430	-0.000000	-0.017841	-C.000000
UR1(2)	-0.005186	-0.000000	-C.056197	0.000000	0.000000	0.005559	-0.000000	0.081369	-C.000000
UL1(3)	-0.005186	-0.000000	-C.056197	0.000000	0.000000	0.066054	-C.000000	0.350049	-C.000000
UR1(3)	-0.074811	-0.000000	-C.097724	0.000000	0.000000	0.053709	C.000000	-0.394646	C.000000
UL1(4)	0.104829	-0.000000	C.031083	0.000000	0.000000	-0.104949	C.000000	0.013840	-C.000000
UR1(4)	0.257928	0.000000	C.120756	-0.000000	-0.000000	0.053709	C.000000	-0.394646	C.000000
UL2(1)	-0.000000	0.069499	-C.000000	-0.027036	-0.001699	-0.000000	0.032306	-0.000000	-C.084412
UR2(1)	-0.000000	0.060763	-C.000000	-0.031705	-0.001431	-0.000000	C.017843	-0.000000	-C.008903
UL2(2)	-0.000000	0.060763	-C.000000	-0.031705	-0.001431	-0.000000	0.017843	-0.000000	-C.008903
UR2(2)	-0.000000	0.09186	-C.000000	-0.056195	C.000000	0.005559	-0.000000	-0.081369	C.012777
UL2(3)	-0.000000	0.09186	-C.000000	-0.097732	0.066052	-0.000000	-C.350051	-0.000000	-C.016777
UR2(3)	-0.000000	0.078817	-C.000000	-0.097732	0.066052	-0.000000	-C.350051	-0.000000	-C.016777
UL2(4)	0.000000	-0.104831	0.000000	0.031085	-0.100499	0.000000	-C.013858	0.000000	-C.001888
UR2(4)	-0.000000	-C.257933	-C.000000	0.120757	0.053711	-0.000000	C.394649	-0.000000	C.016847
BLMD1(1,1)	0.039455	0.000000	0.373464	-0.000000	-0.000000	0.016603	C.000000	0.277787	C.000000
BLMD1(1,2)	0.254767	-0.000000	-C.740801	0.000000	0.000000	-0.029357	C.000000	-0.450900	-C.000000
BLMD1(1,3)	-0.337037	0.000000	C.339944	-0.000000	-0.000000	0.011622	0.000000	0.159773	C.000000
BLMD1(2,1)	0.161950	0.000000	1.000000	-0.000000	-0.000000	0.036910	C.000000	0.310218	C.000000
BLMD1(2,2)	0.805799	-0.000000	C.393671	0.000000	0.000000	0.027186	-C.000000	0.316947	-C.000000
BLMD1(2,3)	-0.641797	0.000000	C.563477	-0.000000	-0.000000	0.013034	C.000000	0.045954	C.000000
BLMD1(3,1)	-0.152607	0.000000	C.098033	-0.000000	-0.000000	0.076550	C.000000	-0.975260	C.000000
BLMD1(3,2)	0.106705	0.000000	C.076755	-0.000000	-0.000000	0.153856	C.000000	-0.360313	C.000000
BLMD1(3,3)	-0.401733	0.000000	-0.114620	-0.000000	-0.000000	-0.08124	0.000000	-0.319976	C.000000
BLMD1(4,1)	-1.000000	0.000000	-0.240842	-0.000000	-0.000000	-1.000000	1.000000	0.616679	C.000000
BLMD1(4,2)	0.301672	0.000000	C.246387	-0.000000	-0.000000	-0.022962	C.000000	-1.000000	C.000000
BLMD1(4,3)	0.901281	-0.000000	C.079515	0.000000	C.935965	-0.000000	0.191026	-C.000000	
BLMD2(1,1)	0.000000	-0.039468	0.000000	0.373582	0.016612	0.000000	-0.277913	0.000000	0.680644
BLMD2(1,2)	-0.000000	-0.254776	-C.000000	-0.740972	-0.029371	-0.000000	C.451084	-0.000000	-1.000000
BLMD2(1,3)	0.000000	0.337063	0.000000	0.339995	C.11627	0.000000	-C.159831	0.000000	C.314693
BLMD2(2,1)	0.000000	-0.162003	0.000000	1.000000	0.036916	0.000000	-0.310149	0.000000	-0.635450
BLMD2(2,2)	-0.000000	-0.805788	-C.000000	0.393699	0.027190	-0.000000	-0.316937	-0.000000	C.157875
BLMD2(2,3)	0.000000	0.641830	0.000000	0.5430449	0.013036	0.000000	-0.045897	0.000000	-C.469643
BLMD2(3,1)	0.000000	0.152608	C.000000	0.098055	0.076554	C.000000	0.975257	0.000000	C.076793
BLMD2(3,2)	0.000000	-0.106707	C.000000	0.076754	0.153857	C.000000	0.360314	0.000000	C.016137
BLMD2(3,3)	0.000000	0.401743	C.000000	-0.114600	-0.008124	0.000000	0.315967	C.000000	C.062803
BLMD2(4,1)	-0.000000	1.000000	-C.000000	-0.240798	-1.000000	-0.000000	-C.616692	-0.000000	C.007415
BLMD2(4,2)	-0.000000	-0.301685	-C.000000	0.246402	-0.022958	-0.000000	1.000000	-0.000000	C.054416
BLMD2(4,3)	0.000000	-0.901273	0.000000	0.079459	0.935962	0.000000	-C.191011	0.000000	-C.053119

MODE	28	29	30	31	32	33	34	35	36
FREQ. GEN. MASS	66.785509 1.2119E 02	133.418671 1.3345E 00	133.418676 1.3345E 00	217.624826 5.1401E_00	217.624975 5.1402E 00	1457.667622 4.4375E 02	1528.753159 4.4376E 02	1955.047623 1.7706E 02	2092.325165 1.7708E 02
UL1(1)	-0.084411	0.000000	-0.000033	0.000123	0.000000	-0.040876	-C.000000	-0.075139	C.000000
UR1(1)	-0.029607	0.000000	-C.000024	0.000017	0.000000	C.040345	-C.000000	C.17157	C.000000
UL1(2)	-0.008907	0.000000	-0.000024	0.000017	0.000000	-0.040345	-0.000000	0.017157	C.000000
UR1(2)	0.012780	0.000000	C.001908	-0.006039	0.000000	-0.071744	-0.000000	C.000346	C.000000
UL1(3)	0.012780	0.000000	C.001908	-0.006039	0.000000	-0.071744	-0.000000	0.000346	C.000000
UR1(3)	-0.016767	0.000000	0.004822	-0.010042	0.000000	0.030228	-0.000000	-0.011432	C.000000
UL1(4)	-0.001888	0.000000	-0.017171	-0.006280	0.000000	-0.000176	-0.000000	0.000003	C.000000
UR1(4)	0.016820	-0.000000	C.006379	A.040792	0.000000	C.000445	0.000000	0.000021	-C.000000
UL2(1)	-0.000000	0.000033	-0.000000	-0.000000	-0.0000123	-0.000000	-0.040869	-0.000000	C.075139
UR2(1)	-0.000000	0.000024	-0.000000	-0.000000	-0.0000017	-0.000000	0.040341	-0.000000	-C.017161
UL2(2)	-0.000000	0.000024	-0.000000	-0.000000	-0.0000017	-0.000000	0.046341	-0.000000	-C.017161
UR2(2)	-0.000000	-0.000000	-0.000000	-0.000000	C.006038	-0.000000	-0.071753	-0.000000	-C.000037
UL2(3)	-0.000000	-0.000000	-0.000000	-0.000000	0.010042	-0.000000	0.030221	-0.000000	0.011430
UR2(3)	-0.000000	-0.000000	-0.000000	-0.000000	0.010042	-0.000000	-0.071753	-0.000000	-C.000037
UL2(4)	0.000000	0.017171	C.000000	-0.000000	0.006280	0.000000	-C.000188	0.000000	-C.000003
UR2(4)	-0.000000	-0.063706	-C.000000	-0.000000	-0.040793	-0.000000	0.006496	-0.000000	-C.000019
BLMD1(1,1)	0.686633	-0.000000	C.000220	-0.000080	-0.000000	0.324243	C.000000	0.551871	-C.000000
BLMD1(1,2)	-1.000000	0.000000	-C.000311	0.001161	0.000000	-0.386533	-0.000000	-0.699443	C.000000
BLMD1(1,3)	0.314699	-0.000000	0.000078	-0.000283	-0.000000	0.095091	0.000000	0.168310	-C.000000
BLMD1(2,1)	-0.635343	-0.000000	C.001659	-0.002491	-0.000000	-1.000000	0.000000	1.000000	-C.000000
BLMD1(2,2)	-0.157813	0.000000	C.002807	-0.007579	0.000000	-0.785196	-0.000000	0.314040	C.000000
BLMD1(2,3)	-0.466599	-0.000000	0.000010	0.000795	-0.000000	-0.248286	C.000000	0.49986	-C.000000
BLMD1(3,1)	-0.076765	-0.000000	C.032877	0.121189	-0.000000	-0.270340	0.000000	0.065226	-C.000000
BLMD1(3,2)	0.016128	-0.000000	C.023888	0.098365	-0.000000	-0.060908	0.000000	0.022688	-C.000000
BLMD1(3,3)	0.062791	-0.000000	C.006301	0.021014	-0.000000	-0.249111	0.000000	0.41761	-C.000000
BLMD1(4,1)	0.007422	-0.000000	0.667236	0.730805	-0.000000	0.003432	0.000000	0.000582	-C.000000
BLMD1(4,2)	0.054390	-0.000000	C.038978	0.325269	-0.000000	0.024644	C.000000	0.002124	-C.000000
BLMD1(4,3)	-0.053108	0.000000	-1.000000	-1.000000	0.000000	-0.05608	-C.000000	-0.000752	C.000000
BLMD2(1,1)	0.000000	-0.000221	0.000000	0.000000	0.000880	0.000000	0.324168	0.000000	C.551868
BLMD2(1,2)	-0.000000	0.000312	-C.000000	-0.0000					

BLMD2(3,1)	0.03000	0.032877	0.00000	0.00000	-0.121191	0.00000	-0.276284	0.00000	-0.065210
BLMD2(3,2)	0.03000	0.023888	0.00000	0.00000	-0.098366	0.00000	-0.060865	0.00000	-0.022674
BLMD2(3,3)	0.00000	0.006301	0.00000	0.00000	-0.021016	0.00000	-0.265105	0.00000	-0.041759
BLMD2(4,1)	-0.09000	-0.667236	-0.00000	-0.00000	-0.730804	-0.00000	0.004114	-0.00000	-0.000528
BLMD2(4,2)	-0.09000	-0.389789	-0.00000	-0.00000	-0.325270	0.00000	0.002817	-0.00000	0.000195
BLMD2(4,3)	0.00000	1.00000	0.00000	0.00000	1.00000	0.00000	-0.006588	0.00000	0.000682

ACCURACY CHECK MATRICES FOLLOW

RMEGA**2*a*x

COLUMN(1)	COLUMN(2)	COLUMN(3)	COLUMN(4)	COLUMN(5)	COLUMN(6)	COLUMN(7)	COLUMN(8)	COLUMN(9)	COLUMN(10)	
RW(1,1)	-6.2508E 0C	0.0000E-39	-4.1189E 01	0.0000E-39	0.0000E-39	-4.4635E C5	-6.2077E 05	-0.0CC0E-39	-3.1918E 06	-0.0000E-39
RW(1,2)	-4.7710E 01	0.0000E-39	-2.522CE 01	0.0000E-39	0.0000E-39	0.6712E C5	1.2215E 06	-0.0CC0E-39	7.357CE 06	-0.0000E-39
RW(1,3)	-4.5258E 01	0.0000E-39	1.2832E 00	0.0000E-39	0.0000E-39	3.548BE C5	-1.7279E 05	-0.0CC0E-39	-7.975E 06	-0.0000E-39
RW(1,4)	-3.3006E 01	0.0000E-39	3.7031E 00	0.0000E-39	0.0000E-39	-2.C56EE C5	-7.7877E 05	-0.0CC0E-39	2.1215E 06	-0.0000E-39
RW(1,5)	-9.9966E 0C	0.0000E-39	1.2947E 00	0.0CC0E-39	0.0000E-39	-1.7431E C5	-2.8937E 04	-0.0000E-39	2.1291E 06	-0.0000E-39
RW(1,6)	-5.1960E 0C	0.0000E-39	7.6545E-01	0.0CC0E-39	0.0CC0E-39	-1.9170E C5	3.7575E 05	-0.0000E-39	-4.4506E 05	-0.0000E-39
RW(1,7)	0.0300E-39	-5.5326E 01	0.0CC0E-39	1.4712E 01	4.4633E 05	0.0CC0E-39	C.0000E-39	6.2C78E 05	0.0000E-39	3.192CE 06
RW(1,8)	0.0000E-35	-4.3593E 01	0.0000E-39	-1.0385E 01	-6.6708E 05	0.0CC0E-39	0.0CC0E-36	-1.2215E 06	0.0000E-39	7.3574E 06
RW(1,9)	0.0000E-35	-8.3416E 00	0.0000E-39	-2.0545E 01	-3.5486E 05	0.0CC0E-39	C.0000E-39	1.7279E 05	0.0000E-39	-7.9712E 06
RW(1,10)	0.0000E-35	-2.4592E 00	0.0000E-39	-1.6157E 01	2.0967E C5	0.0CC0E-39	0.0CC0E-39	7.7881E 05	0.0000E-39	2.1292E 06
RW(1,11)	-0.0000E-35	-5.1803E-01	-0.0000E-39	-4.9668E 00	1.7431E 05	-0.0CC0E-39	-0.0CC0E-39	2.8947E 04	-0.0000E-39	2.1218E 06
RW(1,12)	-0.0000E-35	-1.4813E-01	-0.0000E-39	-2.6208E 00	1.9170E C5	-0.0CC0E-39	-0.0CC0E-36	3.7975E 05	-0.0000E-39	4.4506E 05
RW(1,13)	1.3558E 01	0.0000E-39	2.3779E 01	0.0000E-39	0.0000E-39	2.1841E C5	-1.6C94E 05	-0.0CC0E-39	-4.21CE 06	-0.0000E-39
RW(1,14)	1.4484E 01	0.0000E-39	3.1825E 01	0.0000E-39	0.0000E-39	9.7453E C4	-4.1911E 04	-0.0000E-39	3.4003E 06	-0.0000E-39
RW(1,15)	1.4552E 01	0.0000E-39	3.8064E 01	0.0000E-39	0.0000E-39	1.8799E C5	1.0C7CE 05	-0.0000E-39	-2.4283E 06	-0.0000E-39
RW(1,16)	-3.2061E 01	0.0000E-39	-2.2961E 00	0.0000E-39	0.0000E-39	4.9840E C5	5.3115E 05	-0.0000E-39	-3.6133E 06	-0.0000E-39
RW(1,17)	3.0158E 01	0.0000E-39	1.6944E 00	0.0000E-39	0.0000E-39	-4.5800E 05	4.4681E 05	-0.0000E-39	4.2063E 06	-0.0000E-39
RW(1,18)	3.3026E 01	0.0000E-39	2.6197E 00	0.0000E-39	0.0000E-39	5.2C78E C5	-5.8005E 05	-0.0000E-39	3.2515E 06	-0.0000E-39
RW(1,19)	-3.3913E 01	0.0000E-39	3.6343E 00	0.0000E-39	0.0000E-39	-1.4696E 05	7.2553E 05	-0.0000E-39	1.0124E 05	0.0000E-39
RW(1,20)	3.0466E 01	0.0000E-39	-3.3263E 00	0.0000E-39	0.0000E-39	1.3584E C5	7.2514E 05	-0.0000E-39	-3.2226E 05	-0.0000E-39
RW(1,21)	2.8134E 01	0.0000E-39	-2.9753E 00	0.0000E-39	0.0000E-39	9.0201E C4	6.4717E 05	-0.0000E-39	7.9018E 05	-0.0000E-39
RW(1,22)	6.6898E 0C	0.0000E-39	-9.32C5E-01	0.0000E-39	0.0000E-39	1.7701E C5	-1.4941E 05	-0.0000E-39	-9.6505E 05	-0.0000E-39
RW(1,23)	6.8250E 0C	0.0000E-39	-9.7473E-01	0.0000E-39	0.0000E-39	2.1061E C5	-3.1608E 05	-0.0000E-39	-3.8635E 05	-0.0000E-39
RW(1,24)	6.9580E 0C	0.0000E-39	-9.7462E-01	0.0000E-39	0.0000E-39	1.9094E 05	-2.2206E 05	-0.0000E-39	-8.5857E 05	-0.0000E-39
RW(1,25)	0.0000E-39	3.4158E 01	0.0000E-39	-4.1012E 01	-2.1884E 05	0.0000E-39	0.0000E-39	5.2C78E 05	0.0000E-39	-4.2109E 06
RW(1,26)	0.0000E-35	4.4890E 01	0.0000E-39	-4.1012E 01	-2.1884E 05	0.0000E-39	0.0000E-39	1.8C54E 05	0.0000E-39	-4.2109E 06
RW(1,27)	0.0000E-35	5.3073E 01	0.0000E-39	-9.7133E 00	-1.8798E C4	0.0000E-39	0.0000E-39	4.19C7E 04	0.0000E-39	-3.4006E 06
RW(1,28)	0.0000E-35	-1.0107E 01	0.0000E-39	-1.3195E 01	-4.9838E C5	0.0000E-39	0.0000E-39	-1.0C70E 05	0.0000E-39	-2.4285E 06
RW(1,29)	0.0000E-35	8.8595E 00	0.0000E-39	1.2609E 01	4.5798E C5	0.0000E-39	0.0000E-39	5.3117E 05	0.0000E-39	-3.6135E 06
RW(1,30)	0.0000E-35	1.0744E 01	0.0000E-39	1.3494E 01	5.2076E 05	0.0000E-39	0.0000E-39	5.BC7CE 05	0.0000E-39	3.2514E 06
RW(1,31)	0.0000E-35	-2.7550E 00	0.0000E-39	-1.6528E 01	4.4697E C5	0.0000E-39	0.0000E-39	7.8565E 05	0.0000E-39	1.0112E 05
RW(1,32)	0.0000E-35	2.4788E 00	0.0000E-39	1.5051E 01	-1.3985E C5	0.0000E-39	0.0000E-39	-7.2517E 05	0.0000E-39	-3.2211E 05
RW(1,33)	0.0000E-35	2.3334E 00	0.0000E-39	1.3695E 01	-9.8208E 04	0.0000E-39	0.0000E-39	6.4721E 05	0.0000E-39	7.9038E 05
RW(1,34)	0.0000E-35	2.6053E 01	0.0000E-39	3.3512E 00	-1.7701E 05	0.0000E-39	0.0000E-39	1.8451E 05	0.0000E-39	-9.6511E 05
RW(1,35)	0.0000E-35	2.3477E-01	0.0000E-39	3.6295E 00	-2.1061E C5	0.0000E-39	0.0000E-39	3.1668E 05	0.0000E-39	-3.8635E 05
RW(1,36)	0.0000E-35	2.6438E-01	0.0000E-39	3.4882E 00	-1.9094E 05	0.0000E-39	0.0000E-39	2.2206E 05	0.0000E-39	-8.5863E 05

COLUMN(11)	COLUMN(12)	COLUMN(13)	COLUMN(14)	COLUMN(15)	COLUMN(16)	COLUMN(17)	COLUMN(18)	COLUMN(19)	COLUMN(20)	
RW(1,1)	0.0000E-39	-9.6332E 05	-0.0CC0E-39	-1.81C9E 05	0.0CC0E-39	2.3367E C6	3.5894E 05	-0.0CC0E-39	3.068CE 06	-0.0000E-39
RW(1,2)	0.0000E-39	1.8047E 06	-0.0CC0E-39	6.5973E 05	0.0000E-39	-4.4298E C6	-5.C217E 05	-0.0CC0E-39	-3.8054E 06	-0.0000E-39
RW(1,3)	0.0000E-39	-7.2391E 05	-0.0CC0E-39	-1.L9890E 06	0.0000E-39	7.6768E C5	-2.C691E 05	-0.0CC0E-39	-5.9424E 06	-0.0000E-39
RW(1,4)	0.0000E-35	2.8968E 06	-0.0CC0E-39	4.0461E 06	0.0000E-39	2.3314E C6	3.4235E 04	-0.0CC0E-39	-1.621CE 07	-0.0000E-39
RW(1,5)	0.0000E-39	-2.3123E 05	-0.0CC0E-39	-2.0849E 06	0.0000E-39	-4.7153E C5	-3.5381E 06	-0.0CC0E-39	2.2044E 07	-0.0000E-39
RW(1,6)	0.0000E-35	-2.3123E 05	-0.0CC0E-39	-4.5076E 05	0.0000E-39	-5.3461E C5	4.6475E 05	-0.0000E-39	8.5212E 05	-0.0000E-39
RW(1,7)	-9.6331E 05	0.0000E-39	1.8121E 05	0.0000E-39	2.3369E C4	0.0000E-39	0.0000E-39	3.5856E 05	0.0000E-39	-3.0664E 06
RW(1,8)	1.8048E 06	0.0000E-39	-6.5985E 05	0.0000E-39	-4.4299E 06	0.0000E-39	0.0000E-39	-5.0222E 05	0.0000E-39	3.8059E 06
RW(1,9)	-7.2393E 05	0.0000E-39	1.589CE 06	0.0000E-39	7.6790E 05	0.0000E-39	0.0000E-39	-2.0688E 05	0.0000E-39	5.9435E 06
RW(1,10)	2.8968E 06	0.0000E-39	-4.4691E 06	0.0000E-39	2.3315E 06	0.0000E-39	0.0000E-39	3.4236E 06	0.0000E-39	1.6216E 07
RW(1,11)	-2.7832E 05	-0.0000E-39	2.0852E 06	0.0000E-39	-4.7154E 05	-0.0000E-39	0.0000E-39	-5.3462E 06	-0.0000E-39	-2.2045E 07
RW(1,12)	-2.3123E 05	-0.0000E-39	4.5076E 05	0.0000E-39	-5.3461E C5	-0.0000E-39	0.0000E-39	4.6475E 05	0.0000E-39	-8.5218E 05
RW(1,13)	0.0000E-39	-6.6074E 06	0.0000E-39	6.0872E 06	0.0000E-39	-1.4340E C7	-6.8452E 05	0.0000E-39	7.14CCE 07	-0.0000E-39

RW(14)	0.0000E-35	-6.3404E 06	-0.0CCCE-39	6.2797E 06	0.0000E-39	-1.6412E 07	-1.2166E 06	-0.0CCOE-39	3.491EE 07	-0.0000CE-39	
RW(15)	0.0000E-35	-5.9532E 06	-0.0CCCE-39	6.5959E 06	0.0000E-39	-2.0192E 07	-2.2787E 06	-0.0CCOE-39	-4.8877E 07	-0.0000CF-39	
RW(16)	0.0000E-35	-7.1613E 06	-0.0CCCE-39	2.4209E 05	0.0000E-39	9.5394E 06	2.4162E 06	-0.0CCOE-39	1.6394E 07	-0.0000E-39	
RW(17)	0.0000E-35	6.8661E 06	-0.0CCCE-39	-1.7292E 06	0.0000E-39	-1.0494E 07	-1.5439E 06	-0.0CCOE-39	1.6067E 07	-0.0000E-39	
RW(18)	0.0000E-35	7.3315E 06	-0.0CCCE-39	-2.8430E 06	0.0000E-39	-8.8679E 06	-2.6689E 06	-0.0CCOE-39	-3.7466E 07	-0.0000E-39	
RW(19)	0.0000E-35	4.4731E 06	-0.0CCCE-39	3.1313E 06	0.0000E-39	-1.0619E 06	5.5229E 06	-0.0CCOE-39	1.8577E 07	-0.0000E-39	
RW(20)	0.0000E-35	-6.1253E 06	-0.0CCCE-39	-3.3064E 06	0.0000E-39	3.9737E 05	-5.588CE 06	-0.0CCOF-39	-6.2173E 06	-0.0000CE-39	
RW(21)	0.0000E-35	-4.3128E 06	-0.0CCCE-39	-1.7562E 06	0.0000E-39	3.1807E 06	-4.6957E 06	-0.0CCOE-39	-7.0326E 07	-0.0000CE-39	
RW(22)	0.0000E-35	2.0736E 06	-0.0CCCE-39	2.2268E 06	0.0000E-39	2.0861E 06	-1.3295E 06	-0.0CCOE-39	-5.4855E 06	-0.0000CE-39	
RW(23)	0.0000E-35	1.5335E 06	-0.0CCCE-39	1.8819E 06	0.0000E-39	2.6808E 06	-2.1828E 06	-0.0CCOE-39	1.0822E 06	-0.0000CE-39	
RW(24)	0.0000E-35	2.0165E 06	-0.0CCCE-39	2.2278E 06	0.0000E-39	2.1799E 06	-1.6515E 06	-0.0CCOE-39	-3.6014E 06	-0.0000E-39	
RW(25)	-6.6089E 06	0.0000E-39	-6.0871E 06	0.0000E-39	-1.4338E 07	0.0000E-39	0.0000E-39	6.8442E 05	0.0000E-39	-7.1409E 07	
RW(26)	-6.3411E 06	0.0000E-39	-6.2757E 06	0.0000E-39	-1.6411E 07	0.0000E-39	0.0000E-39	-2.1266E 06	0.0000E-39	-3.4921E 07	
RW(27)	-5.9539E 06	0.0000E-39	-6.5956E 06	0.0000E-39	-2.0190E 07	0.0000E-39	0.0000E-39	2.2778E 06	0.0000E-39	4.8881E 07	
RW(28)	-7.1613E 06	0.0000E-39	-6.2404E 06	0.0000E-39	-9.5394E 06	0.0000E-39	3.9737E 05	-5.588CE 06	-0.0CCOF-39	-6.2173E 06	-0.0000CE-39
RW(29)	6.8662E 06	0.0000E-39	1.7286E 06	0.0000E-39	-1.0495E 07	0.0000E-39	0.0000E-39	2.4169E 06	0.0000E-39	-1.6393E 07	
RW(30)	7.3316E 06	0.0000E-39	2.8442E 06	0.0000E-39	-8.8679E 06	0.0000E-39	0.0000E-39	-1.9440E 06	0.0000E-39	-1.6069E 07	
RW(31)	4.4731E 06	0.0000E-39	-3.1314E 06	0.0000E-39	-1.0619E 06	0.0000E-39	0.0000E-39	2.6650E 06	0.0000E-39	3.7463E 07	
RW(32)	-4.1255E 06	0.0000E-39	3.3064E 06	0.0000E-39	3.9736E 05	0.0000E-39	0.0000E-39	5.8029E 06	0.0000E-39	-1.858CE 07	
RW(33)	-4.3128E 06	0.0000E-39	1.7563E 06	0.0000E-39	3.1808E 06	0.0000E-39	0.0000E-39	4.6955E 06	0.0000E-39	6.2187E 06	
RW(34)	2.0736E 06	0.0000E-39	-2.2248E 06	0.0000E-39	2.0881E 06	0.0000E-39	0.0000E-39	-1.3255E 06	0.0000E-39	5.4861E 06	
RW(35)	1.5335E 06	0.0000E-39	-1.8815E 06	0.0000E-39	2.0898E 06	0.0000E-39	0.0000E-39	-2.1282E 06	0.0000E-39	-1.0826E 06	
RW(36)	2.0165E 06	0.0000E-39	-2.2278E 06	0.0000E-39	2.1799E 06	0.0000E-39	0.0000E-39	-1.6515E 06	0.0000E-39	3.6016E 06	

COLUMN(21)	COLUMN(22)	COLUMN(23)	COLUMN(24)	COLUMN(25)	COLUMN(26)	COLUMN(27)	COLUMN(28)	COLUMN(29)	COLUMN(30)	
RW(1)	4.2611E 06	0.0000E-39	0.0000CE-39	1.8857E 05	-0.0L00E-39	2.7529E 06	-C.0CCCDE-39	3.5457E 06	0.00CE-39	-1.2023E 04
RW(2)	-4.1094E 06	0.0000E-39	0.0000CE-39	-2.6764E 05	-0.0C00E-39	-4.9943E 06	C.-0CCCDE-39	-8.5366E 06	0.0000CE-39	-1.5677E 04
RW(3)	-4.8649E 06	0.0000E-39	0.0000CE-39	1.2067E 06	-0.0000E-39	-7.8393E 06	C.-0CCCDE-35	1.0744E 07	0.0000CE-39	6.0517E 05
RW(4)	-9.7352E 06	0.0000E-39	0.0000CE-39	2.4214E 07	-0.0600E-39	5.1345E 07	C.-0CCCDE-39	-7.5171E 06	0.0000CE-39	2.0717E 06
RW(5)	1.5227E 07	0.0000E-39	0.0000CE-39	-2.7436E 07	-0.0000E-39	-3.3659E 07	C.-0CCCDE-39	1.4169E 06	0.0000CE-39	-3.1641E 06
RW(6)	1.2215E 06	0.0000E-39	0.0000CE-39	2.0943E 06	-0.0000E-39	-7.5920E 06	C.-0CCCDE-39	3.9066E 05	0.0000CE-39	5.1488E 05
RW(7)	0.0000E-35	4.2611E 06	1.8974E 05	0.0000E-39	-2.7934E 06	0.0000CE-39	3.5484E 06	0.0000CE-39	1.2033E 04	0.0000CE-39
RW(8)	0.0000E-35	-6.1108E 06	-6.1775E 05	0.0000CE-39	4.9955E 06	0.0000CE-39	-3.5392E 06	0.0000CE-39	1.5638E 04	0.0000CE-39
RW(9)	0.0000E-35	-4.8637E 06	1.2067E 06	0.0000CE-39	7.8151E 06	0.0000CE-39	-1.7373E 07	0.0000CE-39	-6.0504E 05	0.0000CE-39
RW(10)	0.0000E-35	-9.7367E 06	2.4213E 07	0.0000CE-39	5.1345E 07	0.0000CE-39	-7.5192E 06	0.0000CE-39	-2.0718E 06	0.0000CE-39
RW(11)	-0.C00E-35	1.5228E 07	-2.7436E 07	0.0000CE-39	3.3660E 07	0.0000CE-39	-1.422CE 06	-0.0000E-39	3.1641E 06	-0.0000CE-39
RW(12)	-0.3300E-15	1.2215E 06	2.0943E 06	-0.0000E-39	7.5922E 06	-0.0000CE-39	3.5588E 05	-0.0000CE-39	-5.1488E 05	-0.0000CE-39
RW(13)	-7.5843E 07	0.0000E-39	0.0000CE-39	-2.2340E 06	0.0000E-39	-1.2488E 07	C.-0CCCDE-39	1.3848E 07	0.0000E-39	1.3031E 05
RW(14)	-4.9293E 07	0.0000E-39	0.0000CE-39	-1.5485E 06	0.0000CE-39	-1.6101E 07	C.-0CCCDE-39	1.5353E 06	0.0000CE-39	8.4135E 04
RW(15)	2.3758E 07	0.0000E-39	0.0000CE-39	6.4672E 05	0.0000E-39	7.6705E 06	C.-0CCCDE-39	1.6957E 07	0.0000CE-39	2.3772E 04
RW(16)	1.8393E 07	0.0000E-39	0.0000CE-39	6.8583E 05	0.0000E-39	6.8066E 06	C.-0CCCDE-39	2.8619E 06	0.0000E-39	-1.8029E 05
RW(17)	-1.3815E 07	0.0000E-39	0.0000CE-39	1.3650E 05	-0.0000E-39	7.3128E 06	C.-0CCCDE-39	6.6374E 05	0.0000CE-39	5.4122E 05
RW(18)	-1.4260E 07	0.0000E-39	0.0000CE-39	-7.6813E 05	-0.0000E-39	-1.1160E 07	C.-0CCCDE-39	-1.8437E 07	0.0000CE-39	1.812CE 05
RW(19)	2.1175E 07	0.0000E-39	0.0000CE-39	1.5133E 06	-0.0000E-39	-3.0672E 07	C.-0CCCDE-39	-6.6157E 06	0.0000CE-39	3.4312E 05
RW(20)	-1.5205E 07	0.0000E-39	0.0000CE-39	9.4670E 05	-0.0000E-39	3.4223E 06	C.-0CCCDE-39	3.222CE 06	0.0000CE-39	-5.895CE 06
RW(21)	-5.2232E 07	0.0000E-39	0.0000CE-39	-3.4868E 06	-0.0000E-39	-5.0462E 06	C.-0CCCDE-39	2.6872E 07	0.0000CE-39	8.0616E 03
RW(22)	-6.1092E 06	0.0000E-39	0.0000CE-39	-1.1338E 07	-0.0000E-39	3.6366E 07	C.-0CCCDE-39	-1.9730E 06	0.0000E-39	-1.9504E 06
RW(23)	-9.2287E 05	0.0000E-39	0.0000CE-39	-4.2818E 06	-0.0000E-39	9.6735E 06	C.-0CCCDE-39	-5.6202E 06	0.0000CE-39	-3.4325E 05
RW(24)	-6.4656E 06	0.0000E-39	0.0000CE-39	-8.7375E 06	-0.0000E-39	2.8617E 07	C.-0CCCDE-39	-1.5696E 06	0.0000CE-39	-1.6504E 06
RW(25)	0.0000E-39	-7.5843E 07	-2.2309E 06	0.0000E-39	2.0884E 07	0.0000CE-39	-1.3042E 05	0.0000CE-39	-1.3042E 05	0.0000CE-39
RW(26)	0.0000E-39	-4.9293E 07	-1.5488E 06	0.0000E-39	1.6099E 07	0.0000CE-39	1.5191E 06	0.0000CE-39	-8.4212E 04	0.0000CE-39
RW(27)	0.0000E-39	2.3760E 07	6.4747E 05	0.0000E-39	7.3088E 06	0.0000CE-39	-3.6672E 07	0.0000CE-39	-6.6157E 06	0.0000CE-39
RW(28)	0.0000E-39	1.8394E 07	6.8604E 05	0.0000E-39	-6.8071E 07	0.0000CE-39	2.8015E 06	0.0000CE-39	1.8024E 05	0.0000CE-39
RW(29)	0.0000E-39	-1.1380E 07	1.3628E 07	0.0000E-39	-7.3130E 06	0.0000CE-39	6.6735E 05	0.0000CE-39	-5.615CE 05	0.0000CE-39
RW(30)	0.0000E-39	-1.4126E 07	-2.7683E 05	0.0000E-39	1.1162E 07	0.0000CE-39	-1.8427E 07	0.0000CE-39	-1.8116E 05	0.0000CE-39
RW(31)	0.0000E-39	2.1175E 07	2.2175E 06	0.0000E-39	3.0672E 07	0.0000CE-39	-6.6202E 06	0.0000CE-39	-3.4325E 05	0.0000CE-39
RW(32)	0.0000E-39	-1.5205E 07	8.4066E 06	0.0000E-39	-3.4223E 07	0.0000CE-39	3.2205E 06	0.0000CE-39	5.8951E 06	0.0000CE-39
RW(33)	0.0000E-39	-5.2221E 07	-3.4871E 06	0.0000E-39	5.0422E 06	0.0000CE-39	-2.6873E 07	0.0000CE-39	-7.6984E 03	0.0000CE-39
RW(34)	0.0000E-35	-6.1094E 06	-1.1338E 07	0.0000E-39	-3.6365E 07	0.0000CE-39	-1.9730E 06	0.0000CE-39	1.954CE 06	0.0000CE-39
RW(35)	0.0000E-39	-8.2292E 05	-4.2814E 06	0.0000E-39	-9.6766E 06	0.0000CE-39	-5.6570E 05	0.0000CE-39	-9.2284E 05	0.0000CE-39
RW(36)	0.0000E-39	-4.6458E 06	-8.7376E 06	0.0000E-39	-2.8617E 07	0.0000CE-39	-1.5737E 06	0.0000CE-39	1.6504E 06	0.0000CE-39

COLUMN(31)	COLUMN(32)	COLUMN(33)	COLUMN(34)	COLUMN(35)	COLUMN(36)	COLUMN(37)
RW(1)	1.8862E 05	0.0C00E-39	-4.6477E 09	-0.0CC00E-39	-1.1821E 10	0.0CCCE-39
RW(2)	-3.3879E 04	0.0000E-39	1.2324E 10	-0.0000E-39	2.2468E 10	0.0000E-39
RW(3)	-1.0815E 07	0.0000E-39	-2.3080E 09	-0.0000E-39	-6.8475E 09	0.0CCCE-39
RW(4)	1.5550E 07	0.0000E-39	1.4788E 10	-0.0000E-39	-3.8111E 09	0.0CCCE-39
RW(5)	1.0095E 07	0.0000E-39	-1.3464E 07	-0.0000E-39	2.5167E 06	0.0CCCE-39
RW(6)	-0.9731E 06	0.0000E-39	2.9726E 06	-0.0000E-39	-1.1030E 06	0.0CCCE-39
RW(7)	0.0000E-39	-1.8670E 05	0.0000E-39	-4.4736E 09	0.0000CE-39	1.3300E 10
RW(8)	0.0000E-35	3.2529E 04	0.0000CE-39	1.3547E 10	0.0000E-39	-2.4711E 10
RW(9)	0.0000E-35	-1.0813E 07	0.0000CE-39	-2.5393E 12	0.0000E-39	7.5328E 09
RW(10)	0.0000E-39	-1.0548E 07	0.0000CE-39	1.6245E 10	0.0000E-39	4.6818E 09
RW(11)	-0.0000E-39	-1.0496E 07	-0.0000CE-39	-1.4527E 07	-0.0000E-39	-2.515CE 06
RW(12)	-0.0000E-35	9.9732E 06	0.0000CE-39	3.1098E 06	-0.0000E-39	1.109CE 06
RW(13)	-1.850RE 06	0.0000E-39	3.7895E 10	-0.0000E-39	-1.0991E 11	0.0CCCE-39
RW(14)	-3.2344E 05	0.0000E-39	2.5431E 10	-0.0000E-39	7.3818E 10	0.0CCCCE-39
RW(15)	-3.4446E 05	0.0000E-39	6.7477E 09	-0.0000E-39	1.9725E 10	0.0CCOE-39
RW(16)	1.48H5E 06	0.				

Bx VECTORS

	COLUMN(1)	COLUMN(2)	COLUMN(3)	COLUMN(4)	COLUMN(5)	COLUMN(6)	COLUMN(7)	COLUMN(8)	COLUMN(9)	COLUMN(10)
RW1(1)	-4.5053E 01	-0.0000E-39	-2.38C5E 01	-0.0000E-39	-0.0000E-39	-4.4632E C5	-6.2C7E 05	0.0CC0F-39	-3.1917E 06	0.0000E-39
RW1(2)	3.2700E 01	-0.0000E-39	1.58C2E 02	-0.0000E-39	-0.0000E-39	6.6705E C5	1.2214E 06	0.0CC0F-39	7.3567E 06	0.0CCCE-39
RW1(3)	-1.8640E 0C	-0.0000E-39	-8.2432E 01	-0.0000E-39	-0.0000E-39	3.5483E C5	-1.7271E 05	0.0CC0E-39	-7.97C7E 06	0.0000E-39
RW1(4)	1.6195E 01	-0.0000E-39	3.7655E 01	-0.0000E-39	-0.0000E-39	-2.C962E C5	-7.7875E 05	0.0CC0E-39	2.1217E 06	0.0000E-39
RW1(5)	9.3399E 0C	-0.0000E-39	-9.4086E-01	-0.0000E-39	-0.0000E-39	-1.7431E C5	-2.8537E 04	0.0CC0E-39	2.1291E 06	0.0000E-39
RW1(6)	5.0636E 0C	0.0000E-39	-7.5483E-01	0.0000E-39	0.0000E-39	-9.1917E C5	3.7575E 05	-0.0CC0E-39	-4.450E 05	-0.0000E-39
RW1(7)	-2.0000E-39	2.5932E 01	-0.CC0CE-39	-1.9742E 01	4.6630E C5	-0.0CC0E-39	-C.CC0CE-39	6.2C73E 05	-0.0000E-39	-3.191EE 06
RW1(8)	-2.0000E-39	8.073RE 01	-0.0000E-39	7.0441E 01	-6.67C5E C5	-0.0000E-39	-C.CC0CE-39	-1.2215E 06	-0.0000E-39	7.3572E 06
RW1(9)	-0.0000E-39	-5.2766E 01	-0.0000E-39	-7.3389E 01	-3.5477E 05	-0.0000E-39	-C.CC0CE-39	1.7272E 05	-G.0000E-39	-7.9707E 06
RW1(10)	0.0000E-39	-1.5173E 01	0.0000E-39	5.4373E 01	2.0959E 05	0.0000E-39	C.CC0CE-39	7.78BE1E 05	0.0000E-39	2.1216E 06
RW1(11)	0.0000E-39	1.9736E 01	0.0000E-39	-5.8742E 01	1.7431E 05	0.0000E-39	C.CC0CE-39	2.8947E 04	0.0000E-39	2.1292E 06
RW1(12)	-0.0000E-39	1.4653E-01	-0.0000E-39	-2.7180E 00	1.9170E 05	-0.0000E-39	-C.CC0CE-39	-3.7575E 05	-0.0000E-39	-4.450E 05
RW1(13)	6.61R1E 02	-0.0000E-39	8.695CE 02	-0.0000E-39	-9.0600E-39	1.728CE C3	-1.8138E 05	0.0CC0E-39	-4.2117E 06	0.0000E-39
RW1(14)	1.C8R7E 02	-0.0000E-39	3.6958E 02	-0.0000E-39	-9.7472E 05	4.-2.112E 04	0.0CC0E-39	-3.-4.01CE C6	G.CC0CE-39	
RW1(15)	1.C051E 02	-0.0000E-39	5.6495E 01	-0.0000E-39	-9.0600E-39	1.8794E C5	1.0666E 05	0.0CC0E-39	-2.4285E 06	0.0000E-39
RW1(16)	-1.9142E-01	-0.0000E-39	-1.1873E 02	-0.0000E-39	-9.0000E-39	4.9848E C5	5.3127E 05	0.0CC0E-39	-3.6134E 06	0.0000E-39
RW1(17)	3.1754E 01	-0.0000E-39	6.361CE 01	-0.0000E-39	-9.0000E-39	-6.5P1NE C5	-4.46P8E 05	0.0CC0E-39	4.2055E 06	0.0000E-39
RW1(18)	3.6318E 0C	-0.0000E-39	2.4659E 02	-0.0000E-39	-9.0000E-39	-5.2102E C5	5.-5.8C2E 05	0.0CC0E-39	3.2512E 06	0.0000E-39
RW1(19)	3.4287E 01	-0.0000E-39	3.1434E 01	-0.0000E-39	-9.0000E-39	-1.4695E C5	7.-5.656E 05	0.0CC0E-39	1.0085E 05	0.CC0CE-39
RW1(20)	-2.4070E 01	-0.0000E-39	-8.83A1E 00	-0.0000E-39	-9.0000E-39	1.398CE C5	7.2515E 05	0.0CC0E-39	-3.-2.201E 05	0.0000E-39
RW1(21)	-2.4442E 01	-0.0000E-39	-3.735CE 01	-0.0000E-39	-9.0000E-39	9.7945E C5	6.4721E 05	0.0CC0E-39	7.9127E 05	0.0000E-39
RW1(22)	-6.4257E 0C	-0.0000E-39	1.04C3E 00	-0.0000E-39	-9.0000E-39	1.7701E C5	-1.4941E 05	0.0CC0E-39	-9.-6.5CCE 05	0.0000E-39
RW1(23)	-6.9795E 0C	-0.0000E-39	8.929CE 01	-0.0000E-39	-9.0000E-39	-2.1041E C5	-3.1608E 05	0.0CC0E-39	-3.-8.835E 05	0.0000E-39
RW1(24)	-6.3336E 0C	-0.0000E-39	7.5353E 01	-0.0000E-39	-9.0000E-39	1.9C94E C5	-2.2024E 05	0.0CC0E-39	-8.-5.858E C5	0.0000E-39
RW1(25)	-0.0000E-35	4.6496E 02	-0.0000E-39	3.2727E 02	-1.7920E 05	-0.0000E-39	C.CC0CE-39	1.8125E 05	-G.0000E-39	-4.2117E 06
RW1(26)	-0.0000E-39	3.1355E 02	-0.0000E-39	-1.0552E 02	-9.7216E C4	-0.CC0CE-39	C.CC0CE-39	4.2044E 04	-0.0000E-39	-3.4012E 06
RW1(27)	-0.0000E-39	-7.-7.7412E 00	-0.0000E-39	-7.7383E 00	-1.8779E 05	-0.0000E-39	-C.CC0CE-39	-1.0CCE2E 05	-C.0000E-39	-2.4228E 06
RW1(28)	-0.0000E-35	-1.-0.4797E 02	-0.0000E-39	5.7773E 00	-4.9847E C5	-0.0000E-39	-C.CC0CE-35	-5.3124E 05	-0.0000E-39	-3.6133E 06
RW1(29)	-0.0000E-39	8.7250E 01	-0.0000E-39	4.3172E 01	-4.5821E 05	-0.0000E-39	-C.CC0CE-35	5.8C87E 05	-C.0000E-39	3.2512E 06
RW1(30)	-0.0000E-35	2.6225E 02	-0.0000E-39	-1.-3.3747E 00	5.2089E 05	-0.0000E-39	-C.CC0CE-35	-7.858E 05	-0.0000E-39	1.0073E 05
RW1(31)	-0.0000E-39	-1.-3.289E 01	-0.0000E-39	5.0421E 01	-1.4668E 05	-0.0000E-39	-C.CC0CE-39	-7.2517E 05	C.0000E-39	-3.2183E 05
RW1(32)	0.0000E-39	-9.-4.7070E 01	-0.0000E-39	-6.9342E 01	-9.-7.9193E 04	-0.0000E-39	-C.CC0CE-39	-6.4721E 05	G.0000E-39	-7.9115E 05
RW1(34)	0.0000E-39	-1.-9.9999E 01	-0.0000E-39	3.7879E 01	-1.-7.7010E 05	-0.0000E-39	G.0000E-39	1.8491E 05	C.0000E-39	-9.-6.511E 05
RW1(35)	0.0000E-39	-2.2411E 01	0.0000E-39	3.7373E 00	-2.-1.6616E 05	0.0000E-39	-C.CC0CE-35	3.16C7E 05	0.0000E-39	-3.-8.839E 05
RW1(36)	0.0000E-39	-2.6566E 01	0.0000E-39	3.9325E 00	-1.-9.094E 05	0.0000E-39	-C.CC0CE-35	2.22C6E 05	C.0000E-39	-8.-5.856E 05

	COLUMN(11)	COLUMN(12)	COLUMN(13)	COLUMN(14)	COLUMN(15)	COLUMN(16)	COLUMN(17)	COLUMN(18)	COLUMN(19)	COLUMN(20)
RW1(1)	-0.0300E-39	-9.6333E 05	0.0000E-39	-1.8112E 05	-0.0000E-39	2.3369E C6	3.5894E 05	0.0CC0E-39	3.0675E 06	0.0000E-39
RW1(2)	-0.0000E-35	1.8648E 06	0.0000E-39	6.5591E 05	-0.0000E-39	-9.4303E C6	-5.-5.215E 05	0.0CC0F-39	-3.8054E 06	0.0000E-39
RW1(3)	-0.0300E-39	-7.2394E 05	0.3000E-39	-1.9889E 06	-0.0000E-39	7.6785E C5	-2.-6.688E 05	0.0CC0E-39	-5.9424E 06	0.0000E-39
RW1(4)	-0.0300E-39	2.8969E 06	0.0000E-39	4.0461E 06	-0.0000E-39	-2.3314E C6	3.4235E 06	0.0CC0E-39	-1.6216E 07	0.0000E-39
RW1(5)	-0.0000E-39	-2.7832E 06	0.0000E-39	-2.0849E 06	-0.0000E-39	-4.7153E C5	-3.-5.3518E 06	0.0CC0E-39	2.2044E 07	0.0000E-39
RW1(6)	0.0000E-35	-2.3123E 05	-0.0000E-39	-4.5076E 05	0.0000E-39	-5.-3461E C5	4.6475E 05	0.0CC0E-39	8.5212E C5	-0.0000E-39
RW1(7)	-9.-632RE 05	-0.0000E-39	1.8119E 05	-0.0000E-39	2.3368E 06	-0.0000E-39	C.CC0CE-39	3.5895E 05	-G.0000E-39	-3.-6.048E 06
RW1(8)	1.8047E 06	-0.0000E-39	-6.5981E 05	-0.0000E-39	-9.-4.4301E 06	-0.0000E-39	-C.CC0CE-39	-5.-0.0226E 05	-0.0000E-39	3.8061E 06
RW1(9)	-7.2390E 05	-0.0000E-39	1.9894E 05	-0.0000E-39	7.6800E 05	-0.0000E-39	-C.CC0CE-39	-2.-0.064E 05	-0.0000E-39	5.9434E 06
RW1(10)	2.-8.963E 05	0.0000E-39	-4.-0.4616E 06	0.0000E-39	2.3314E 05	0.0000E-39	-C.CC0CE-39	3.-4.324E 06	0.0000E-39	1.6216E 07
RW1(11)	-2.7832E 04	0.0000E-39	2.0850E 05	0.0000E-39	-4.-7.154E 05	0.0000E-39	-C.CC0CE-39	-3.-5.3282E 06	0.0000E-39	-2.2045E 07
RW1(12)	-2.3123E 04	-0.0000E-39	4.57C6E 05	-0.0000E-39	-5.-5.3461E 05	-0.0000E-39	-C.CC0CE-39	6.-4.6755E 05	-0.0000E-39	8.-5.212E 05
RW1(13)	-0.0000E-35	6.-6.6071E 06	0.0000E-39	-6.6073E 06	-0.0000E-39	-1.-4.340E 07	6.-8.454E 05	0.0CC0E-39	7.-1.40CE 07	0.0000E-39
RW1(14)	-0.0000E-35	-6.-6.3452E 06	0.0000E-39	-6.2797E 06	-0.0000E-39	-1.-6.143E 07	7.-1.2166E 06	0.0CC0E-39	3.-4.911E 07	0.0000E-39
RW1(15)	-0.0000E-39	-5.-5.9532E 06	0.0000E-39	-6.5959E 06	-0.0000E-39	-2.-0.0219E 07	7.-2.7878E 06	0.0CC0E-39	-4.-8.877E 07	0.0000E-39
RW1(16)	-0.0000E-39	-7.-16.12E 06	0.0000E-39	-6.4228E 06	-0.0000E-39	-9.-5.9379E 06	2.-4.2428E 06	0.0CC0E-39	2.-4.2428E 06	0.0000E-39
RW1(17)	-0.0000E-39	6.-6.8660E 06	0.0000E-39	-1.-7.289E 06	-0.0000E-39	-1.-1.4956E 07	7.-1.5439E 06	0.0CC0E-39	1.-6.067E 07	0.0000E-39
RW1(18)	-0.0000E-39	7.-3.3131E 06	0.0000E-39	-2.-8.248E 06	-0.0000E-39	-8.-8.684E 06	2.-4.2432E 06	0.0CC0E-39	3.-7.3461E 07	0.0000E-39
RW1(19)	-0.0000E-39	3.-4.4732E 06	0.0000E-39	-6.1313E 06	-0.0000E-39	-9.-1.0621E 07	6.-5.8029E 06	0.0CC0E-39	1.-8.857E 07	0.0000E-39
RW1(20)	-0.0000E-39	-4.-12.53E 06	0.0000E-39	-3.-5.3063E 06	-0.0000E-39	-3.-3.0636E 07	6.-3.9740E 05	0.0CC0E-39	-6.-4.6957E 06	0.0000E-39
RW1(21)	-0.0000E-39	-4.-2.0763E 06	0.0000E-39	-2.-2.2268E 06	-0.0000E-39	-3.-1.7508E 07	6.-3.1608E 06	0.0CC0E-39	-6.-2.173E 06	0.0000E-39
RW1(22)	-0.0000E-39	1.5305E 06	0.0000E-39	-8.-8.684E 06	-0.0000E-39	-2.-2.2278E 06	7.-2.0786E 06	0.0CC0E-39	-5.-5.4855E 06	0.0000E-39
RW1(24)	-0.0000E-39	2.-0.0145E 06	0.0000E-39	-2.0778E 06	-0.0000E-39	-2.-1.7199E 06	1.-1.6515E 06	0.0CC0E-39	-3.-3.6014E 06	0.0000E-39
RW1(25)	-6.-6.084E 06	-0.0000E-39	-6.-6.087EE 06	-0.0000E-39	-9.-1.4338E 07	-0.-0.0000E-39	-C.CC0CE-35	-6.-8.6416E 05	-0.0000E-39	-7.-14.05E 07
RW1(26)	-6.-3415E 06	-0.0000E-39	-6.-6.2758E 06	-0.0000E-39	-1.-1.6410E 07	-0.0000E-39	-C.CC0CE-39	-1.-2.1615E 06	-0.0000E-39	-3.-4.922E 07
RW1(27)	-7.-5.9539E 06	-0.0000E-39	-6.-5.9597E 06	-0.0000E-39	-2.-0.0190E 07	-0.0000E-39	-C.CC0CE-39	-3.-2.2787E 06	-0.0000E-39	4.-8.881E 07
RW1(28)	-7.-1.6121E 06	-0.0000E-39	-2.-4.2424E 06	-0.0000E-39	-5.-5.3979E 06	-0.0000E-39	-C.CC0CE-39	-2.-1.0621E 06	-0.0000E-39	1.-6.3597E 07
RW1(29)	-6.-8.6605E 06	-0.0000E-39	-1.-7.1284E 06	-0.0000E-39	-5.-5.3979E 06	-0.0000E-39	-C.CC0CE-39	-1.-2.0940E 06	-0.0000E-39	1.-6.0606E 07
RW1(30)	-7.-3.3134E 06	-0.0000E-39	-2.-8.248E 06	-0.0000E-39	-8.-8.684E 06	-0.0000E-39	-C.CC0CE-39	-3.-2.		

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RW( 1) 1.8662E 05 -0.0000E-39 -4.674E 09 0.0000E-39 -1.1821E 10 -0.0000E-39
RW( 2) -5.1754E 07 -0.0000E-39 1.24C9E 10 0.0000E-39 2.2468E 10 -0.0000E-39
RW( 3) -1.0892E 07 -0.0000E-39 -2.3125E 10 0.0000E-39 -6.8475E C9 -0.0000E-39
RW( 4) 1.0554E 07 -0.0000E-39 1.4787E 10 0.0000E-39 -3.8011E 09 -0.0000E-39
RW( 5) 1.0293E 07 -0.0000E-39 -6.6878E 06 0.0000E-39 -2.5167E 06 -0.0000E-39
RW( 6) -9.9730E 06 0.0000E-39 2.2537E 06 -0.0000E-39 -1.1103E 06 0.0000E-39
RW( 7) -0.0000E-35 -1.8670E 05 -0.0000E-39 -4.4736E 08 -0.0000E-39 1.3003E 10
RW( 8) -0.0000E-35 5.2490E 04 -0.0000E-39 1.3649E 10 -0.0000E-39 -2.4716E 10
RW( 9) -0.0000E-35 1.0806E 07 -0.0000E-39 -2.5438E 10 -0.0000E-39 7.5328E C9
RW(10) 0.C000E-35 -1.0552E 07 0.0000E-39 1.6266E 10 0.0000E-39 4.1810E C9
RW(11) 0.0000E-35 -1.0093E 07 0.0000E-39 -6.0647E 06 0.0000E-39 -2.5153E C6
RW(12) -0.0000E-35 9.9730E 06 -0.0000E-39 2.2489E 06 -0.0000E-39 1.1090E L6
RW(13) -1.8368E 06 -0.0000E-39 3.7847E 10 0.0000E-39 1.0991E 11 -0.0000E-39
RW(14) -1.2193E 06 -0.0000E-39 2.5416E 10 0.0000E-39 -7.3819E 10 -0.0000E-39
RW(15) -3.2665E 05 -0.0000E-39 6.7055E 09 0.0000E-39 1.9725E 10 -0.0000E-39
RW(16) 1.4853E 04 -0.0000E-39 4.7455E 09 0.0000E-39 -2.8150E 10 -0.0000E-39
RW(17) -3.6012E 05 -0.0000E-39 -3.0742E 10 0.0000E-39 2.9437E 10 -0.0000E-39
RW(18) -1.6605E 07 -0.0000E-39 2.8134E 09 0.0000E-39 4.6644E 10 -0.0000E-39
RW(19) -1.6405E 07 -0.0000E-39 2.2848E 10 0.0000E-39 -5.8739E 09 -0.0000E-39
RW(20) 4.4603E 07 -0.0000E-39 -1.6039E 10 0.0000E-39 4.1275E 09 -0.0000E-39
RW(21) 7.4266E 06 -0.0000E-39 -6.6568E 10 0.0000E-39 1.7116E 10 -0.0000E-39
RW(22) 4.3975E 07 -0.0000E-39 -9.8022E 06 0.0000E-39 4.8287E 06 -0.0000E-39
RW(23) 2.3268E 07 -0.0000E-39 -4.8798E 06 0.0000E-39 2.4116E 06 -0.0000E-39
RW(24) 3.6097E 07 -0.0000E-39 -8.0766E 06 0.0000E-39 3.9794E 06 -0.0000E-39
RW(25) -0.0000E-35 1.8377E 06 -0.0000E-39 4.1622E 10 -0.0000E-39 -1.2090E 11
RW(26) -0.0000E-35 1.2199E 06 -0.0000E-39 2.7951E 10 -0.0000E-39 -8.1119E 10
RW(27) -0.0000E-35 3.2681E 05 -0.0000E-39 7.4680E 09 -0.0000E-39 -2.1698E 10
RW(28) -0.0000E-35 -1.4837E 06 -0.0000E-39 5.2216E 09 -0.0000E-39 3.0966E 10
RW(29) -0.0000E-35 3.5960E 06 -0.0000E-39 -3.3814E 10 -0.0000E-39 -3.238CE 10
RW(30) -0.0000E-35 1.6591E 06 -0.0000E-39 3.0928E 09 -0.0000E-39 -5.1308E 10
RW(31) -0.0000E-35 1.6608E 07 -0.0000E-39 2.5133E 10 -0.0000E-39 6.4609E C9
RW(32) 0.0000E-35 -8.4605E 07 0.0000E-39 -1.7641E 10 0.0000E-39 -4.5390E C9
RW(33) 0.0000E-35 -7.4357E 06 0.0000E-39 -7.3247E 10 0.0000E-39 -1.8826E 10
RW(34) 0.0000E-35 -4.3975E 07 0.0000E-39 -9.7789E 06 0.0000E-39 -4.8232E C6
RW(35) 0.0000E-35 -2.3269E 07 0.0000E-39 -4.8676E 06 0.0000E-39 -2.4088E L6
RW(36) 0.0000E-35 -3.6397E 07 0.0000E-39 -8.0592E 06 0.0000E-39 -3.9749E C6

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BMEGA**2*A*X - B*X VECTORS

COLUMN(1)	COLUMN(2)	COLUMN(3)	COLUMN(4)	COLUMN(5)	COLUMN(6)	COLUMN(7)	COLUMN(8)	COLUMN(9)	COLUMN(10)																										
RW(1) 3.9612E 01 0.0000E-39 1.7385E 01 0.0000E-39 0.0000E-39 2.7742E C1 1.3031E 01 0.0000E-39 8.2375E 01 0.0000E-39	RW(2) 8.0410E 01 0.0000E-39 1.8324E 01 0.0000E-39 0.0000E-39 6.7680E C1 1.2406E 02 0.0000E-39 3.0475E 02 0.0000E-39	RW(3) 4.3394E 01 0.0000E-39 8.3715E 01 0.0000E-39 0.0000E-39 4.9508E C1 7.4596E 01 0.0000E-39 2.3912E 02 0.0000E-39	RW(4) 4.9201E 01 0.0000E-39 3.3956E 01 0.0000E-39 0.0000E-39 4.33559E C1 1.5266E 01 0.0000E-39 1.8034E 02 0.0000E-39	RW(5) 1.9396E 01 0.0000E-39 2.2356E 00 0.0000E-39 0.0000E-39 6.8359E-C2 3.7786E-01 0.0000E-39 0.0000E-39 0.0000E-39	RW(6) 1.0260E 01 0.0000E-39 1.52C3E 00 0.0000E-39 0.0000E-39 2.5391E-C2 3.750CE-01 0.0000E-39 7.6953E-01 0.0000E-39	RW(7) 0.0000E-35 8.1258E 01 0.0000E-39 3.6445E 01 0.0000E-39 6.2853E v1 0.0000E-39 0.0000E-39 4.8336E 01 0.0000E-39 1.5028E 02	RW(8) 0.0000E-35 1.2433E 02 0.0000E-39 8.0827E 01 3.2469E 01 0.0000E-39 0.0000E-39 7.9042E 01 0.0000E-39 2.1056E 02	RW(9) 0.0000E-35 4.4624E 01 0.0000E-39 5.2844E 01 0.0000E-39 0.0000E-39 0.0000E-39 6.2450E C1 0.0000E-39 5.1665E 02	RW(10) 0.0000E-35 9.4192E-01 0.0000E-39 1.4700E 01 0.0000E-39 0.0000E-39 0.0000E-39 6.5625E-01 0.0000E-39 2.4844E 02	RW(11) 0.0000E-35 6.2539E-01 0.0000E-39 9.0741E-01 2.7148E-01 0.0000E-39 0.0000E-39 7.9590E-02 0.0000E-39 4.3750E-01	RW(12) 0.0000E-35 2.8866E-01 0.0000E-39 9.7154E-02 8.2031E-02 0.0000E-39 0.0000E-39 0.0000E-39 0.0000E-39 1.0273E 00	RW(13) 6.4825E 01 0.0000E-39 8.4533E 02 0.0000E-39 0.0000E-39 4.5612E 02 4.3651E 02 0.0000E-39 1.1344E 03 0.0000E-39	RW(14) 9.4391E 01 0.0000E-39 3.3775E 02 0.0000E-39 0.0000E-39 1.8587E 01 2.099E 02 0.0000E-39 6.2366E 02 0.0000E-39	RW(15) 8.5947E 01 0.0000E-39 1.6632E 01 0.0000E-39 0.0000E-39 4.4521E 01 4.0134E 01 0.0000E-39 2.6434E 02 0.0000E-39	RW(16) 3.1870E 01 0.0000E-39 1.1644E 02 0.0000E-39 0.0000E-39 7.6586E 01 1.2321E 02 0.0000E-39 1.5628E 02 0.0000E-39	RW(17) 1.5959E 0C 0.0000E-39 6.1916E 01 0.0000E-39 0.0000E-39 1.7858E C2 7.2288E 01 0.0000E-39 2.0925E 02 0.0000E-39	RW(18) 2.9394E 01 0.0000E-39 2.4432E 02 0.0000E-39 0.0000E-39 2.3173E C2 2.0287E 02 0.0000E-39 2.9562E 02 0.0000E-39	RW(19) 6.8200E 01 0.0000E-39 2.7799E 01 0.0000E-39 0.0000E-39 1.2680E C1 1.5805E 01 0.0000E-39 4.4494E 02 0.0000E-39	RW(20) 5.4945E 01 0.0000E-39 1.5118E 00 0.0000E-39 0.0000E-39 3.5100E C1 8.3672E 00 0.0000E-39 2.4754E 02 0.0000E-39	RW(21) 5.2576E 01 0.0000E-39 3.4375E 01 0.0000E-39 0.0000E-39 2.5608E C2 2.7555E 01 0.0000E-39 1.0976E 03 0.0000E-39	RW(22) 1.3115E 01 0.0000E-39 1.9724E 00 0.0000E-39 0.0000E-39 3.9848E-01 1.4727E 02 0.0000E-39 5.2734E 00 0.0000E-39	RW(23) 1.3804E 01 0.0000E-39 1.8676E 00 0.0000E-39 0.0000E-39 4.2969E-C2 3.1641E-01 0.0000E-39 1.8555E 00 0.0000E-39	RW(24) 1.3292E 01 0.0000E-39 1.7261E 00 0.0000E-39 0.0000E-39 4.2419E-C1 1.1309E 00 0.0000E-39 2.8516E 00 0.0000E-39	RW(25) 0.0000E-35 4.1533E 02 0.0000E-39 3.3128E 02 3.9637E 02 0.0000E-39 0.0000E-39 3.1236E 02 0.0000E-39 8.2744E 02	RW(26) 2.6866E 02 0.0000E-39 9.8421E 01 2.3779E 02 0.0000E-39 0.0000E-39 0.0000E-39 1.4145E 02 0.0000E-39 6.0822E 02	RW(27) 0.0000E-35 6.0814E 01 0.0000E-39 1.9750E 01 1.6982E 01 0.0000E-39 0.0000E-39 7.6827E 01 0.0000E-39 1.6031E 02	RW(28) 9.4685E 01 0.0000E-39 1.8972E 01 9.0152E 01 0.0000E-39 0.0000E-39 7.0633E 01 0.0000E-39 2.1469E 02	RW(29) 0.0000E-35 7.8335E 01 0.0000E-39 3.0563E 01 2.3034E 02 0.0000E-39 0.0000E-39 9.4191E 01 0.0000E-39 1.2226E 02	RW(30) 0.0000E-35 2.5151E 02 0.0000E-39 1.4841E 01 1.2625E 02 0.0000E-39 0.0000E-39 2.0047E 02 0.0000E-39 1.4472E 02	RW(31) 0.0000E-35 1.0539E 01 0.0000E-39 5.8646E 01 9.9668E 01 0.0000E-39 0.0000E-39 1.5266E 01 0.0000E-39 3.9182E 02	RW(32) 0.0000E-35 9.4587E 00 0.0000E-39 3.5377E 01 5.7664E 01 0.0000E-39 0.0000E-39 1.6250E 00 0.0000E-39 2.8105E 02	RW(33) 0.0000E-35 9.7040E 01 0.0000E-39 1.1004E 02 2.9480E 02 0.0000E-39 0.0000E-39 4.7578E 00 0.0000E-39 7.725CE 02	RW(34) 0.0000E-35 4.6052E-01 0.0000E-39 4.3798E-01 2.1484E-01 0.0000E-39 0.0000E-39 9.0234E-01 0.0000E-39 1.5781E 00	RW(35) 0.0000E-35 4.5888E-01 0.0000E-39 3.0786E-01 1.0930E-01 0.0000E-39 0.0000E-39 3.6328E-01 0.0000E-39 9.2965E-01	RW(36) 0.0000E-35 5.3004E-01 0.0000E-39 4.4427E-01 4.6875E-02 0.0000E-39 0.0000E-39 3.2227E-01 0.0000E-39 3.1719E 00

COLUMN(11)	COLUMN(12)	COLUMN(13)	COLUMN(14)	COLUMN(15)	COLUMN(16)	COLUMN(17)	COLUMN(18)	COLUMN(19)	COLUMN(20)					
RW(1) 0.0000E-35 5.2734E 00 0.0000E-39 3.2283E 01 0.0000E-39 1.4725E C2 2.8789E 00 0.0000E-39 1.1362E 02 0.0000E-39	RW(2) 0.0000E-35 4.4906E 01 0.0000E-39 8.2555E 01 0.0000E-39 4.8544E C2 1.9758E 01 0.0000E-39 5.7625E 01 0.0000E-39	RW(3) 0.0000E-35 2.3273E 01 0.0000E-39 3.0562E 01 0.0000E-39 1.7C90E C2 2.540CE 01 0.0000E-39 4.1437E 01 0.0000E-39	RW(4) 0.0000E-35 5.4187E 01 0.0000E-39 3.2562E 01 0.0000E-39 2.3500E 01 8.1256E 00 0.0000E-39 2.5087E 02 0.0000E-39	RW(5) 0.0000E-35 1.8438E 00 0.0000E-39 1.5156E 00 0.0000E-39 1.4922E C0 5.000CE-01 0.0000E-39 6.250CE 00 0.0000E-39	RW(6) 0.0000E-35 9.4336E-01 0.0000E-39 7.5391E-01 0.0000E-39 4.3473E-C1 6.1719E-01 0.0000E-39 1.1719E-01 0.0000E-39	RW(7) 2.7133E 01 0.0000E-39 1.3617E 01 0.0000E-39 4.0594E C1 0.0000E-39 C.0000E-39 1.0270E 01 0.0000E-39 1.7119E 02	RW(8) 9.4242E 01 0.0000E-39 4.1461E 01 0.0000E-39 0.0000E-39 0.0000E-39 0.0000E-39 2.2178E 02	RW(9) 2.7117E 01 0.0000E-39 2.2859E 01 0.0000E-39 9.6109E 01 0.0000E-39 0.0000E-39 1.8106E 02	RW(10) 4.45719E 01 0.0000E-39 1.91C66E 01 0.0000E-39 1.5312E 01 0.0000E-39 0.0000E-39 2.9275E 02	RW(11) 1.56225E 00 0.0000E-39 2.3594E 00 0.0000E-39 1.4414E 00 0.0000E-39 0.0000E-39 3.1250E-01 0.0000E-39 5.250CE 00	RW(12) 1.1661E 00 0.0000E-39 7.6953E 01 0.0000E-39 6.6460E-01 0.0000E-39 0.0000E-39 2.7734E-01 0.0000E-39 1.3750E 00	RW(13) 0.0000E-39 2.6125E 02 0.0000E-39 1.2481E 02 0.0000E-39 6.7875E C1 2.8625E 01 0.0000E-39 1.96CCE 02 0.0000E-39	RW(14) 0.0000E-39 6.5312E 01 0.0000E-39 2.4625E 02 0.0000E-39 2.3912E 02 4.6594E 01 0.0000E-39 2.65CCE 02 0.0000E-39	RW(15) 0.0000E-39 1.8312E 01 0.0000E-39 5.7002E 01 0.0000E-39 2.0225E C2 5.1875E 0C 0.0000E-39 6.200CE 01 0.0000E-39

RW(16)	0.0000E-39	7.8437E 01	0.00CCE-39	8.9437E 01	0.00CCE-39	2.88CCE C2	8.5687E CC	0.0CCOE-39	4.375CE 00	0.0000E-39
RW(17)	0.0000E-39	1.3012E 02	0.0CCCCE-39	1.1678E 02	0.00CCE-39	2.7187F C2	4.4266E 01	0.0CCOE-39	1.7625E 02	0.0000E-39
RW(18)	'1.0000E-39	8.3931E 01	0.00CCE-39	1.9544E 02	0.0000E-39	4.3575E C2	3.2344E 01	0.0CCOE-39	8.4450E 02	0.0000E-39
RW(19)	0.0000E-39	5.3500E 01	0.0000E-39	6.8625E 01	0.0000E-39	1.3541E 01	8.750CE CC	0.0CCOE-39	7.1500E 01	0.0000E-39
RW(20)	0.0000E-39	3.4437E 01	0.00CCE-39	4.7500E 01	0.0000E-39	3.4669E C1	1.8125E 01	0.0CCOE-39	1.0542E 01	0.0000E-39
RW(21)	3.0000E-35	2.6406E 02	0.00CCCCE-39	1.6647E 02	0.0000E-39	1.2800E C1	0.0CCOE-39	0.0CCOE-39	1.970CE 02	0.0000E-39
RW(22)	0.0000E-35	4.4531E 00	0.0000CCE-39	3.0937E 00	0.0000E-39	2.1094E C0	2.5156E 00	0.0CCOE-39	2.125CE 00	0.0000E-39
RW(23)	0.0000E-35	2.3438E 00	0.0000CCE-39	1.4046E 00	0.0000E-39	8.2813E-01	9.6875E-01	0.0000E-39	9.8438E-01	0.0000E-39
RW(24)	0.0000E-35	4.2056E 00	0.0000CCE-39	4.8438E 00	0.0000E-39	1.1875E C0	2.6719E 00	0.0CCOE-39	1.9063E 00	0.0000E-39
RW(25)	4.0012E 02	0.0000E-39	4.0381E 02	0.0000E-39	2.5450E C2	0.00CCE-39	C.CCCE-35	1.854CE 02	0.000CE-39	4.9900E 02
RW(26)	4.5144E 02	0.0000E-39	1.1537E 02	0.00CCE-39	4.8600E C2	0.0000E-39	7.1516E 01	0.000CE-39	5.695CE 02	
RW(27)	3.2562E 31	0.0000E-39	7.7062E 01	0.00CCE-39	1.1425E C2	0.0000E-39	2.9344E 01	0.000CE-39	2.185CE 02	
RW(28)	1.8956E 32	0.0000E-39	2.6156E 01	0.0000E-39	6.1800E C1	0.0CCOE-39	C.CCCE-39	7.3750F 00	0.000CE-39	1.0454E 03
RW(29)	1.8787E 03	0.0000E-39	1.2046E 00	0.0000E-39	3.6975E 00	0.0CCOE-39	C.CCCE-39	3.6719E 01	0.000CE-39	7.3556E 02
RW(30)	1.16162E 02	0.0000E-39	6.3156E 01	0.0000E-39	6.0250E C1	0.0CCOE-39	0.0CCOE-39	1.050CE 01	0.000CE-39	8.3050E 02
RW(31)	1.1800E 02	0.0000E-39	2.5406E 01	0.0000E-39	1.5558E C2	0.0000E-39	0.0CCOE-39	1.4312E 01	0.0000E-39	5.7125E 02
RW(32)	6.1344E 01	0.0000E-39	4.9375E 00	0.00CDE-39	6.6219E C1	0.0CCOE-39	C.CCCE-39	4.5625E 00	0.000CE-39	1.8450E 02
RW(33)	2.7656E 02	0.0000E-39	1.0339E 02	0.0033E 02	2.0131E C2	0.0CCOE-39	C.CCCE-39	2.9250E 01	0.000CE-39	1.011CE 03
RW(34)	2.6044E 03	0.0000E-39	1.5312E 00	0.000GE-39	7.8125E C2	0.0000E-39	0.0CCOE-39	1.7188E-01	0.000CE-39	2.625CE 00
RW(35)	1.5625E 03	0.0000E-39	1.5625E 00	0.0000E-39	1.8750E-01	0.0CCOE-39	C.CCCE-39	6.2550E-02	0.000CE-39	9.3750E-02
RW(36)	4.8594E 03	0.0000E-39	4.7187E 01	0.0000E-39	8.4375E C1	0.0CCOE-39	C.CCCE-39	2.14C6E 0C	0.00CCE-39	8.750CE 01

COLUMN(21)	COLUMN(22)	COLUMN(23)	COLUMN(24)	COLUMN(25)	COLUMN(26)	COLUMN(27)	COLUMN(28)	COLUMN(29)	COLUMN(30)	
RW(1)	3.8850E 02	0.0000E-39	0.00CCE-39	5.8730E 00	0.0C00E-39	2.0966E C2	C.CCCE-39	1.6566E 02	0.00CCE-39	1.2793E-01
RW(2)	2.9931E 02	0.0000E-39	0.00CCE-39	1.2418E 01	0.0000E-39	1.8125E C0	C.CCCE-39	5.5754E 04	0.000CE-39	5.6032E 01
RW(3)	2.2937E 01	0.0000E-39	0.000CE-39	1.8828E 01	0.0000E-39	2.7573E C2	C.CCCE-39	4.5333E 04	0.000CE-39	2.4453E 00
RW(4)	7.3875E 01	0.0000E-39	0.00CCE-39	1.7750E 01	0.0000E-39	2.8000E C2	C.CCCE-39	1.0551E 04	0.00CCE-39	4.4355F 01
RW(5)	5.1250F 0C	0.0000E-39	0.000CE-39	1.0250E 01	0.0000E-39	1.0250E C2	C.CCCE-39	1.9462E 04	0.00CCE-39	2.1875E-01
RW(6)	4.3594E 0C	0.0000E-39	0.000CE-39	2.9531E 00	0.0000E-39	2.4581E C2	C.CCCE-39	4.3765E 04	0.000CE-39	4.9492E 00
RW(7)	0.0000E-39	4.0375E 02	4.8164E 00	0.0000E-39	9.1344E C1	0.0CCCE-39	5.1478E 02	0.00CCE-39	1.6467E-01	0.0000E-39
RW(8)	0.0000E-39	4.6719E 02	2.4891E 01	0.0000E-39	6.2437E C1	0.0000E-39	4.5606E 04	0.0CCOE-39	5.6955E 01	0.000CE-35
RW(9)	0.0000E-39	1.205CE 02	2.00CCE 00	0.0000E-39	2.4490E 02	0.0000E-39	4.0301E 04	0.0CCOE-39	1.5547E 00	0.0000E-39
RW(10)	0.0000E-39	7.1250E 01	1.900CE 01	0.0000E-39	8.7600E 01	0.0000E-39	8.9459E 03	0.0CCOE-39	4.1953E 01	0.0000E-39
RW(11)	0.0000E-39	8.250CE 00	8.00CCCCE 00	0.0000E-39	1.6000E 01	0.0000E-39	1.7225E 04	0.0CCOE-39	3.000CE 00	0.0000E-39
RW(12)	0.0000E-39	8.9063E 03	3.125CE-02	0.0000E-39	4.9375E C1	0.0000E-39	3.7474E 04	0.0000E-39	3.4023E 00	0.0000E-39
RW(13)	2.4910E 03	0.0000E-39	0.000CE-39	7.1562E 01	0.0000E-39	3.7275E C2	C.CCCE-39	4.3830E 03	0.000CE-39	9.2969E 00
RW(14)	5.0350E 02	0.0000E-39	0.000CE-39	2.5094E 01	0.0000E-39	9.3525E 02	C.CCCE-39	5.8547E 03	0.000CE-39	8.4561E 00
RW(15)	1.2520E 01	0.0000E-39	0.000CE-39	2.4914E 01	0.0000E-39	2.6669E 02	C.CCCE-35	7.4135E 03	0.000CE-39	1.0549E 01
RW(16)	1.4252E 01	0.0000E-39	0.000CE-39	5.6953E 00	0.0000E-39	4.5262E 00	C.CCCE-39	3.9172E 04	0.000CE-39	5.2271E 01
RW(17)	3.2100E 02	0.0000E-39	0.000CE-39	2.9492E 00	0.0000E-39	1.6637E 02	C.CCCE-39	3.8021E 04	0.000CE-39	5.2377E 01
RW(18)	2.0431E 93	0.0000E-39	0.000CE-39	5.4500E 01	0.0000E-39	3.1275E 02	C.CCCE-35	4.1242E 04	0.000CE-39	5.0648E 01
RW(19)	6.0500E 93	0.0000E-39	0.000CE-39	1.6875E 01	0.0000E-39	2.2500E 00	C.CCCE-35	1.9759E 04	0.000CE-39	4.4367E 01
RW(20)	1.5625E 01	0.0000E-39	0.000CE-39	1.3500E 01	0.0000E-39	2.6595E 02	C.CCCE-39	1.4437E 04	0.000CE-39	3.8812E 01
RW(21)	1.6270E 02	0.0000E-39	0.000CE-39	3.0000E-39	0.0000E-39	4.6686E 01	C.CCCE-39	1.4556E 04	0.000CE-39	1.4375E 01
RW(22)	4.6250E 0C	0.0000E-39	0.000CE-39	5.1250E 00	0.0000E-39	1.7375E 02	C.CCCE-35	3.1116E 04	0.000CE-39	2.0078E 01
RW(23)	5.6797E 0C	0.0000E-39	0.000CE-39	6.3750E 00	0.0000E-39	2.3812E 02	C.CCCE-35	4.2441E 04	0.000CE-39	3.3906E 00
RW(24)	4.5000E 0C	0.0000E-39	0.000CE-39	6.2500E-01	0.0000E-39	1.9200E 02	C.CCCE-35	3.4940E 04	0.000CE-39	1.2484E 01
RW(25)	0.0300E-35	1.8260E 03	1.2484E 02	0.0000E-39	2.5727E 03	0.0000E-39	5.4832E 03	0.0CCOE-39	1.1585E 01	0.000CE-39
RW(26)	0.0000E-39	2.1875E 03	2.1212E 01	0.0000E-39	1.4919E 03	0.0000E-39	6.1589E 03	0.0CCOE-39	1.2021E 01	0.0000E-39
RW(27)	0.0000E-39	8.8575E 02	1.5422E 01	0.0000E-39	2.6595E 02	0.0000E-39	6.5222E 03	0.0CCOE-39	1.1567E 01	0.000CE-39
RW(28)	0.0000E-39	7.1925E 02	3.3453E 00	0.0000E-39	5.7312F C1	0.0000E-39	3.4782E 04	0.000CE-39	4.8275E 01	0.0000E-39
RW(29)	0.0300E-39	6.6150E 02	3.3418E 01	0.0000E-39	1.4794E 02	0.0000E-39	3.3345E 04	0.000CE-39	4.6273E 01	0.0000E-39
RW(30)	0.0000E-39	5.3587E 02	1.7727E 01	0.0000E-39	5.7612E C2	0.0000E-39	3.6312E 04	0.0CCOE-39	5.2963E 01	0.000CE-39
RW(31)	0.0000E-39	1.1859E 02	3.2984E 01	0.0000E-39	1.5700E 02	0.0000E-39	1.4001E 04	0.0CCOE-39	4.6711E 01	0.000CE-39
RW(32)	0.0000E-39	1.0112E 02	9.750CE 00	0.0000E-39	8.5600E C0	0.0000E-39	1.2777E 04	0.0CCOE-39	3.8062E 01	0.0000E-39
RW(33)	0.0000E-39	4.8100E 02	6.8750E 01	0.0000E-39	4.4200E 02	0.0000E-39	1.3034E 04	0.0CCOE-39	2.5114E 01	0.0000E-39
RW(34)	0.0000E-39	7.8750E 00	2.3750E 00	0.0000E-39	2.9500E L1	0.0000E-39	2.7607E 04	0.0CCOE-39	2.8125E 00	0.000CE-39
RW(35)	0.0000E-39	9.5859E 00	3.00CCE 00	0.0000E-39	4.6375E C1	0.0000E-39	3.7572E 04	0.0CCOE-39	6.3047E 00	0.0000E-39
RW(36)	0.0000E-39	8.8750E 00	2.50CCCCE-01	0.0000E-39	3.7750E C1	0.0000E-39	3.0896E 04	0.0CCOE-39	1.4641E 01	0.000CE-39

RW(1)	4.2188E-01	0.0000E-39	7.3600E 02	0.0000E-39	3.9808E C4	0.0CCOE-39				
RW(2)	1.7875E 04	0.0000E-39	8.5533E 07	0.0000E-39	6.6560E C3	0.0CCOE-39				
RW(3)	5.8981E 03	0.0000E-39	4.5366E 07	0.0000E-39	7.3600E C3	0.0CCOE-39				
RW(4)	3.4425E 03	0.0000E-39	9.8484E 05	0.0000E-39	9.9200E -2	0.0CCOE-39				
RW(5)	2.3264E 02	0.0000E-39	7.3957E 06	0.0000E-39	3.9156E L1	0.0CCOE-39				
RW(6)	1.8875E 02	0.0000E-39	7.1885E 05	0.0000E-39	1.8966E CC	0.0CCOE-39				
RW(7)	0.0000E-39	1.4043E 00	0.000CE-39	8.8956E 03	0.0000E-39	3.3353E C4	0.0CCOE-39			
RW(8)	0.0000E-39	1.9961E 04	0.000CE-39	3.1259E 07	0.0000E-39	2.1248E C4	0.0CCOE-39			
RW(9)	0.0000E-39	6.5566E 03	0.000CE-39	5.4390E 07	0.0000E-39	7.2320E C3	0.0CCOE-39			
RW(10)	0.0000E-39	3.8871E 03	0.000CE-39	1.9117E 06	0.0000E-39	2.5920E C3	0.0CCOE-39			
RW(11)	0.0000E-39	2.5705E 02	0.000CE-39	8.8626D 06	0.0000E-39	1.1406E C1	0.0CCOE-39			
RW(12)	0.0000E-39	2.0100E-02	0.000CE-39	8.6094E 05	0.0000E-39	2.7464E 04	0.0CCOE-39			
RW(13)	1.3960E 04	0.0000E-39	4.3076E 07	0.0000E-39	2.5776E 04	0.0CCOE-39				
RW(14)	1.5165E 04	0.0000E-39	1.5725E 07	0.0000E-39	7.5776E 04	0.0CCOE-39				
RW(15)	1.7870E 04	0.0000E-39	4.2829E 07	0.0000E-39	6.0416E 04	0.0CCOE-39				
RW(16)	3.2379E 03	0.0000E-39	5.265CE 07	0.0000E-39	6.7584E 04	0.0CCOE-39				
RW(17)	2.5016E 03	0.0000E-39	6.5604E 07	0.0000E-39	1.3556E 04	0.0CCOE-39				
RW(18)	3.7309E 23	0.0000E-39	5.3545E 07	0.0000E-39	2.0408E 04	0.0CCOE-39				
RW(19)	1.6116E 04	0.0000E-39	1.2311E 07							

NORMALIZED ERR.P MATRIX

	COLUMN(1)	COLUMN(2)	COLUMN(3)	COLUMN(4)	COLUMN(5)	COLUMN(6)	COLUMN(7)	COLUMN(8)	COLUMN(9)	COLUMN(10)	
RW(1)	6.3371E-05	0.0000E-39	7.303CE-01	0.0000E-39	0.0000E-39	6.215AE-05	2.0992E-05	0.0000E-39	2.58C9E-05	0.0000E-39	
RW(2)	2.4570E-05	0.0000E-39	7.2657E-00	0.0000E-39	0.0000E-39	1.0146E-04	1.0157E-04	0.0000E-39	4.1425E-05	0.0000E-39	
RW(3)	2.3281E-01	0.0000E-39	6.5241E-01	0.0000E-39	0.0000E-39	1.3553E-04	4.3422E-04	0.0000E-39	3.00C1E-05	0.0000E-39	
RW(4)	3.0181E-05	0.0000E-39	4.1659E-01	0.0000E-39	0.0000E-39	0.0000E-39	2.078CE-04	1.9602E-05	0.0000E-39	8.4995E-05	0.0000E-39
RW(5)	2.0635E-05	0.0000E-39	2.3761E-00	0.0000E-39	0.0000E-39	3.0600E-05	3.9218E-05	0.0000E-39	0.0000E-39	0.0000E-39	
RW(6)	2.0261E-05	0.0000E-39	2.0141E-00	0.0000E-39	0.0000E-39	0.0000E-39	1.3245E-05	9.675CE-07	0.0000E-39	1.729CE-06	0.0000E-39
RW(7)	0.0000E-39	3.1335E-00	0.0000E-39	2.3419E-00	5.7889E-05	0.0000E-39	0.0000E-39	7.7870E-05	0.0000E-39	4.7083E-05	
RW(8)	0.0000E-35	2.8521E-00	0.0000E-39	7.7828E-00	4.8675E-05	0.0000E-39	0.0000E-39	6.4728E-05	0.0000E-39	2.8620E-05	
RW(9)	0.0000E-39	5.3257E-00	0.0000E-39	2.5721E-00	2.3711E-04	0.0000E-39	0.0000E-39	3.6243E-04	0.0000E-39	6.4824E-05	
RW(10)	0.0000E-39	6.2279E-01	0.0000E-39	3.0715E-01	3.8372E-04	0.0000E-39	0.0000E-39	4.8223E-07	0.0000E-39	1.171CE-04	
RW(11)	0.0000E-39	5.8253E-00	0.0000E-39	1.8272E-01	1.5575E-06	0.0000E-39	0.0000E-39	2.7495E-06	0.0000E-39	2.0542E-07	
RW(12)	0.0000E-39	2.0546E-00	0.0000E-39	3.7070E-02	4.2791E-07	0.0000E-39	0.0000E-39	9.8749E-07	0.0000E-39	2.3084E-06	
RW(13)	4.7813E-01	0.0000E-39	3.5532E-01	0.0000E-39	0.0000E-39	2.6396E-01	2.4125E-03	0.0000E-39	2.6844E-04	0.0000E-39	
RW(14)	5.5170E-03	0.0000E-39	1.6111E-01	0.0000E-39	0.0000E-39	1.9737E-04	4.7557E-03	0.0000E-39	1.8341E-04	0.0000E-39	
RW(15)	5.9022E-05	0.0000E-39	4.3554E-01	0.0000E-39	0.0000E-39	2.3489E-04	3.5752E-04	0.0000E-39	1.0826E-04	0.0000E-39	
RW(16)	1.6650E-02	0.0000E-39	5.9711E-01	0.0000E-39	0.0000E-39	1.5366E-04	2.3197E-04	0.0000E-39	4.325CE-05	0.0000E-39	
RW(17)	5.2919E-02	0.0000E-39	3.6555E-01	0.0000E-39	0.0000E-39	3.8992E-04	1.6178E-04	0.0000E-39	4.9747E-05	0.0000E-39	
RW(18)	8.0334E-05	0.0000E-39	9.3261E-01	0.0000E-39	0.0000E-39	4.4496E-04	4.4575E-04	0.0000E-39	9.0925E-05	0.0000E-39	
RW(19)	2.0110E-05	0.0000E-39	7.6492E-00	0.0000E-39	0.0000E-39	8.6228E-05	2.5209E-05	0.0000E-39	4.412CE-03	0.0000E-39	
RW(20)	2.2919E-05	0.0000E-39	4.5455E-01	0.0000E-39	0.0000E-39	2.5105E-05	1.1539E-05	0.0000E-39	7.6875E-04	0.0000E-39	
RW(21)	2.1511E-05	0.0000E-39	1.1515E-01	0.0000E-39	0.0000E-39	2.6114E-05	4.2376E-05	0.0000E-39	1.3891E-03	0.0000E-39	
RW(22)	2.0410E-05	0.0000E-39	2.1162E-00	0.0000E-39	0.0000E-39	2.2509E-06	7.9642E-06	0.0000E-39	5.4644E-06	0.0000E-39	
RW(23)	2.0226E-05	0.0000E-39	2.0917E-00	0.0000E-39	0.0000E-39	2.4204E-07	0.1C1CE-04	0.0000E-39	4.8026E-06	0.0000E-39	
RW(24)	2.0586E-05	0.0000E-39	2.2934E-00	0.0000E-39	0.0000E-39	1.2684E-06	5.0266E-06	0.0000E-39	3.3213E-06	0.0000E-39	
RW(25)	0.0000E-35	1.2159E-01	0.0000E-39	8.0908E-01	2.2119E-01	0.0000E-39	0.0000E-39	4.7264E-03	0.0000E-39	1.9650E-04	
RW(26)	0.0000E-35	5.9848E-00	0.0000E-39	1.3857E-01	2.4460E-03	0.0000E-39	0.0000E-39	3.3754E-03	0.0000E-39	1.7878E-04	
RW(27)	0.0000E-35	7.8455E-00	0.0000E-39	2.5523E-01	9.0347E-05	0.0000E-39	0.0000E-39	7.6351E-05	0.0000E-39	6.6013E-05	
RW(28)	0.0000E-35	9.3686E-00	0.0000E-39	3.2838E-00	1.8089E-04	0.0000E-39	0.0000E-39	1.3298E-04	0.0000E-39	5.941CE-05	
RW(29)	0.0000E-35	8.8069E-00	0.0000E-39	2.4239E-00	5.0295E-04	0.0000E-39	0.0000E-39	2.1C80E-04	0.0000E-39	2.9153E-05	
RW(30)	3.0000E-39	2.3439E-01	0.0000E-39	1.0933E-01	2.4243E-04	0.0000E-39	0.0000E-39	3.4559E-04	0.0000E-39	4.512E-05	
RW(31)	0.0000E-35	3.8322E-00	0.0000E-39	3.5483E-00	6.7860E-04	0.0000E-39	0.0000E-39	3.9430E-05	0.0000E-39	3.8898E-03	
RW(32)	0.0000E-35	3.8465E-00	0.0000E-39	2.3502E-00	4.1251E-06	0.0000E-39	0.0000E-39	2.24C9E-06	0.0000E-39	8.7327E-04	
RW(33)	0.0000E-35	4.1588E-01	0.0000E-39	8.0348E-00	3.0109E-03	0.0000E-39	0.0000E-39	7.3513E-06	0.0000E-39	9.7738E-04	
RW(34)	0.0000E-35	2.3027E-00	0.0000E-39	1.30369E-01	1.2137E-06	0.0000E-39	0.0000E-39	4.88C0E-06	0.0000E-39	1.6352E-06	
RW(35)	0.0000E-35	2.0476E-00	0.0000E-39	8.9768E-02	5.1933E-07	0.0000E-39	0.0000E-39	1.1494E-06	0.0000E-39	2.4061E-06	
RW(36)	0.0000E-35	2.0498E-00	0.0000E-39	1.2736E-01	2.4550E-07	0.0000E-39	0.0000E-39	1.4513E-06	0.0000E-39	3.6941E-06	
	COLUMN(11)	COLUMN(12)	COLUMN(13)	COLUMN(14)	COLUMN(15)	COLUMN(16)	COLUMN(17)	COLUMN(18)	COLUMN(19)	COLUMN(20)	
RW(1)	0.0000E-39	5.4742E-06	0.0000E-39	1.7E27E-04	0.0000E-39	6.3015E-05	8.2C06E-06	0.0000E-39	3.7037E-05	0.0000E-39	
RW(2)	0.0000E-35	2.4488E-05	0.0000E-39	1.2513E-04	0.0000E-39	1.0959E-04	3.5347E-05	0.0000E-39	1.5143E-05	0.0000E-39	
RW(3)	0.0000E-35	3.2149E-05	0.0000E-39	1.5366E-05	0.0000E-39	1.2517E-04	1.2278E-04	0.0000E-39	6.9732E-06	0.0000E-39	
RW(4)	0.0000E-35	1.8706E-05	0.0000E-39	8.0480E-06	0.0000E-39	1.008CE-05	2.2733E-06	0.0000E-39	1.5471E-05	0.0000E-39	
RW(5)	0.0000E-35	6.6242E-07	0.0000E-39	7.2694E-07	0.0000E-39	3.1645E-06	1.4132E-07	0.0000E-39	2.8353E-07	0.0000E-39	
RW(6)	0.0000E-35	4.0797E-06	0.0000E-39	1.6725E-06	0.0000E-39	6.4299E-07	1.2828E-06	0.0000E-39	1.3752E-07	0.0000E-39	
RW(7)	2.8167E-05	0.0000E-39	7.5153E-05	0.0000E-39	1.7371E-05	0.0000E-39	7.5153E-05	0.0000E-39	5.5791E-05	0.0000E-39	
RW(8)	5.2319E-05	0.0000E-39	6.2838E-05	0.0000E-39	4.6192E-05	0.0000E-39	0.0000E-39	7.6162E-05	0.0000E-39	5.8273E-05	
RW(9)	3.7460E-05	0.0000E-39	1.1453E-05	0.0000E-39	2.1516E-04	0.0000E-39	0.0000E-39	1.7363E-04	0.0000E-39	3.0464E-05	
RW(10)	1.5782E-05	0.0000E-39	2.9427E-06	0.0000E-39	2.3725E-05	0.0000E-39	0.0000E-39	8.3322E-08	0.0000E-39	2.3815E-07	
RW(11)	5.6141E-07	0.0000E-39	1.3131E-06	0.0000E-39	3.0568E-06	0.0000E-39	0.0000E-39	8.8322E-08	0.0000E-39	1.8053E-05	
RW(12)	5.0342E-06	0.0000E-39	1.7072E-06	0.0000E-39	1.2421E-06	0.0000E-39	0.0000E-39	3.0134E-06	0.0000E-39	1.6135E-06	
RW(13)	3.9541E-05	0.0000E-39	2.0504E-05	0.0000E-39	4.1734E-06	0.0000E-39	0.0000E-39	4.1818E-06	0.0000E-39	0.0000E-39	
RW(14)	0.0000E-39	1.0301E-05	0.0000E-39	3.9214E-05	0.0000E-39	1.4570E-05	0.0000E-39	3.2995E-05	0.0000E-39	1.2685E-06	
RW(15)	0.0000E-39	3.0761E-06	0.0000E-39	8.6466E-06	0.0000E-39	3.2166E-05	2.2167E-06	0.0000E-39	1.0016E-05	0.0000E-39	
RW(16)	0.0000E-35	1.0953E-05	0.0000E-39	3.6346E-05	0.0000E-39	3.019CE-05	3.711CE-06	0.0000E-39	2.6688E-07	0.0000E-39	
RW(17)	0.0000E-35	1.8952E-05	0.0000E-39	6.7548E-05	0.0000E-39	2.5907E-05	2.2772E-05	0.0000E-39	1.097CE-05	0.0000E-39	
RW(18)	0.0000E-39	1.1449E-05	0.0000E-39	3.6874E-05	0.0000E-39	4.9138E-05	1.2119E-05	0.0000E-39	2.2524E-05	0.0000E-39	
RW(19)	0.0000E-35	1.1960E-05	0.0000E-39	2.1916E-05	0.0000E-39	1.2751E-04	1.5756E-05	0.0000E-39	3.8487E-06	0.0000E-39	
RW(20)	7.0000E-35	8.3479E-06	0.0000E-39	1.4366E-05	0.0000E-39	8.3420E-05	3.2626E-06	0.0000E-39	1.6985E-06	0.0000E-39	
RW(21)	0.0000E-39	6.1228E-05	0.0000E-39	9.4584E-05	0.0000E-39	4.0243E-05	1.2129E-05	0.0000E-39	7.0311E-06	0.0000E-39	
RW(22)	0.0000E-39	2.1475E-06	0.0000E-39	6.1398E-06	0.0000E-39	1.1111E-06	1.8522E-06	0.0000E-39	3.8737E-07	0.0000E-39	
RW(23)	0.0000E-39	1.5234E-06	0.0000E-39	7.4723E-07	0.0000E-39	3.7959E-07	4.4382E-07	0.0000E-39	9.0926E-07	0.0000E-39	
RW(24)	0.0000E-39	2.1153E-06	0.0000E-39	1.7147E-06	0.0000E-39	5.4474E-07	1.6179E-06	0.0000E-39	5.2932E-07	0.0000E-39	
RW(25)	6.0552E-05	0.0000E-39	9.4735E-05	2.5478E-05	0.0000E-39	1.7751E-05	0.0000E-39	3.2272E-05	0.0000E-39	6.9875E-06	
RW(26)	7.1193E-05	0.0000E-39	1.8373E-05	2.9262E-05	0.0000E-39	2.9616E-05	0.0000E-39	5.8078E-05	0.0000E-39	1.6308E-05	
RW(27)	5.4691E-05	0.0000E-39	1.6777E-05	3.0902E-05	0.0000E-39	5.6587E-06	0.0000E-39	0.0000E-39	1.2878E-05	0.0000E-39	
RW(28)	2.6471E-05	0.0000E-39	1.08C7E-05	3.6934E-05	0.0000E-39	8.3943E-06	0.0000E-39	0.0000E-39	3.0515E-06	0.0000E-39	
RW(29)	2.7363E-05	0.0000E-39	6.9806E-05	0.0000E-39	3.5234E-05	0.0000E-39	0.0000E-39	1.8888E-05	0.0000E-39	4.5782E-05	
RW(30)	2.4774E-05	0.0000E-39									

RW(1)	2.2629E-06	0.0000E-39	1.8095E-07	0.0CC0E-39	3.3676E-06	0.0CC00E-39
RW(2)	5.2759E-31	0.0000E-39	6.94C6E-03	0.0000E-39	2.9624E-07	0.0CC00E-39
RW(3)	5.4568E-04	0.0000E-39	1.565AE-03	0.0000E-39	1.0749E-06	0.0CC0CE-39
RW(4)	3.2629E-04	0.0000E-39	6.66C6E-05	0.0000E-39	2.6CS8E-07	0.0CC0E-39
RW(5)	2.3049E-04	0.0000E-39	1.21F7E-09	0.0000E-39	1.5559E-05	0.0000E-39
RW(6)	1.8926E-05	0.0000E-39	3.1898E-01	0.0000E-39	1.7U28E-06	0.0CC00E-39
RW(7)	0.0000E-39	7.5216E-06	0.0000E-39	1.9886E-06	0.0000E-39	2.3790E-C6
RW(8)	0.0000E-39	6.1362E-01	0.0CC0E-39	7.5734E-03	0.0000E-39	8.5965E-C7
RW(9)	0.0000E-39	6.0763E-04	0.0CC0E-39	2.1427E-03	0.0000E-39	9.6007E-C7
RW(10)	3.3000E-39	3.6852E-04	0.0000E-39	7.3268E-05	0.0000E-39	6.1998E-C7
RW(11)	0.0000E-39	2.5468E-04	0.0000E-39	1.4612E-01	0.0000E-39	1.1849E-C4
RW(12)	0.0000E-39	2.0154E-05	0.0000E-39	3.8282E-01	0.0000E-39	1.C285E-C5
RW(13)	7.63002E-39	0.0000E-39	1.138CE-03	0.0000E-39	2.5154E-07	0.0CC00E-39
RW(14)	1.2433E-02	0.0000E-39	6.1779E-04	0.0000E-39	1.0265E-06	0.0CC00E-39
RW(15)	5.4512E-02	0.0000E-39	6.3473E-03	0.0000E-39	3.0629E-C6	0.0CC0E-39
RW(16)	2.1800E-03	0.0000E-39	1.1095E-02	0.0000E-39	2.4080E-06	0.0CC0CE-39
RW(17)	6.9465E-04	0.0000E-39	2.134CE-03	0.0000E-39	4.6691E-07	0.0000E-39
RW(18)	2.2468E-03	0.0000E-39	1.94C1E-02	0.0000E-39	4.3907E-07	0.0CC00E-39
RW(19)	9.8242E-34	0.0000E-39	5.39C5E-04	0.0000E-39	3.2687E-C7	0.0CC0E-39
RW(20)	2.1378E-04	0.0000E-39	9.1251E-05	0.0000E-39	3.3338E-C7	0.0000E-39
RW(21)	1.8248E-03	0.0000E-39	7.6481E-04	0.0000E-39	1.4957E-C7	0.0000E-39
RW(22)	2.8529E-05	0.0000E-39	2.5645E-01	0.0030E-39	2.6016E-06	0.0CC00E-39
RW(23)	1.1134E-04	0.0000E-39	1.8957E-02	0.0000E-39	1.3956E-C5	0.0CC00E-39
RW(24)	3.8231E-06	0.0000E-39	2.7938E-01	0.0000E-39	2.8114E-06	0.0CC00E-39
RW(25)	0.0000E-39	8.4894E-03	0.0000E-39	1.2404E-03	0.0000E-39	4.3195E-C7
RW(26)	0.0000E-39	1.3882E-02	0.0000E-39	6.7337E-04	0.0000E-39	2.5222E-C7
RW(27)	0.0000E-39	6.0860E-02	0.0000E-39	6.9272E-03	0.0000E-39	6.2532E-C7
RW(28)	3.0000E-39	2.4223E-03	0.0000E-39	1.2091E-02	0.0000E-39	1.0747E-C6
RW(29)	0.0000E-39	7.7766E-04	0.0000E-39	2.3265E-02	0.0000E-39	1.3124E-C6
RW(30)	0.0000E-39	2.5181E-03	0.0000E-39	2.1197E-02	0.0000E-39	4.2909E-C7
RW(31)	0.0000E-39	1.0975E-03	0.0000E-39	5.8800E-04	0.0000E-39	1.0C05E-C4
RW(32)	0.0000E-39	2.3897E-04	0.0000E-39	9.8443E-05	0.0000E-39	9.8700E-C7
RW(33)	0.0000E-39	2.0467E-03	0.0000E-39	8.3398E-04	0.0000E-39	4.7593E-C7
RW(34)	0.0000E-39	3.1597E-05	0.0000E-39	3.0776E-01	0.0000E-39	1.2375E-C5
RW(35)	0.0000E-39	1.2158E-04	0.0000E-39	2.2473E-02	0.0000E-39	7.9117E-C5
RW(36)	0.0000E-39	2.5903E-06	0.0000E-39	3.3530E-01	0.0000E-39	1.3436E-C6